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MERGING PLEISTOCENE LITHOSTRATIGRAPHY WITH GEOTECHNICAL AND  
HYDROGEOLOGIC DATA - EXAMPLES FROM EASTERN WISCONSIN

by

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1988

## PREFACE

This open-file report is a Master of Science thesis by Sue A. Rodenbeck, University of Wisconsin-Madison Department of Geology and Geophysics. This work was completed while Ms Rodenbeck was employed as a Research Assistant by the Wisconsin Geological and Natural History Survey, and reflects the Survey's continuing interest in the hydrogeologic properties of Pleistocene materials in Wisconsin. This study was funded through the Survey by a grant from the Wisconsin Department of Natural Resources.

This report contains the most complete synthesis to date of hydrogeologic and geotechnical data from solid waste disposal sites in eastern Wisconsin. These data, collected from 41 sites, are organized by lithostratigraphic unit, and are presented in spreadsheet format. The report discusses the values and ranges of variation of hydraulic conductivity, grain size, Atterberg Limits, and other parameters in relation to lithostratigraphic unit. The resulting analyses should be of interest to regulatory agencies and private firms involved in waste disposal and other shallow geotechnical projects in eastern Wisconsin.

Merging Pleistocene Lithostratigraphy with Geotechnical and  
Hydrogeologic Data--Examples from Eastern Wisconsin

by

Sue Anita Rodenbeck

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## ABSTRACT

The objectives of this project are: 1) to identify the hydrogeologic and geotechnical properties of Pleistocene materials in eastern Wisconsin, 2) to associate the properties with mappable, extensive hydrostratigraphic units that can be identified in the field, and 3) to assess the variability and expected range of values within the individual units. This study is a synthesis of hydrogeologic and engineering data submitted by geotechnical consulting firms to the Wisconsin Department of Natural Resources. Values of hydraulic conductivity (380), particle size analyses (475 completed to .002 mm), Atterberg limits (525), approximations of strength (964 pocket penetrometer measurements), and dry unit weights (155) were compiled, geologically interpreted, and assigned to the till units in five mapped formations of late Wisconsin age. Published definitions of lithostratigraphic units are used.

The data are organized by till unit, then statistically analyzed to examine variation of properties within each till unit and to compare till units of superposed lithostratigraphic units. In cases for which at least five field measurements of hydraulic conductivity (K) are available at more than one site within a single till unit, ANOVA tests suggest that the till units have significant internal variation in K. Thus, the till units are heterogeneous. Application of ANOVA tests to field measurements of separate till units also indicates heterogeneity. Median field measurements of K vary considerably among till units of late Wisconsin age, from  $10^{-6}$  to

$10^{-4}$  cm/s. With respect to laboratory measurements of K at more than one site within a single till unit, only one till is homogeneous in a statistical sense while the others are statistically significantly different, thus heterogeneous. In contrast to field measurements, ANOVA tests of laboratory measurements of K for superposed, separate till units suggest that not all the till units are significantly different. Moreover, median laboratory and field measurements of K frequently differ by more than an order of magnitude for a single till unit.

Underlying relationships among the data recorded are statistically analyzed using correlation and regression. Median values of each parameter for each till unit were used in the analysis because geotechnical properties and hydraulic conductivity are typically not determined for the same sample. A weak relation between plastic limit and log field hydraulic conductivity ( $R^2 = 67\%$ ) and a relatively strong relationship between natural moisture content and dry unit weight ( $R^2 = 80\%$ ) could be used by hydrogeologists and engineers to constrain modeled values of hydraulic conductivity

Wisconsin Administrative Code should be modified to require a standard method for calculation of hydraulic conductivity from field measurements and should cite a specific reference for use of the Unified Soil Classification System. More than one classification and description system should be used, as no classification system seems best suited to hydrogeologic characterization. The lithostratigraphic framework has practical applications for landfill site assessment

since it is useful for predicting the occurrence and characteristics of subsurface materials.

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I would not have been able to complete my studies at the UW - Madison if it were not for the financial assistance of the Jessie Smith Noyes Foundation, the Wisconsin Geological and Natural History Survey, and the Department of Geology and Geophysics. The Department of Natural Resources funded this project through the Wisconsin Geological and Natural History Survey. The staff at the Bureau of Solid Waste Management, Wisconsin Department of Natural Resources provided me with the background information necessary to collect data, and the Bureau provided office space.

My fellow graduate students provided a stimulating environment for the exchange of ideas and opinions. I would have given up without their support during especially difficult times. I owe special thanks to fellow users of the Quaternary lab.

My list of acknowledgments would be incomplete without mention of my parents. My father instilled me with a desire to understand nature and with the belief that people matter more than books. My mother encouraged me to choose my own path and cheerfully shared the cost

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## I. Introduction

### A. Reason for study

Pleistocene materials cover roughly three-quarters of Wisconsin's surface, including its most densely populated areas, yet the hydrogeologic properties of these materials have not been fully assessed. Nationally, concern over human degradation of drinking water supplies has grown tremendously since the 1960s. Recent estimates indicate that "... 95 percent of rural America and in total about half the U. S. population rely on ground water" (U. S. EPA, 1987, p. 3). At the federal level, the actions of citizens concerned about degradation of water resources resulted in statutory laws like the National Environmental Pollution Act (1970), the Federal Water Pollution Control Act (1972), the Clean Water Act (1977), the Safe Drinking Water Act (1974), the Toxic Substances Control Act (1976), the Resource Conservation and Recovery Act (1976), and the Comprehensive Environmental Response, Compensation, and Liability Act (1980). These federal statutory laws required that the states create legislation to protect water resources. In Wisconsin, the Department of Natural Resources wrote Administrative Code Chapter NR 180, "Solid Waste Management," in response to Wisconsin Statutes Chapters 144 and 227 (Laws of 1977). Chapter NR 180 requires geotechnical investigations to document hydrogeologic conditions at proposed solid waste land disposal sites (hereafter referred to as 'landfills').

The data submitted in accord with NR 180 and similar regulations is important for protection of drinking water supplies near proposed

landfills, but much greater use could be made of the information if it could be easily retrieved and if it was organized so that a user could tell which information might be relevant to another location. Natural resource professionals working in the public and private sector are already accustomed to using written and computerized databases of well records and water quality analyses. A similar database of hydrogeologic and geotechnical data for Pleistocene materials in Wisconsin had not been attempted until this project. The Wisconsin Geological and Natural History Survey's Pleistocene mapping program and the development of a stratigraphic framework make this study possible.

#### B. Study definition

This study is part of a larger research project funded by the Wisconsin Department of Natural Resources and administered by the Wisconsin Geological and Natural History Survey. Long term objectives of the project are as follows:

1. To identify the hydrogeologic properties (permeability, porosity, etc.) and geotechnical properties (grain-size distribution, Atterberg limits, etc.) of Pleistocene materials in Wisconsin.
2. To associate these properties with mappable, areally extensive hydrostratigraphic units that can be identified in the field.
3. To assess the variability and expected range of values for these properties within any stratigraphic unit.
4. To develop field and laboratory methodologies for the evaluation of hydrogeologic and geotechnical properties in previously untested areas.

In keeping with these broad objectives, this study organizes and provides a geologic interpretation of the geotechnical and hydrogeologic information submitted in accord with NR 180 and other regulations for most of eastern Wisconsin. The lithostratigraphic framework defined in *Pleistocene Stratigraphic Units in Wisconsin* (Mickelson et al., 1984) is the organizational framework used to categorize the submitted data. I compiled the properties of samples and then assigned the data to a lithostratigraphic unit. I studied type and reference sections of these mapped units in the field to improve my interpretation of the data in reports. I combined the properties of each lithostratigraphic unit and then analyzed them. The statistical techniques used to assess the variability and the expected range of values are discussed later in this report. Although this study does not directly address the development of new methodologies, suggestions are made for improvements based on a review of existing geotechnical test methods and the statistical analysis of data.

In addition to the larger research project objectives, the data compilation, interpretation, and analysis completed here provide information for the discussion of three additional questions:

1. Are the formally defined lithostratigraphic units also hydrostratigraphic units?
2. Would other sampling and testing procedures better define the site hydrogeology?
3. Can geotechnical index tests function as lithic criteria to identify and differentiate units?

These issues are discussed in Part V.

### C. Location of study

I collected data from reports of geotechnical investigations on file at the Bureau of Solid Waste Management, Wisconsin Department of Natural Resources. I limited the study's extent to late Wisconsin-aged glacial sediments in twenty-four counties of eastern Wisconsin glaciated by the Green Bay and Lake Michigan Lobes of the Laurentide Ice Sheet (Figure 1). Plate 1 (in pocket) illustrates the location of more than forty proposed or existing landfills. My emphasis on the collection of grain size analyses, atterberg limits, and hydraulic conductivities restricted data collection to sites with relatively recent investigations, usually located in areas of dense population or economic development requiring land disposal facilities.

### D. Why combine geotechnical data with lithostratigraphy?

There are many good reasons for both engineers and geologists to organize geotechnical data into a lithostratigraphic framework. Geologic studies provide relevant background information prior to detailed civil, structural, or foundation engineering investigations. Geotechnical consultants unfamiliar with the state's Pleistocene materials may find the compiled index test data and summary of geologic history useful for bid preparation. Regulatory agencies can refer to the data analysis to evaluate the reasonableness of submitted reports containing geotechnical data for which no standardized quality assurance and quality control methods exist.

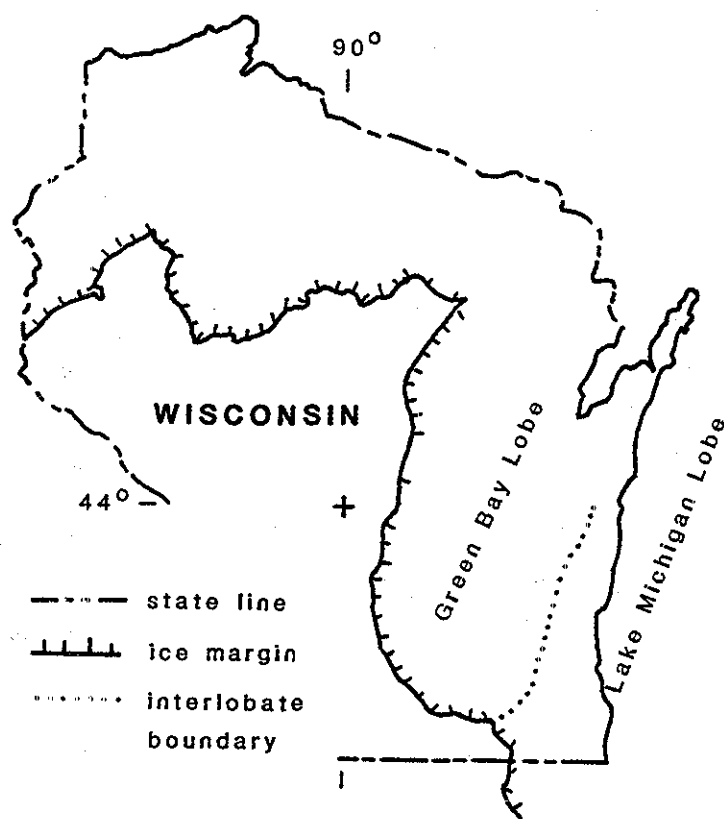


Figure 1. Maximum extent of ice during late Wisconsin time. Only the ice lobes pertinent to this study are labelled.

Hydrogeologists can use the hydraulic conductivity values reported here as input variables in groundwater flow models. Statistical summaries of hydraulic conductivity may be used to construct likely best and worst case scenarios for advective flow arrival times. Association of the hydraulic conductivity with mapped units makes it useful for site selection and screening on a statewide or regional scale.

Assessment of the local hydrogeologic setting prior to site-specific investigation usually consists of reviewing regional or county water resources investigations and geologic studies, soil surveys, and remote sensing techniques such as aerial photography. Unfortunately, water resources investigations in Wisconsin have tended to focus on bedrock aquifers, and have restricted discussion of Pleistocene and Holocene sediments to sand and gravel aquifers. Soil surveys are generally limited to materials within 6 feet of the land surface. This report uses the lithostratigraphic framework (Mickelson *et al.*, 1984) to present statistical summaries of geotechnical data for sediments from the land surface to bedrock, aquitards as well as aquifers. The same geologic conditions that make till units lithologically recognizable, areally continuous, and mappable may produce similar hydrogeologic and geotechnical properties within each unit. Once geotechnical data has been associated with lithostratigraphic units, the question, "Can geotechnical tests function as lithic criteria to differentiate units?" may be answered.

#### E. Problems of classification

The problem of how samples of earth materials should be described and classified has received considerable attention both in the past and in the present. The geologists who study the Quaternary materials in eastern Wisconsin define lithostratigraphic units using some or all of the criteria listed in Table 1 (Mickelson et al., 1984). The American Society for Testing Materials (ASTM) "Standard Practice for Classification of Soils for Engineering Purposes" (D2488-84, ASTM, 1986) relies upon the Unified Soil Classification System (USCS). The USCS criteria are also listed in Table 1. Soil scientists use yet another descriptive scheme (see Table 1) and have devoted considerable attention to the revisions to Chapter 4 in the *Soil Survey Manual*, "Examination and Description of Soils in the Field," (Soil Survey Staff, 1981). All of these classifications include grain size analysis and a description of the soil color; other criteria and descriptive terms are related but not synonymous.

Even the common factors of the classifications are expressed in different terms and thus are not directly transferable. For example, soil scientists and geologists who study the Quaternary describe the grain size distribution of a sample using a textural triangle (figure 2) on which sand, silt, and clay percentages of the less than 2 mm size fraction are plotted. Geotechnical reports for landfill investigations describe the grain size distribution of a sample using a USCS group name and group symbol. The same reports generally include graphs of cumulative percent finer versus particle size in

Table 1 Description of 'soil' for classification

- a. -by geologists who study the Quaternary in eastern Wisconsin  
(Mickelson et al., 1984)

texture  
munsell color  
clay mineralogy  
calcite to dolomite ratio  
pebble lithology  
stratigraphic position  
magnetic susceptibility  
depth of carbonate leaching

- b. -by USCS  
(ASTM, 1986)

percent finer than the #200 sieve (0.075 mm)  
coefficient of uniformity  
coefficient of curvature  
liquid limit  
plastic index  
plotted location on the plasticity chart

- c. -by soil scientists  
(Soil Survey Staff, 1981)

depth  
munsell color  
texture  
structure  
cutans  
consistance  
special features  
reaction or effervescence  
boundary



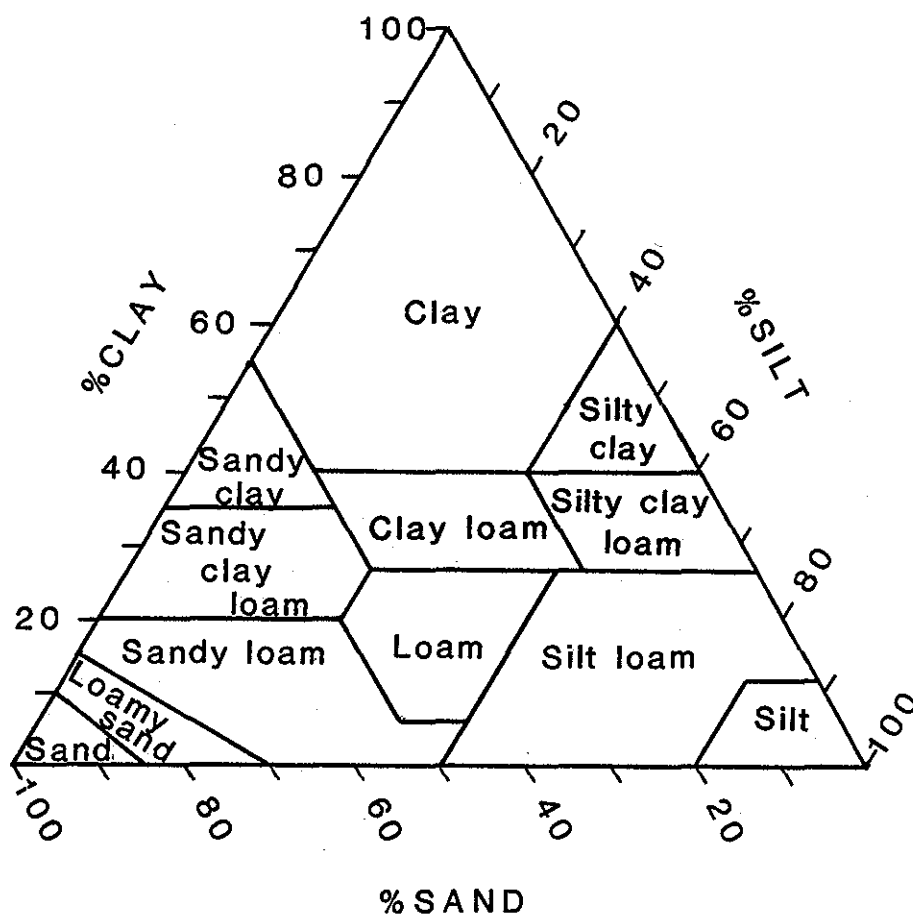


Figure 2. The U. S. Department of Agriculture (USDA) textural triangle. Both geologists and soil scientists use the textural triangle despite their differing definitions of silt and clay.

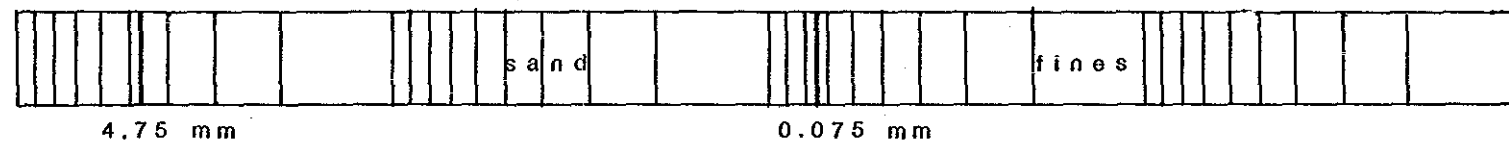
appendices. The exchange of information is hindered further by differing definitions of sand, silt, and clay. Figure 3 illustrates these definitions.

With respect to color, both Quaternary geologists and soil scientists use the Munsell color chart and notation (Munsell Color Co., Inc., Baltimore) in an attempt to standardize terminology. Geotechnical reports use descriptive phrases like "reddish-brown" that do not distinguish subtle variations in sediment color unless the phrases are standardized. Considering these inconsistent methods of sample description and classification, interdisciplinary transfer of information can be quite challenging.

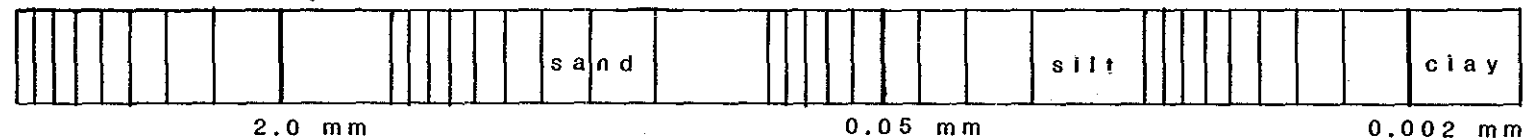
#### F. Combination of geological and geotechnical approaches

The approach of assigning geotechnical data to stratigraphic units is not without precedent. Many authors have combined geotechnical data with glacial depositional or sedimentary models, but few, if any combine existing geotechnical data, including hydraulic conductivities, with a published formal lithostratigraphic framework. Kenney (1976) discusses glacial sedimentation in fresh and marine waters, the fabric of lacustrine sediments, and the relationship between the preceding factors and geotechnical behavior. May and Thompson (1978) discuss the Quaternary glacial deposits of the Edmonton area and describe circumstances in which lack of geologic interpretation can lead to engineering problems. Mickelson, Acomb, and Edil (1979) studied Wisconsin's Lake Michigan shoreline using

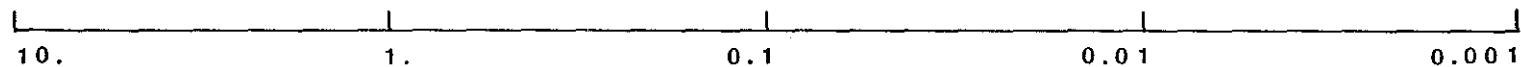
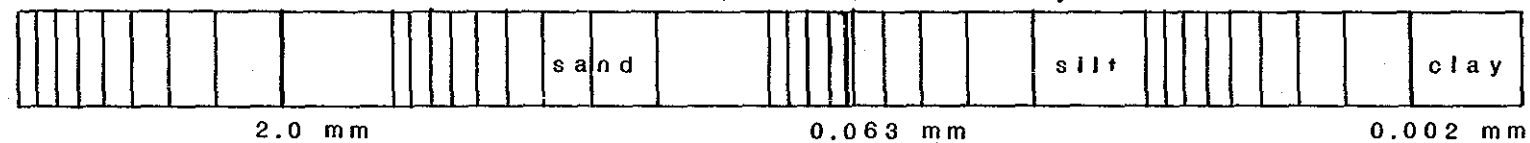
Unified Soil Classification System



USDA Soil Survey Staff



Wisconsin Geological and Natural History Survey, this study



grain size in millimeters, log 10 scale

Figure 3. The USCS does not divide 'fines' into silt and clay fractions. The geologists studying the Quaternary materials in Wisconsin and soil scientists divide the silt and clay classes at different particle sizes.

engineering index properties and shear strength to interpret glacial processes. Singh, Tatioussian, and Flagg (1983) used a lithostratigraphic framework for their statistical summary of geotechnical data for the Milwaukee area and found the depositional environment valuable to their interpretation of the data. Baracos et al. (1983) prepared a series of engineering and geotechnical maps from geotechnical and geological data collected from several thousand boreholes in urban Winnipeg, Manitoba. Although Baracos et al. incorporated geological genetic terms, stratigraphy, sedimentary environment, and post-depositional changes in the environment, they did not use lithostratigraphic names for glacial sediments. Lo and McCabe (1984) used existing engineering and pedologic data, grouped by physiographic regions and soil classification, to create a geotechnical data base for Indiana. Similar studies too numerous to detail here include those by Chassefiere and Monaco (1983), Connell (1984), Eyles and Sladen (1981), Quigley (1980), and Richards (1976). This study is different from these for three reasons: 1) the geotechnical data base includes both hydraulic conductivity and engineering properties, 2) the properties have been organized with a published lithostratigraphic framework, and 3) data from diverse sources are organized within a single spatial coordinate system.

## II. Pleistocene History and Stratigraphy

### A. Stratigraphic terminology

#### 1. Definition of rock stratigraphic terms

In addition to using the characteristics listed in Table 1, geologists subdivide, classify, and map sediments as stratigraphic units. The North American Stratigraphic Code (North American Commission on Stratigraphic Nomenclature (NACSN), 1983) requires that lithostratigraphic units be formally distinguished from each other and mapped on the basis of observable lithic characteristics and stratigraphic position. The formation is the fundamental unit in this system and must be mappable at land surface or traceable in the subsurface. Formations may be subdivided into members--these are the next lower hierarchy in the classification and need not be distinguishable in the field. Members are named when the formation is heterogeneous and when it is beneficial to do so. A member has lithic characteristics distinguishing it from adjacent parts of the formation.

#### 2. Definition of geochronologic terms

Geologists' stratigraphic nomenclature also includes geochronologic units. These are divisions of time traditionally distinguished by bodies of rock with synchronous boundaries (NACSN, Articles 66 and 80). Geochronologic terms used include eon, era, period, epoch, and age. Geochronologic epochs may be modified with

the adjectives Early, Middle, and Late (NACSN, Article 82). Capital letters indicate formal definition of time, whereas lower case, as in 'late Wisconsin', indicate informal use and lack of a formal definition. Figure 4a illustrates the temporal position of the late Wisconsin.

### 3. Definition of diachronic terms

Another category of stratigraphic terms, diachronic terms, is used when discussing the time during which the glacier produced specific stratigraphic units or an assemblage of units. Attig, Clayton, and Mickelson (1985) use event-stratigraphic units to associate landforms with ice advances that deposited specific lithostratigraphic units. These event-stratigraphic units are not recognized by the NACSN, but closely resemble the NACSN's diachronic units. Simultaneous use of lithostratigraphic, event-stratigraphic or diachronic, and geochronologic names confuses users and complicates the nomenclature. However, it also reduces confusion caused by revisions of the nomenclature when the same name (e.g., 'Cary' or 'Valders') is used for a lithostratigraphic unit, an interval of time, and the ice advance that deposited it (Attig, personal communication, 1987).

The nomenclature of diachronic units includes the terms episode and phase, with phase being subordinate in the hierarchy to episode (NACSN, Articles 91-95). Geographic names previously used for "geochronologic" units may be used for diachronic units only if the geochronologic use has been formally abandoned (NACSN, 1983, p. 871).

GEOCHRONOLOGIC					DIACHRONIC			
Era	Period	Epoch	Age	Subdivision of age (10 <sup>3</sup> years ago)		Episode	Phase	
CENOZOIC	QUATERNARY	HOLOCENE				<div>WISCONSIN</div> <div>WISCONSIN</div> <div>SANGAMON</div> <div>INTERGLACIAL</div>	See figure 4b	
		PLEISTOCENE	WISCONSIN	10	10			late
			SANGAMONIAN	23	35			middle
				65	65			early
			ILLINOIAN	80	79			
				130	132			

Figure 4a. Time-stratigraphic terminology. The late Wisconsin spanned the time from 10,000 b. p. to 23,000 b. p. (Fulton and Prest, 1987) or to 35,000 b. p. (Richmond and Fullerton, 1986). Informal stratigraphic units frequently have differing interpretations. Modified from Fulton and Prest, 1987 and Richmond and Fullerton, 1986.

Thus, the time when the Lake Michigan Lobe advanced to deposit the Cary Moraine in Illinois is now properly called the Cary phase (as used by Hansel *et al.*, 1985). Of all the tills described by Thwaites (1943) and Thwaites and Bertrand (1957) as being of Cary age, only the Oak Creek Formation is now (informally) associated with the Cary phase. Willman and Frye (1970) formally abandoned the geochronologic use of "Cary". Figure 4b provides the diachronic terms associated with late Wisconsin-aged glacial events in eastern Wisconsin.

#### B. History of stratigraphic nomenclature in eastern Wisconsin

Previous authors have classified the late Wisconsin-aged glacial sediments in eastern Wisconsin into five formations. Table 2 synthesizes some of the stratigraphic nomenclature found in the literature predating *Pleistocene Lithostratigraphic Units in Wisconsin* (Mickelson *et al.*, 1984). Observations made during earlier investigations should not be discounted because the terminology used is not up-to-date. Figure 5 is intended to improve the transition from past terminology to the present names.

#### C. The late Wisconsin lithostratigraphic framework in eastern Wisconsin

##### 1. Introduction

The Zenda, Horicon, New Berlin, Oak Creek, and Kewaunee Formations include sediments of late Wisconsin age in eastern Wisconsin. They are heterogenous units containing a variety of ice-



GREEN BAY LOBE West Side	GREEN BAY LOBE East Side	LAKE MICHIGAN LOBE
<u>Kewaunee Fm.</u>	<u>Kewaunee Fm.</u>	<u>Kewaunee Fm.</u>
Middle Inlet M. (Late Athelstane phase)	Glenmore M. (Denmark phase)	Two Rivers M. (Two Rivers advance)
-----	-----	Two Creeks Forest Bed (Two Creeks retreat)
		Valders M. (Inner Port Huron advance)
Kirby Lake M. (Early Athelstane phase)	Chilton M.	Haven M. (Inner Port Huron advance)
Silver Cliff M. (Early Athelstane phase)	Branch River M.	Ozaukee M. (Outer Port Huron advance)
		<u>Oak Creek Fm.</u> (Cary advance)
<u>Horicon Fm.</u>	<u>Horicon Fm.</u>	<u>New Berlin Fm.</u>
Mapleview M. (Hancock phase)	Liberty Grove M.	<u>Zenda Fm.</u> Tiskilwa M.

Figure 4b. Lithostratigraphic framework of the study area with associated diachronic or event-stratigraphic phase names in parentheses. Phase names for the west side of the Green Bay Lobe are from Attig, Clayton, and Mickelson, 1985; these supercede phase names in McCartney, 1983. Phase names for the east side of the Green Bay Lobe have not been established except for McCartney's (1983) use of 'Denmark phase'. Phase names in the Lake Michigan Lobe are from Hansel et al., 1985 and are based on stratigraphic position and geomorphic evidence. At the time of writing, these have not been verified with field work in Wisconsin. McCartney and Mickelson (1982) correlated the Two Creeks Forest Bed across the Green Bay lobe.



deposited (till), water-deposited (lacustrine or fluvial), or air-deposited (aeolian) sediments. The tills within the formations are more easily distinguished--using lithic criteria as stipulated by the NACSN's code--than the lacustrine and fluvial sediments that in many places separate them. Very similar lacustrine and fluvial sediments may occur repeatedly within a given stratigraphic sequence because the glacial lobes advanced into proglacial lakes, deposited till, and ablated into pro- and post glacial lakes. Eventually, as the study of these sediments continues and more subsurface stratigraphy is mapped, geologists may define lithostratigraphic members composed primarily of lacustrine and fluvial sediments.

This report summarizes late Wisconsin geologic history for the Green Bay and Lake Michigan Lobes. As Boulton and Paul (1976) write, "It seems axiomatic that the geotechnical properties of sediments should be related to their source, their mode of transport, and their mode of deposition" (p. 159). Papers by Hansel *et al.* (1985), McCartney and Mickelson (1982), Acomb, Mickelson, and Evenson (1982), Schneider and Need (1985), and Attig, Clayton, and Mickelson (1985) give a more detailed review of the relevant geology and complete references. The following narration collects the main features of the literature into an overview so that the sediments at a particular site can be more easily anticipated.

## 2. Zenda Formation

Of the five late Wisconsin formations, the Zenda Formation is the oldest. The Harvard Sublobe of the Lake Michigan Lobe deposited the

Tiskilwa Member of the Zenda Formation between 18,000 to 20,000 years ago. This pinkish-tan sandy till is associated with the Wedron Formation and the Marengo moraine in Illinois (Mickelson *et al.*, 1984, p. A6-6), but it is mapped at the surface only in the extreme south-central portion of Walworth County in Wisconsin. It is present at least as far north as Milwaukee in the subsurface. No glacial sediments in the Green Bay Lobe have been formally correlated with the Zenda Formation; burial of the Zenda Formation by younger sediments complicates such correlation.

### 3. New Berlin Formation

The second-oldest late Wisconsin formations are the Horicon Formation, deposited by the Green Bay Lobe approximately 14,000 to 18,000 years ago, and the New Berlin Formation, deposited by the Delavan Sublobe of the Lake Michigan Lobe approximately 14,000 to 18,000 years ago. The Kettle Moraine was formed when the two ice lobes abutted against each other and discharged fluvial sand and gravel (outwash) over blocks of ice that later melted.

Two till units, one superposed on the other, can be recognized in the New Berlin Formation that outcrops in Lake Michigan shoreline bluffs, but these have not been mapped or traced in the subsurface individually. The New Berlin Formation has not been studied extensively or subdivided into formal lithostratigraphic members. Till in the formation has been described as gravelly sandy loam till of brown to yellowish brown color or gray color when unoxidized. Sand and gravel outwash underlies the till strata in the type and reference

sections. The formation has been mapped at the land surface behind the Darien Moraine and between the Kettle Moraine and the Valparaiso Moraine (Mickelson *et al.*, 1984, p. A7-3).

#### 4. Horicon Formation

The Horicon Formation includes three named lithostratigraphic members, the Mapleview, the Wayside, and the Liberty Grove Members. Till in the Horicon Formation have been described as brown to reddish-brown cobbly, pebbly, silty sand (Mapleview Member) and as light brown to yellowish brown pebbly sandy loam (Liberty Grove Member) (Mickelson *et al.*, 1984, p. A9-1). Each of these members was defined in the northernmost part of the Green Bay Lobe but the members have not been delimited. No lithostratigraphic members have been defined in the formation's southern extent. The moraines mapped by Alden (1918, Plates XXXVI and XXIII) indicate that separate till units may exist south of Lake Winnebago. The Hancock Moraine forms the Horicon Formation's western boundary (Attig, Clayton, and Mickelson, 1985). Prior to 1970, the Horicon Formation was known as drift of Cary age, or 'Cary drift'.

#### 5. Oak Creek Formation

Deposition of the Horicon Formation coincides with deposition of the Oak Creek Formation in the Lake Michigan Lobe 14,000 to 12,500 years ago (Mickelson *et al.*, 1984, p. A8-3). Members of the Oak Creek Formation have been informally called the "Valparaiso," "Tinley," and "Lake Border" (Rodenbeck *et al.*, 1987) and "2A, 2B, and 2C" (Mickelson *et al.*, 1984). These preliminary designations are based on

lithic characteristics and are associated with minor readvances of the retreating ("Cary advance" in Hansel *et al.*, 1985) ice that formed the Valparaíso, Tinley, and Lake Border Moraines. Tills in the Oak Creek Formation are silty because the ice overrode gray, silty lake sediments of Glacial Lake Milwaukee (Schneider and Need, 1985). In places, silty lake sediments separate the till units in the Oak Creek Formation.

Following deposition of the Oak Creek and Horicon Formations, both the Green Bay and Lake Michigan Lobes wasted back to the north beyond the Straits of Mackinac. Lake levels fell as the glacier retreated and Lake Superior, with its modern outlet blocked by ice, drained through a channel across the upper peninsula of Michigan and into the Lake Michigan Basin (Hansel *et al.*, 1985). This glacial retreat was temporary, and both lobes of the glacier again advanced down the Lake Michigan Basin and the Green Bay Lowland.

#### 6. Kewaunee Formation

This Early Port Huron advance incorporated the finer grained, red sediment that had been carried into these basins from iron-rich glacial sediments in the Lake Superior Basin (Murray, 1953). The Kewaunee Formation, described in a very general way as having red, clayey tills, includes ten lithostratigraphic members consisting primarily of till (figure 4b). McCartney and Mickelson (1982) use the Fox River as an arbitrary dividing line between the lithostratigraphic members on the east and west sides of the Green Bay Lobe; Kewaunee Formation tills on the east and west sides have distinct lithic

properties because the bedrock, which the glacier eroded as it advanced, outcrops in a pattern nearly parallel to the axis of the Green Bay Lobe. On the east side, ice of the Green Bay Lobe overrode the Maquoketa Formation of Ordovician age and dolomites of the Silurian System. On the west side, ice of the Green Bay Lobe eroded the Sinnippee, Ancell, and Prairie du Chien Groups of Ordovician age, Cambrian sandstones, and igneous rocks of the Middle Proterozoic Wolf River Batholith (Mudrey, Brown, and Greenberg, 1982).

The Ozaukee Member, stratigraphically the lowest Kewaunee Formation till in the Lake Michigan Basin, has been estimated as 12,900 years old (Mickelson *et al.*, 1984, p. A10-4). In the Green Bay Lobe, the lowermost Kewaunee Formation tills are included in the Silver Cliff Member on the west side and the Branch River Member on the east side. No radiocarbon dates are available and no member-to-member contacts have been observed, so the estimated age of greater than 12,200 years before present (b.p.) is by correlation of stratigraphic position and geomorphology (McCartney and Mickelson, 1982). The Silver Cliff Member is bounded by the Early Athelstane Moraine to the west (Attig, Clayton, and Mickelson, 1985). The Branch River Member has been assumed to extend as far south as Alden's (1918) "Outer Moraine of Red Drift."

After deposition of the first red tills, both lobes retreated at least as far north as Algoma (Acomb, Mickelson, and Evenson, 1982) before readvancing and depositing a second red till. In the Lake Michigan Lobe, the Haven Member overlies silty glacial Lake Chicago

sediments and/or the Ozaukee Member. In the Green Bay Lobe, ice deposited the tills of the Chilton and Kirby Lake Members of the east and west sides of the Fox River, respectively. Sediment from a proglacial lake, Early Lake Oshkosh (Thwaites and Bertrand, 1957), in places separates the first and second tills of the Kewaunee Formation in the Green Bay Lowland. A third till was deposited by the Lake Michigan Lobe, and is included in the Valders Member. The Valders and Chilton Members form an interlobate boundary west of the late Woodfordian interlobate moraine, the Kettle Moraine (McCartney and Mickelson, 1982).

Roughly 12,000 years ago, ice again withdrew north of the Lake Michigan Basin and lake levels fell below the modern level. Water again entered the Lake Michigan Basin from the Lake Superior Basin across the upper peninsula of Michigan, bringing more red, fine-grained sediments. The boreal Two Creeks Forest grew during the time of this low lake level only to be drowned by the rise to Calumet level and buried in Lake Chicago sediments (Hansel *et al.*, 1985). The next ice advance (11,800 to 11,200 years b. p.) flattened the forest and deposited the uppermost Kewaunee Formation members in the Green Bay Lowland and Lake Michigan Basin: the Middle Inlet, Glenmore, and Two Rivers Members. The southern extents of the Two Rivers Member, the Glenmore Member, and the Middle Inlet Member are marked by the Two Rivers, the Denmark, and the Late Athelstane moraines, respectively (Evenson and Mickelson, 1974; Attig, Clayton, and Mickelson, 1985).

Later Lake Oshkosh, at the margin of the Greatlakean-age ice in



the Green Bay Lowland, fell from an elevation of 829 feet. Apparently the ice margin was very jagged, and the lakes that formed at various elevations did not have sufficiently stable levels for mappable beaches to develop (Thwaites, 1943, p. 139). Lake levels fell from the time of Greatlakean ice retreat until the Nipissing I (4,500 b.p.) and later lake phases (Hansel *et al.*, 1985).

#### 7. Importance of the Pleistocene history and stratigraphy

An understanding of the geologic setting and the variability possible is necessary to understand the potential variability in geotechnical properties (May and Thomson, 1978, p. 362). The proglacial and postglacial ice marginal lakes described by Quigley (1980) in Ontario may be very similar to Thwaites' Early Lake Oshkosh and Lake Oconto. Quigley (1980) describes glaciolacustrine facies including ice-contact deltas, fluvial or turbidite sands and gravels or clays in ice-proximal areas to thick, massive clays in distal regions (p. 266). Since Thwaites' mapping, additional buried beaches have been discovered in the area glaciated by the Green Bay Lobe (Gordon and Huebner, 1984).

### III. Study methods

#### A. Application of lithostratigraphy

My interpretation and analysis of geotechnical data is based on the lithostratigraphic framework described in the preceding section. I associated the geotechnical and hydrogeologic properties compiled from geotechnical reports with the defined lithostratigraphic units. I interpreted the stratigraphy of the individual sites using stratigraphic investigations conducted at a reconnaissance level (McCartney, 1979; Need, 1985; Acomb, 1978) in conjunction with stratigraphic interpretation and geologic mapping of Wisconsin's Lake Michigan bluffs (Mickelson *et al.*, 1977). Detailed geologic mapping has not been attempted over most of the area glaciated by the Green Bay and Lake Michigan Lobes in late Wisconsin time; recent reports on Brown County (Need, 1985), Florence County (Clayton, 1986), and Portage County (Clayton, 1986) are notable exceptions.

One convention established by Mickelson *et al.* (1984) is to associate facies other than till with a named lithostratigraphic member. For example, "the Valdres Member contains basal glacial till deposited by ice of the Lake Michigan Lobe and associated fluvial and lacustrine deposits" (p. A10-8). To be included in one lithostratigraphic member, all of the facies must be clearly lithologically associated with each of the others (Mickelson *et al.*, 1984, p. 3).

The boring logs that I used were not always written by geologists and frequently did not include the lithic criteria (e.g., mineralogy) necessary to distinguish one fluvial or lacustrine sediment from another. I made three assumptions: Mickelson *et al.*'s (1984) descriptions of tills in lithostratigraphic members are 1) accurate, 2) complete, and 3) the extent of the stratigraphic units is closely approximated by figure 6. Then I expected to find the mapped unit from the land surface to variable depths, underlain by a possibly discontinuous fluvial and/or a lacustrine layer of sediment, in turn underlain by the next lower lithostratigraphic member (including a till) in the stratigraphic section, and so forth. To some extent, my expectations were based on glacio-depositional models like those in Clayton and Moran (1974) and Boulton and Paul (1976), but consideration of local constraints (e.g., mapped distribution, topography) and my observations of modern glacial processes in Alaska influenced my interpretation more than the generic models. The buried glacial geomorphology produced by repeated ice advances (White, 1974) and other disruptions of bedding, such as involutions (Mickelson and Evenson, 1974) and glaciotectionic structures (Moran, 1971) frequently complicated stratigraphic interpretation.

#### B. USDA Soil Conservation Service county reports

I did not find published Soil Conservation Service reports consistently helpful for distinguishing lithostratigraphic members within a formation. The Soil Conservation Service map units are

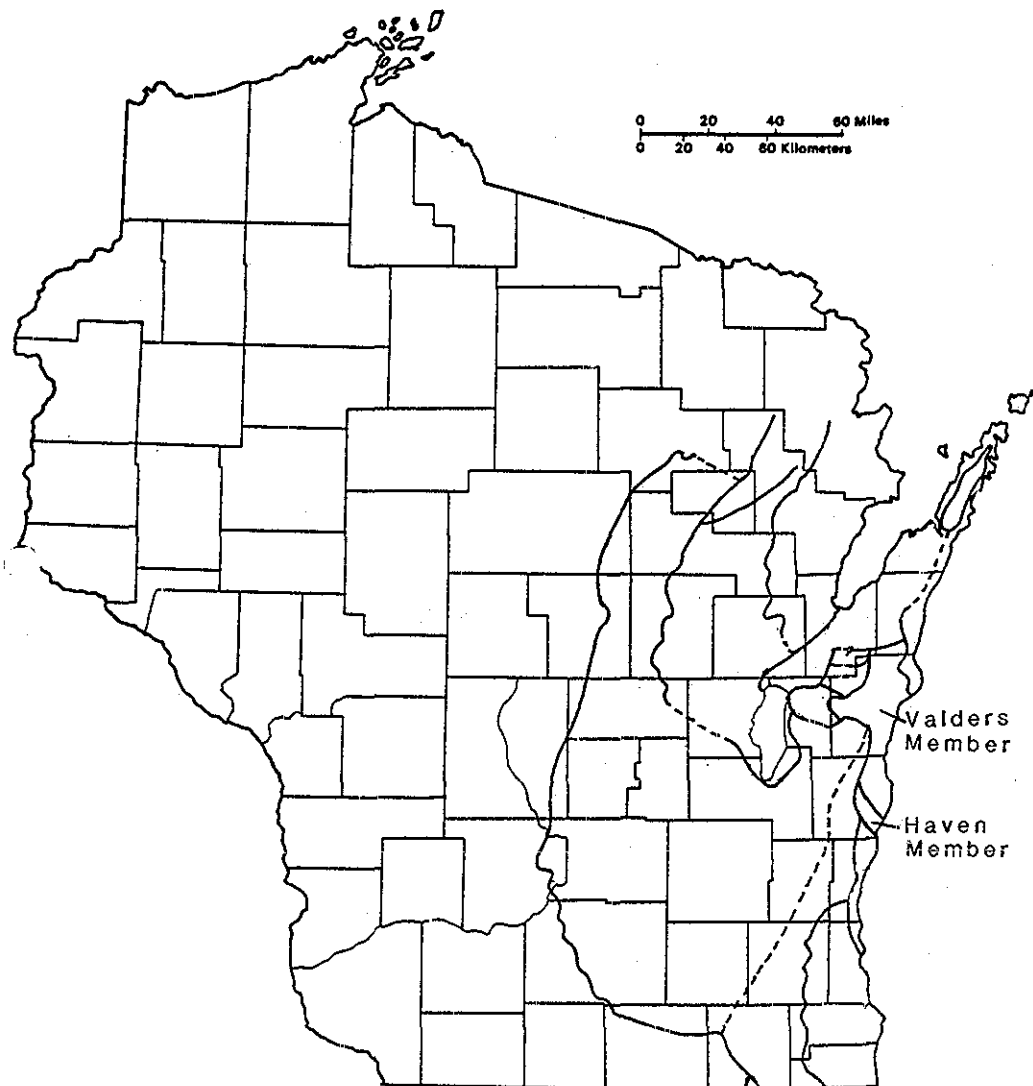


Figure 6. Surface distribution of named lithostratigraphic units of late Wisconsin age. (From Mickelson et al., 1984.) This map differs from Plate 1 by showing surface distribution of the Haven Member farther south than the Valders Member.

influenced by climate, living organisms, relief, parent material, and time. In other words, the factor pertinent to this study is combined with other factors in the determination of soils mapping units. As a result, the same soils mapping units may form on different lithostratigraphic members.

C. Geotechnical reports submitted in accord with Administrative Code

1. The influence of Wisconsin Administrative Code

The quality and quantity of data suitable for this study is strongly affected by the legal requirements for geotechnical information in the Wisconsin Administrative Code. Some reports of geotechnical investigations for proposed landfills prior to 1980 exceeded the minimum data requirements of Chapters NR 51 (1969) and NR 151 (1971). These early codes required investigations to a depth of only 10 feet below proposed base grade (revised to 15 feet) and did not stipulate a minimum number of borings or specific tests until a 1976 revision. NR 180 (1980) requires a minimum number of borings per area with descriptive boring logs, grain size analyses, permeability tests, and raw data in appendices. Data from geotechnical investigations prior to 1980 were included in the database of this report if the data resulted from standard engineering practices commensurable with those of post-1980 investigations. The availability and quantity of geotechnical information is expected to improve with the promulgation of NR 510 and NR 512; these will replace

NR 180.13 (5) and NR 180.13 (6), respectively. Excerpts from the Wisconsin Administrative Codes dealing with geotechnical investigations for landfills are included in an appendix to this report, "Data required by Wisconsin Administrative Code."

## 2. Compilation of information required by NR 180

### i. Method of compiling data

Compilation of data submitted by consulting firms in individual reports and correspondence required considerable effort. A single site might have ten reports of geotechnical investigations by different consulting firms, each with a slightly different style of data presentation. The amount of suitable data varied with individual histories of site development and expansion. I compiled the data by hand and supervised its entry to a microcomputer spreadsheet.

### ii. Quality and selection of data compiled

Early in the project, several individuals suggested that I eliminate reports by firms with reputations for poor quality work. I did not eliminate any firm's data because the apparent quality of all the reports varied with time, personnel, and circumstances. Moreover, I could not always distinguish between poor quality investigations and written reports of poor quality. Some "wild" data were "eliminated" by the resistant statistical techniques used; these techniques are described later in this report.

The emphasis in this report is on assessment of *in-situ* characteristics of stratigraphic units. For this reason, I did not

compile lab hydraulic conductivities for samples identified as recompacted. I carefully reviewed field hydraulic conductivities and well construction diagrams, then recorded field hydraulic conductivities. If the well screen intersected two materials, I assigned codes indicating that two materials (facies) were present within the saturated interval tested. Hydraulic conductivities for multiple facies are not included in comparisons of tills in lithostratigraphic members.

D. Associating data with a lithostratigraphic unit.

Several difficulties complicated the process of associating geotechnical data with Pleistocene lithostratigraphy. These difficulties include: 1) the confusing and complex stratigraphic nomenclature, 2) the difference in approaches taken by geologists and engineers, 3) distinction of till from other sediment facies, 4) identification of till units, 5) "incompatible" scales and maps. Despite these problems, Pleistocene lithostratigraphy provides a reasonable framework for data organization. Resolution of these problems is described below.

1. Stratigraphic nomenclature

As demonstrated in part II, the late Wisconsin stratigraphic names are numerous and confusing. Using the most detailed information available requires knowledge of the variety of names and what the materials have most recently been called. Associating the engineering information with glacial lithostratigraphic units requires familiarity

with the units both in the literature and in the field. I visited type or reference sections to obtain a better understanding of the literature.

## 2. The different approaches taken by engineers and geologists

It seemed as though the information in the boring logs was collected for a purpose other than definition of soil, bedrock, and groundwater conditions (hydrogeology) at the site. This is due to the difference in professional orientation between geotechnical engineers and geologists. Although Terzaghi, the father of soil mechanics, emphasized the effects of sedimentation, erosion, weathering, jointing, and groundwater flow (Dixon, 1974, p. 234), the boring logs produced by geotechnical consulting firms that are included in initial site reports and feasibility reports seem to emphasize the soil mechanics approximations of strength. To a large extent, this is a matter of presentation. Hydrogeologists prefer to see all test results and geologic interpretation on a boring log. A geotechnical consulting firm, on the other hand, may wish to present boring logs completed by a subcontractor separately (in an appendix) from the geologic interpretation (which is usually in the text).

## 3. Distinction of till from other sedimentary facies

Most geologists who study Quaternary materials rely on field and laboratory evidence to determine whether a sediment is till or sediment of a different facies. Dreimanis (1976) lists five criteria commonly emphasized in the identification of till:

". . . (1) glacial origin; (2) presence of a variety of rock and mineral fragments of various sizes, many of them having been



transported considerable distances; (3) poor sorting, in the geologic meaning of this term, that is: presence of a wide range of particle sizes, usually with bi-modal or multi-modal distribution; (4) lack of stratification, although some tills are foliated, or even truly bedded; (5) compactness or close packing, also with certain exceptions" (p. 14).

Even with good field exposures, the interpretation is open to professional dispute, largely because of the varying definitions of till (see Dreimanis, 1976). The techniques used by geologists to distinguish individual till units have varied to accommodate the lithostratigraphy being studied, and the criteria pertinent to this study have been summarized in table 1. (Other techniques may be found in Raukas, Mickelson, and Dreimanis, 1978.) Within each of the Kewaunee Formation members, I relied on grain size analysis and sorting to determine whether a material was till (poorly sorted), or lacustrine or fluvial (well sorted). Distinguishing till from outwash in the very sandy Horicon Formation was nearly impossible if a complete grain size analysis was not available (i.e., if the grain size analysis was completed only to P200, 0.075 mm). If the genesis of a sediment could not be determined from the information available, it was coded as unknown.

#### 4. Identification of lithostratigraphic units

Distinction of tills in members of the Kewaunee Formation presents another difficulty because the tills have similar provenance. Distinctions between lithostratigraphic members of the Kewaunee Formation were made on the basis of description (including qualitative color changes noted on the log and grain size analysis), mapped location, and stratigraphic sequence. If sediments clearly belonged

within a formation, but could not be confidently identified at the member level, no member code was entered. If not even the formation could be identified, or if the sediment did not fit within a formation's defined range of lithic characteristics, a code of UN for unknown/unnamed was assigned. The sites with sediments that did not fit the expected lithostratigraphic framework are useful for identification of areas requiring further geologic study. Some excellent logs included observations on mineralogy, depth of leaching, or fabric and structure of the samples that were very helpful.

##### 5. "Incompatible" maps and scales

The next difficulty in assigning data to a lithostratigraphic unit has to do with scale. Little detailed mapping of late Wisconsin glacial sediments has been completed in the Green Bay and Lake Michigan Lobes. Thesis (McCartney, 1979) and journal illustrations and two 1:1,000,000 maps of Quaternary sediments and glacial landforms (Lineback *et al.*, 1983; Farrand *et al.*, 1984) were used to determine a preliminary, theoretical stratigraphic section at a site.

Incompatible map bases (lack of common political and hydrographic features or coordinate systems) complicated map-to-map comparisons. The geotechnical boring locations are plotted at a relatively large scale for submittal, on the order of 1 inch equals 200 feet. These boring locations were transferred to 7 1/2 minute topographic quadrangle maps so that the boring locations could be seen in a more regional geomorphic context.

#### E. The spreadsheet

Data from handwritten summary sheets were entered to a microcomputer spreadsheet for ease of manipulation. Table 2 gives the spreadsheet headings and subheadings used, and table 3 lists the codes. The spreadsheet allowed relatively easy sorting and combining of data into files of single parameters, such as lab or field hydraulic conductivity, or single lithostratigraphic units.

#### F. Spatial locations

The data collected for this study have been assigned spatial locations so that the data are suitable for entry to a geographic information system and may be combined with data from other sources. Reconciliation of the spatial location of all data points to a single system provided a difficult problem in the assembly of a large database from diverse sources. Engineering site plans usually record precise spatial locations, but these locations are frequently tied to arbitrary bench marks. In fact, the current administrative code, NR 180, requires site specific grid coordinates and the use of local benchmarks. Although this does not preclude use of a real space coordinate system such as universal transverse mercator, latitude and longitude, or public land survey system (township and range) coordinates for each borehole, none of the submitted reports included coordinates of these types for each boring.

Geological investigations typically use information plotted on 15- or 7 1/2-minute topographic quadrangles. For this study, latitude

Identity:	County Year sampled Lithostratigraphic unit Geologic genesis
Location:	Latitude (degrees, minutes, seconds) Longitude (degrees, minutes, seconds) Boring number Land surface elevation (feet above MSL) Top of interval sampled (depth in feet) Bottom of interval sampled (depth in feet)
Hydraulic conductivity:	Lab K (cm/s) Lab K method of test Field K (cm/s) Field K method of test
Grainsize percentages:	Percent of bulk > 2 mm Sand percentage of matrix (< 2 mm) Silt percentage of matrix (< 2 mm) Clay percentage of matrix (< 2 mm)
Engineering properties:	USCS group symbols P200 (%) Dry unit weight (pcf) SPT N (blows/foot) Natural moisture (% of dry weight) Liquid limit (%) Plastic index (%) Pocket penetrometer measurement (tsf)

Table 2. Categories of data recorded using the spreadsheet. 'K' symbolizes hydraulic conductivity. 'P200' means the percent passing the #200 sieve. 'SPT N' abbreviates standard penetration test blow counts.

<u>Counties</u>		<u>Lithostratigraphic Units</u>	
Brown	BN	Middle Inlet M.	mi
Calumet	CA	Ozaukee M.	oz
Dane	DN	Silver Cliff M.	si
Dodge	DG	Two Rivers M.	tr
Door	DR	Valders M.	va
Fond du Lac	FL		
Green Lake	GL	Oak Creek Fm.	OC
Kenosha	KE		
Kewaunee	KW	Horicon Fm.	HO
Manitowoc	MN	Mapleview M.	ma
Marinette	MT	Liberty Grove M.	lg
Marquette	MQ		
Milwaukee	ML	New Berlin Fm.	NB
Oconto	OC		
Outagamie	OU	Zenda Fm.	ZE
Ozaukee	OZ	Tiskilwa M.	ti
Racine	RA		
Sauk	SK	Unnamed units	UN
Shawano	SH		
Sheboygan	SB		
Walworth	WW		
Washington	WN		
Waupaca	WP		
Winnebago	WI		
<u>Test methods</u>		<u>Materials and genesis</u>	
<u>for hydraulic conductivity</u>		Till (all varieties)	3
lab constant head (vert)	1	Outwash (sand & gravel)	4
lab constant head (hor)	2	Lacustrine (sand, silt	
lab falling head (vert)	3	and/or clay)	5
lab falling head (hor)	4	Loess	6
lab backpressure or		Modern alluvium	7
consolidometer (vert)	5	Rock	12
lab backpressure or		Organic	13
consolidometer (hor)	6	Undifferentiated	99
field rising head	7		
field falling head	8		
pumping test	9		
other	10		

Table 3. Codes used to identify spreadsheet data. Although codes for lithostratigraphic members appear in only lower case here, they may appear in upper or lower case in the appendices.

and longitude coordinates were chosen because these coordinates lend themselves to easy conversion to map projections such as universal transverse mercator, and they follow simple rules like increasing to the north and west. The seconds of latitude and longitude usually provide an adequate resolution of borehole locations' relative positions at individual landfill sites. Use of latitude and longitude avoids problems associated with the use of township and range such as irregular section shapes that resulted from influences of the original system of surveying.

Elevations must be reported relative to USGS datum according to Wisconsin Administrative Code (NR 180.13(6)). The datum was often missing from the documents predating the existing code. Although reports have improved in this respect, lack of datum elevations continues to be a problem.

#### G. Choice of analytical tool

Associating groups of material properties with mapped lithostratigraphic units in Wisconsin is a principal goal of this study. All the material properties recorded vary in three dimensions. Measurement error is associated with each observation of each parameter. The lack of control over how samples were chosen for testing controls the choice of data analysis tools. Many of our sample sizes are small and lack Gaussian distributions; resistant and robust exploratory statistical methods are necessary for confidence in study results. In order to assess the validity of statistical

assumptions that the sample is random, that it has a normal (Gaussian) distribution, and that all of the populations have equal variances, I used Minitab (Release 5.1.1, Minitab, Inc., 1986) statistical software.

Within each unit I constructed histograms of both field and lab  $\log_{10}$  hydraulic conductivities, P200 values, plastic and liquid limits, plastic index, pocket penetrometer measurements, and dry unit weights for each site. According to Ryan, Joiner, and Ryan (1985), "Observations taken in close proximity, either in time or in space, often are correlated. Observations that are correlated do not form a simple random sample" (p. 175). In some cases there were clear patterns from site to site within a single till unit; thus, the sample is not random. However, in most cases, no clear pattern was apparent and a random sample was assumed.

I used several methods to determine whether the data are normally distributed. These methods include comparison of median and mean, normal probability plots (Ryan, Joiner, and Ryan, p. 177), and visual assessment of histograms. Liquid limit, plastic limit, and dry unit weights typically have Gaussian or approximately Gaussian distributions. Values of P200,  $\log_{10}$  hydraulic conductivities, and pocket penetrometer measurements are not always Gaussian.

The assumption of equal variances between populations is important when choosing an analysis of variance (ANOVA) technique. Some of the samples are small ( $15 > n > 5$ ), leading to relatively large standard deviations about the mean; when sample sizes are small

and have unequal variances, use of an ANOVA technique incorporating pooled standard deviations leads to an undesirable Type I error.

Previous workers have described the statistical distribution of hydraulic conductivity data. Freeze and Cherry (1979, p. 31) and Neumann (1983, p. 83), among others, indicate that hydraulic conductivity follows a log-normal distribution. The hydraulic conductivities included here more closely resemble a Gaussian distribution after a base 10 power transformation. But the medians and the means of the hydraulic conductivity data still do not always equal each other; some histograms show a skewed distribution. In addition to the non-Gaussian distribution, the small sample sizes (fewer than 15 values) restrict the use of standard parametric statistical tests. Nonparametric techniques have the advantage of being resistant to the influence of a few outlying data points. In most cases, I used the Kruskal-Wallis test, ". . . a generalization of the Wilcoxon two-sample test to the case of  $k > 2$  samples . . . the test is an alternative nonparametric procedure to the F test for testing the equality of means . . ." (p. 495, Walpole and Myers). The Kruskal-Wallis test assumes that the data form continuous distributions all having the same shape. The hypotheses are:

$H_0$ :  $k$  independent samples are from identical populations;

$H_1$ : there is at least one difference among the  $k$  independent samples.

If the test statistic  $h$  falls in the critical region  $H > X^2$ ,  $H_0$  may be



rejected at a level of significance determined from a statistical table. Otherwise,  $H_1$  is rejected (Walpole and Myers, p. 496).

A nonparametric statistical technique--the boxplot--is well-suited for graphical analysis of data. A box and whisker plot gives more information than a histogram, but requires a minimum of 5 values. Figure 7 shows a median, the fourthspread (box), outerfourth ranges (whiskers), outliers, and the approximate 95% confidence interval (parentheses). The parentheses indicate the confidence interval of the median and are much more sensitive to changes in the data than the box. Batches (the exploratory data analysis equivalent of samples) of data may be compared using the values of the median, the fourth spread, the location of the median with respect to the fourths, whisker length, and outlying data points. Up to 25% of the data in each batch can be "wild" without greatly affecting the features of the box (Emerson and Strenio, 1983).

The methods just described are used to assess the variability and expected range of values for properties of tills within lithostratigraphic units. Other methods are appropriate for investigation of the underlying relationships among data compiled. If the compiled data are from a carefully designed experiment, inferences can be made from straight-line fits. The conditions for statistical inference follow.

- "1. In the underlying population, the relationship between  $x$  and  $y$  should be a straight line...."
- "2. For each  $x$ , the amount of variation in the population of  $y$ s in the population should be approximately the same...."

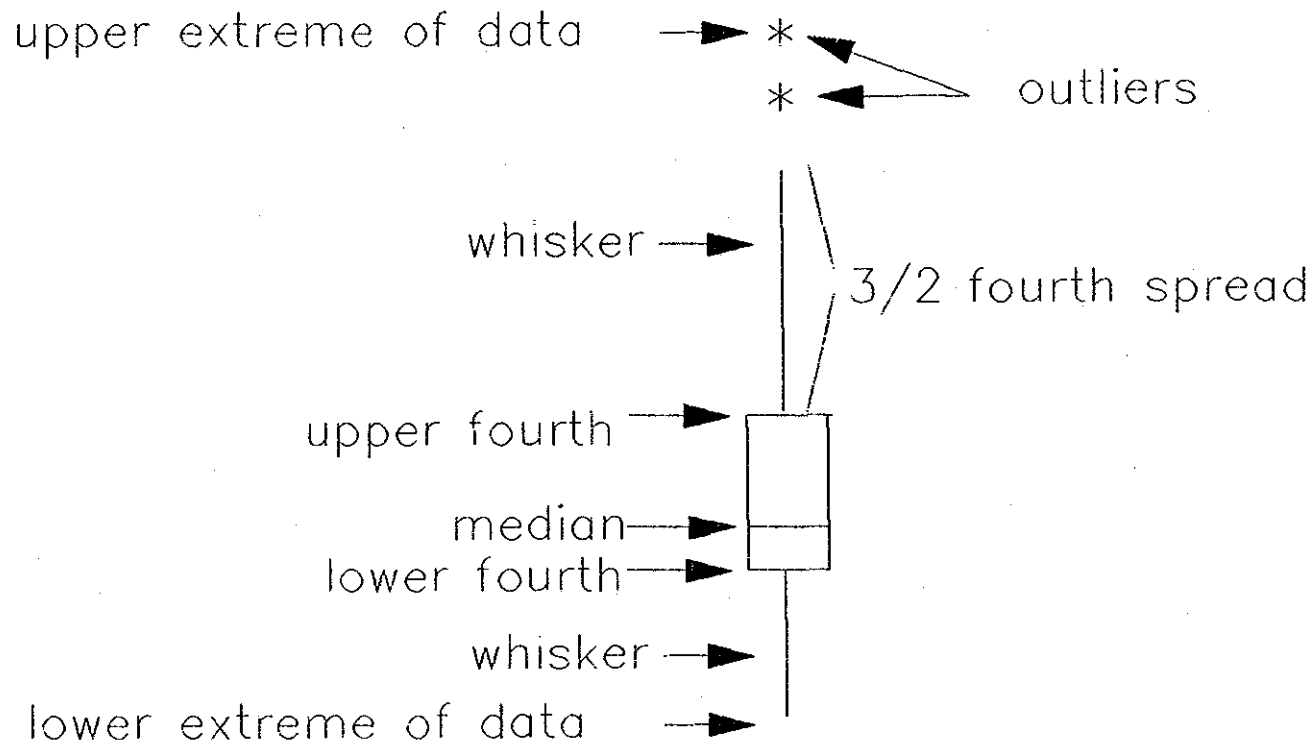


Figure 7. Features of the boxplot. This boxplot was drawn at an arbitrary scale. The fourth spread is the distance (or range of values) between the upper and lower fourths. Whiskers are drawn out to the data value most remote from the median within a distance evaluated as  $(3/2 * \text{fourth spread})$ . Confidence limits for the median may be added in the form of parentheses. See Hoaglin, Mosteller, and Tukey for a discussion of exploratory data analysis terminology (1983, pp. 1-6).

"3. For each  $x$ , the distribution of  $y$ s in the population should be approximately normal...."

"4. The  $y$ s that actually are obtained should be approximately independent..." (Ryan, Joiner, and Ryan, p. 230).

Frequently, only one type of data was available for a specific sample. The data compiled in this project were not always paired, and medians are used to represent individual till units. Thus, few inferences may be confidently made. Correlation and regression are used in this study to determine which tests are useful for hydrogeologic interpretation and to make recommendations for future investigations.

#### IV. Presentation of Data

##### A. Variation within tills of lithostratigraphic units

Data for materials other than till are not discussed here because the extent of these materials is not known. However, values of hydraulic conductivity for Pleistocene sand and gravel outwash in eastern Wisconsin are typically within an order of magnitude of  $10^{-3}$  cm/s. Values of hydraulic conductivity measured in the field for silty lacustrine sediments are typically about  $10^{-5}$  cm/s while rhythmites of silt and clay (commonly referred to as 'varved' lacustrine sediments) have lower values of hydraulic conductivity. Site-specific data for all materials at each site were included in appendices.

The following discussion of the variability of till units assumes that the stratigraphic and geologic interpretations are correct. Histograms of  $\log_{10}$  values of hydraulic conductivity measured in the field and in the laboratory were plotted for the till(s) of each lithostratigraphic unit. Matrix percentages of sand, silt, and clay are plotted in textural triangles. Plasticity charts illustrate the range in liquid limit and plastic index. Pocket penetrometer and dry unit weight data are not discussed until section IV B unless sufficient data were available for an analysis of variance test (ANOVA). The standard penetration test, USCS group symbols, plastic limits, and other indices derived from Atterberg limits will be presented only for discussion in part V.

Within some tills, no quantitative comparison of data may be made for one of two reasons: 1) insufficient data are available at each site for statistical analysis, or 2) data were collected for only one site. Data points are coded by site within each of the four diagrams for each unit. Refer to Plate 1 for the location of sites. County names and section, township, and range numbers are provided for the sites in an appendix. The site numbers are consistent throughout text, illustrations, and appendices.

#### 1. Kewaunee Formation

Figures 8a through 8h illustrate the hydraulic conductivities, grain size analyses, and plasticity charts for the tills in members of the Kewaunee Formation. Due to the geographic distribution of both the landfills and the Branch River Member, no data for the Branch River Member were recorded. Although some data for the Silver Cliff Member may have been recorded, I could not differentiate it from other Kewaunee Formation sediments.

##### a. Hydraulic conductivities measured in the field

In the Middle Inlet (figure 8a) and Kirby Lake (figure 8b) Members on the west side of the Green Bay Lobe, field hydraulic conductivities have the widest range, varying over four orders of magnitude. Tills in other members may have an equal range, but data are too sparse to show it. Sufficient samples for the Kruskal-Wallis test were available in both the Kirby Lake and Glenmore Members (figure 8c). In the Glenmore Member, I rejected the null hypothesis that two independent samples, sites 1 and 10 (figure 8c), are from

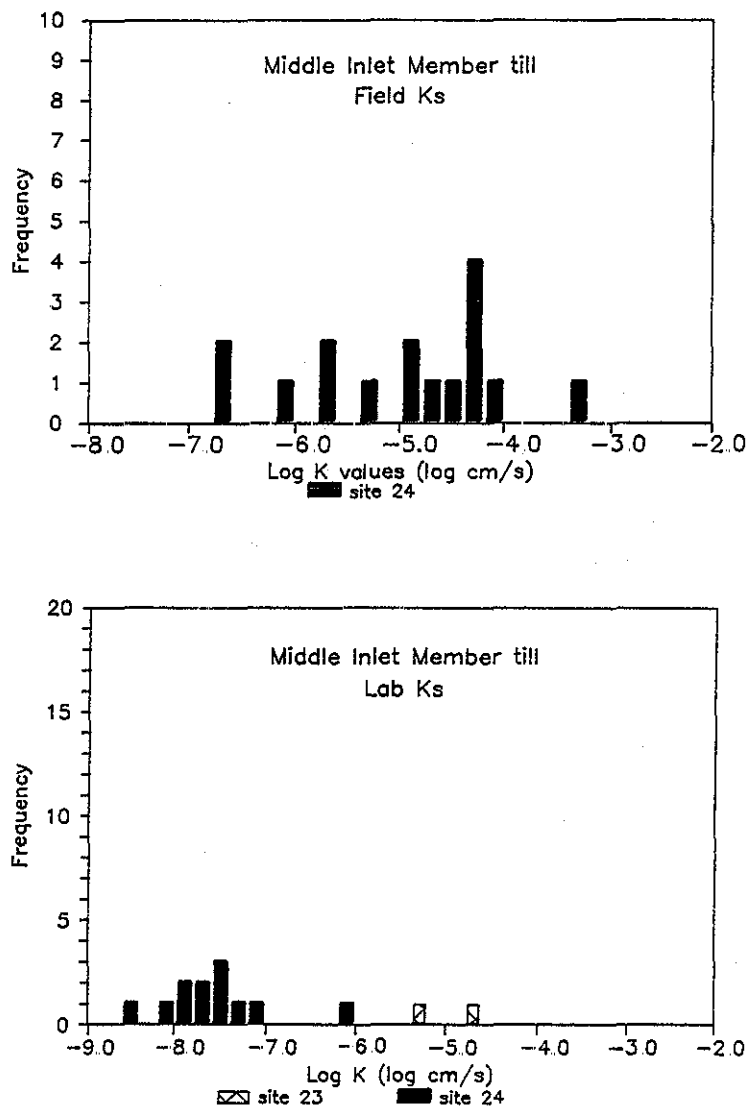


Figure 8a. Data for till in the Middle Inlet Member of the Kewaunee Formation. Field K means hydraulic conductivity measured in the field. Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.

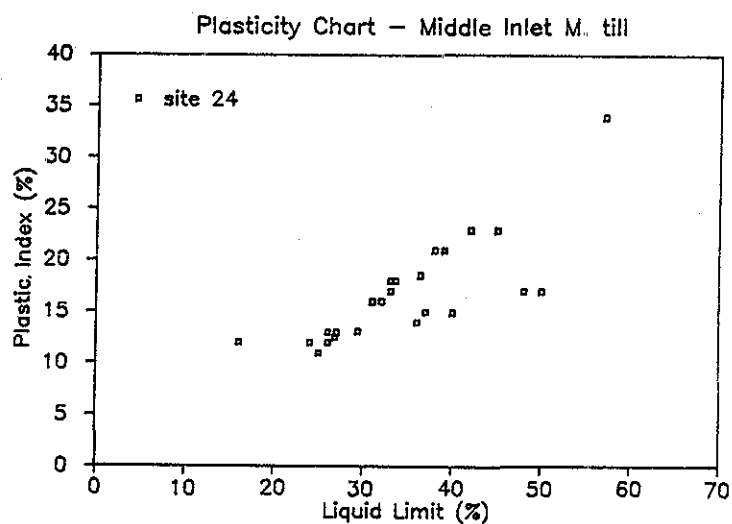
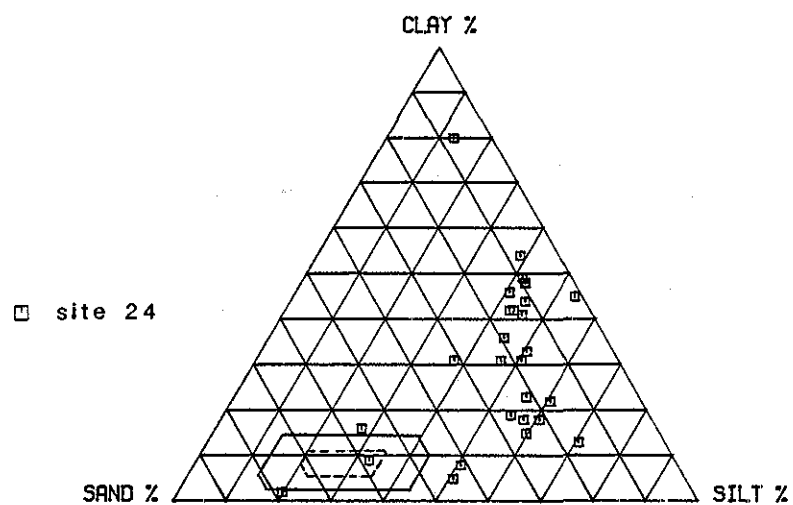


Figure 8a, cont. Data for till in the Middle Inlet Member of the Kewaunee Formation. Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the source.

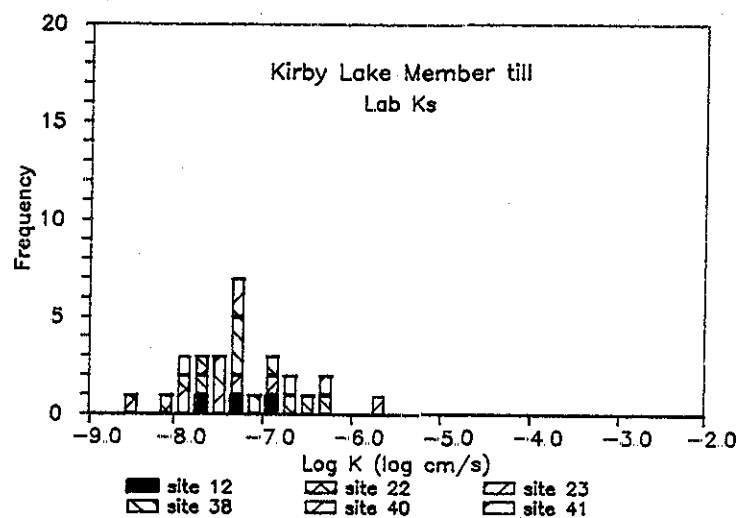
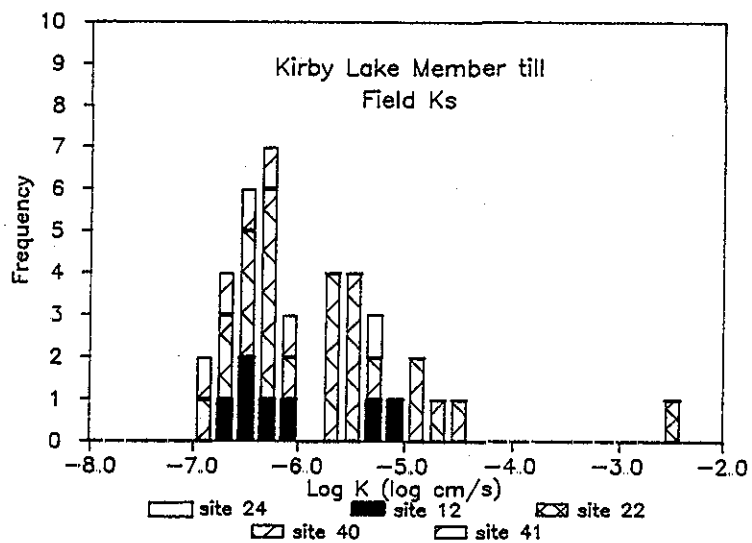


Figure 8b. Data for till in the Kirby Lake Member of the Kewaunee Formation. Field K means hydraulic conductivity measured in the field. Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.



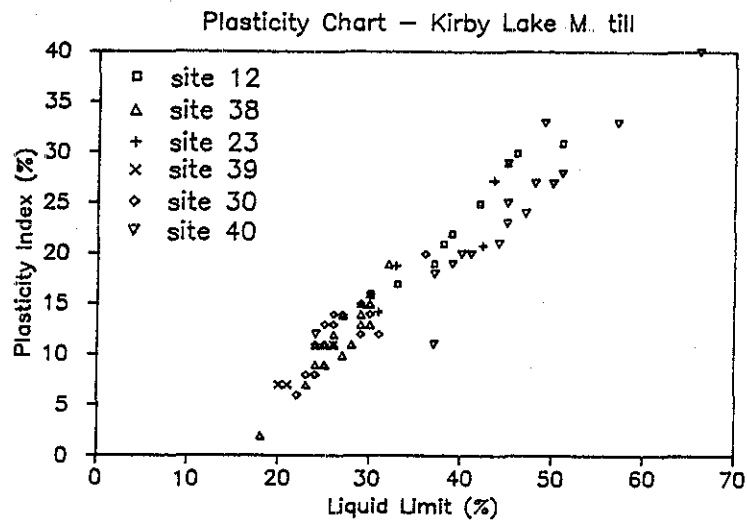
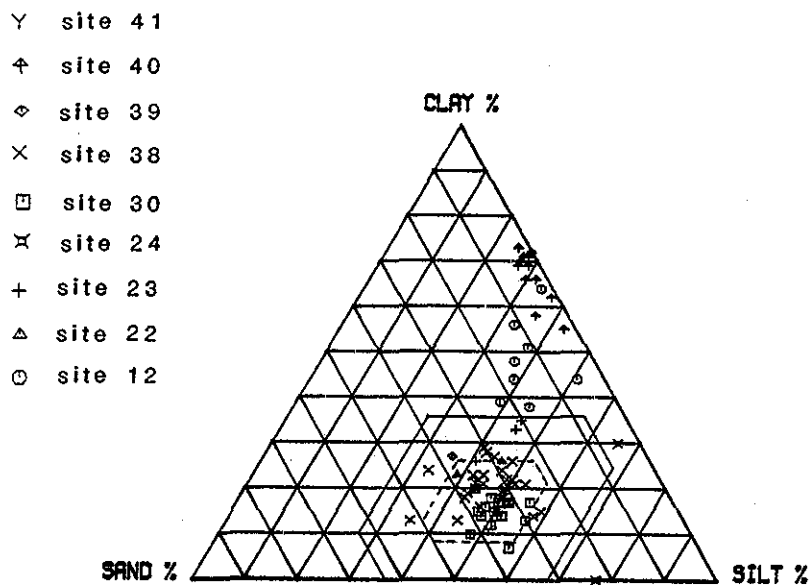


Figure 8b, cont. Data for till in the Kirby Lake Member of the Kewaunee Formation. Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the source.

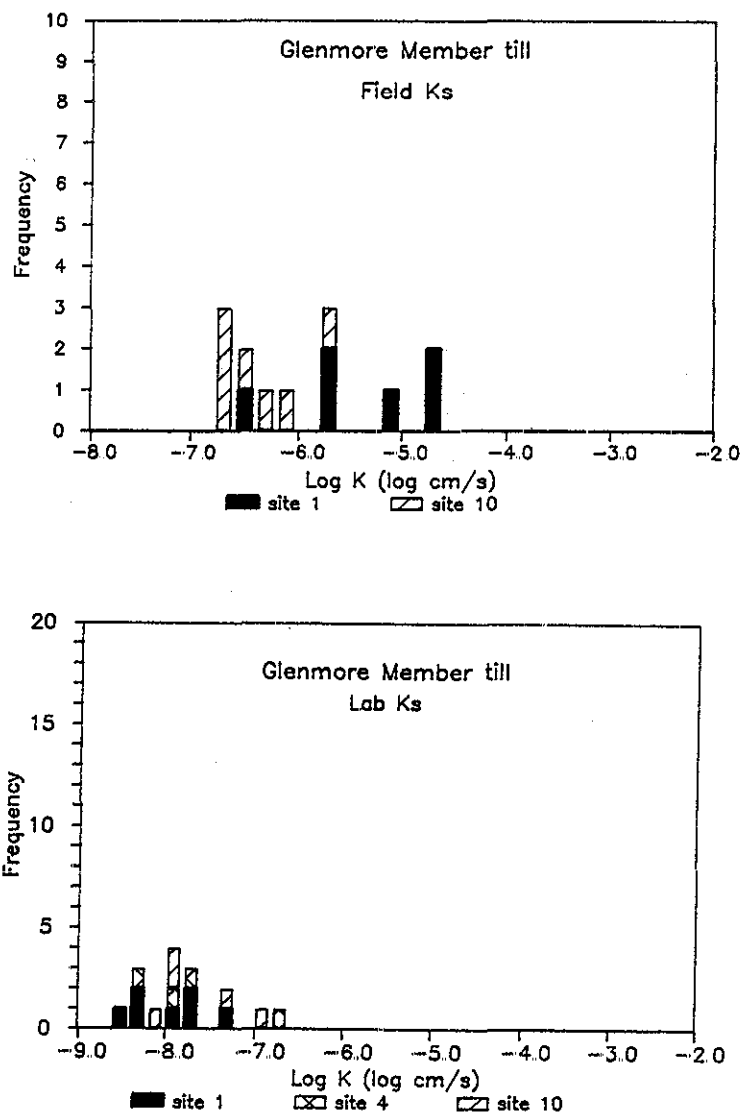


Figure 8c. Data for till in the Glenmore Member of the Keweenaw Formation. Field K means hydraulic conductivity measured in the field. Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.

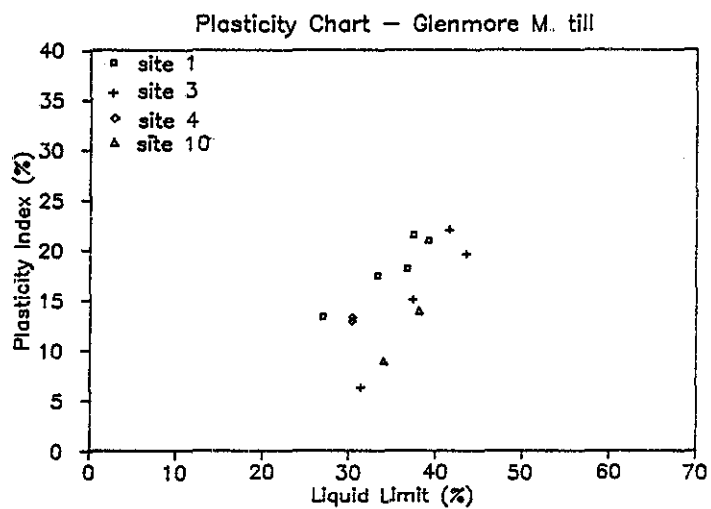
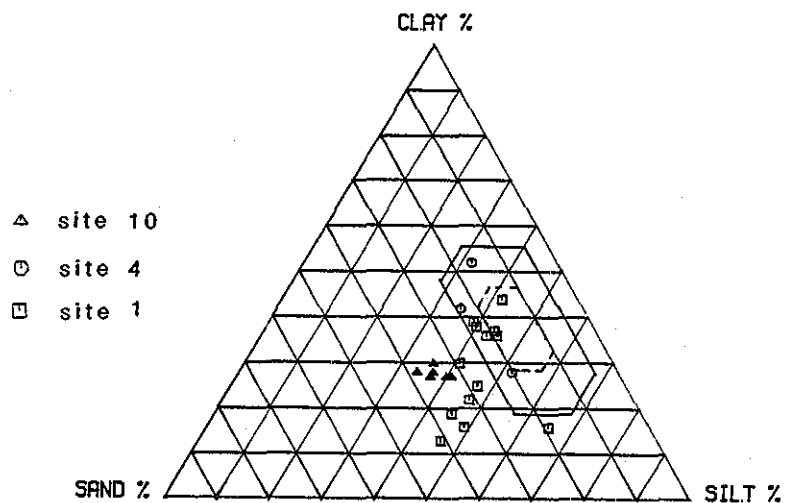


Figure 8c, cont. Data for till in the Glenmore Member of the Kewaunee Formation. Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the source.

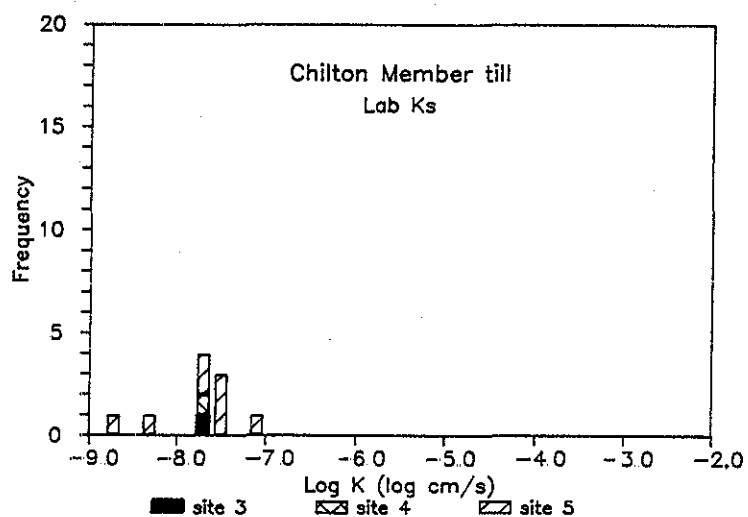
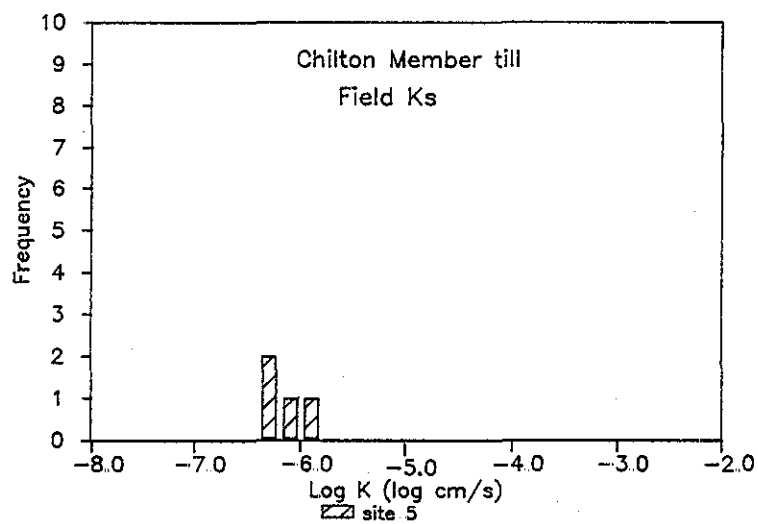


Figure 8d. Data for till in the Chilton Member of the Kewaunee Formation. Field K means hydraulic conductivity measured in the field. Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.

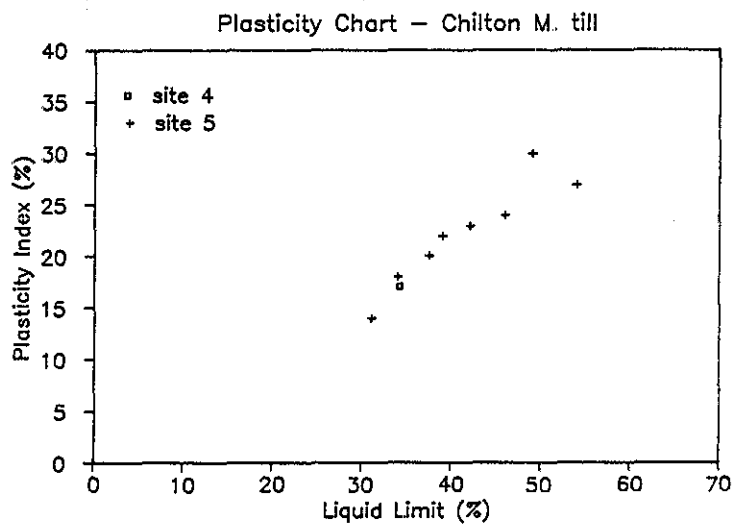
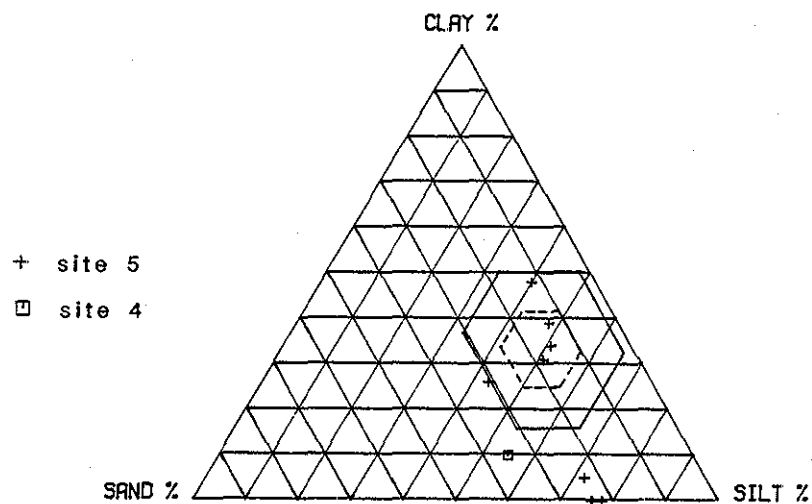


Figure 8d, cont. Data for till in the Chilton Member of the Kewaunee Formation. Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the site.

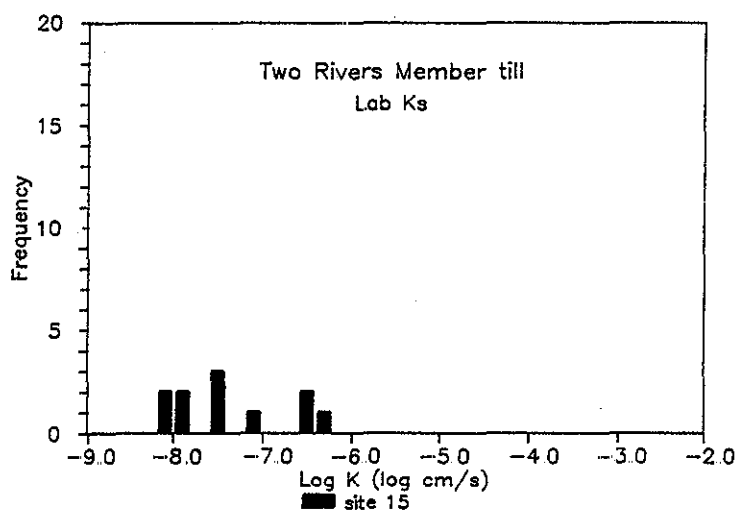


Figure 8e. Data for till in the Two Rivers Member of the Kewaunee Formation. No values of hydraulic conductivity measured in the field were compiled. Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.

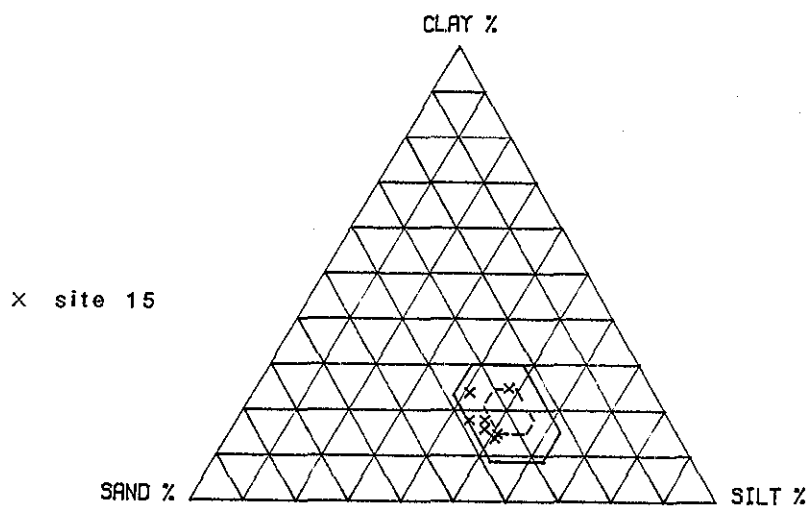


Figure 8e, cont. Data for till in the Two Rivers Member of the Kewaunee Formation. Sand, silt, and clay percentages are for the less than 2 mm fraction. No Atterberg limit data were compiled. Data are plotted with a symbol indicating the source.

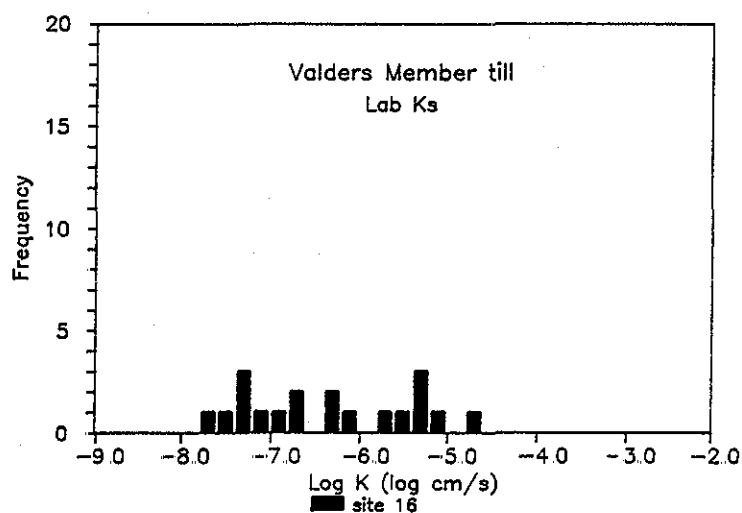


Figure 8f. Data for till in the Valders Member of the Kewaunee Formation. No values of hydraulic conductivity measured in the field were compiled. Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.



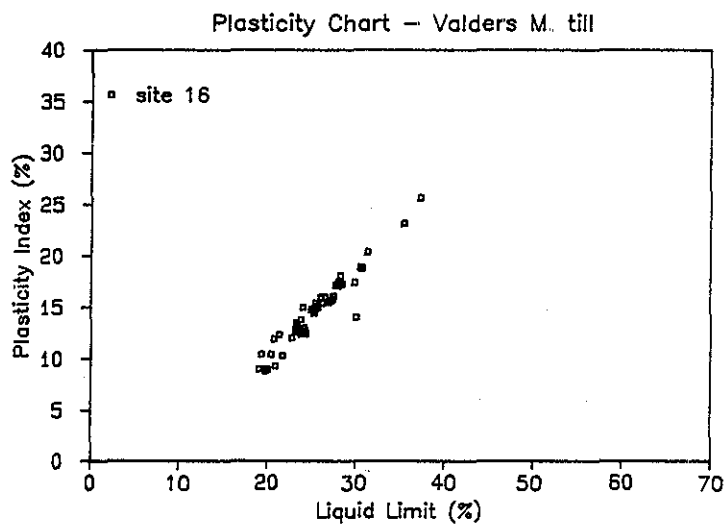
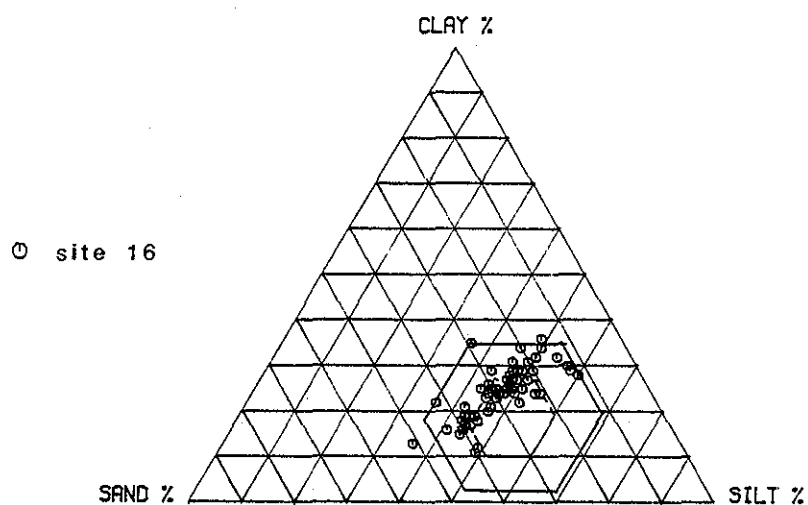


Figure 8f, cont. Data for till in the Valders Member of the Kewaunee Formation. Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the source.

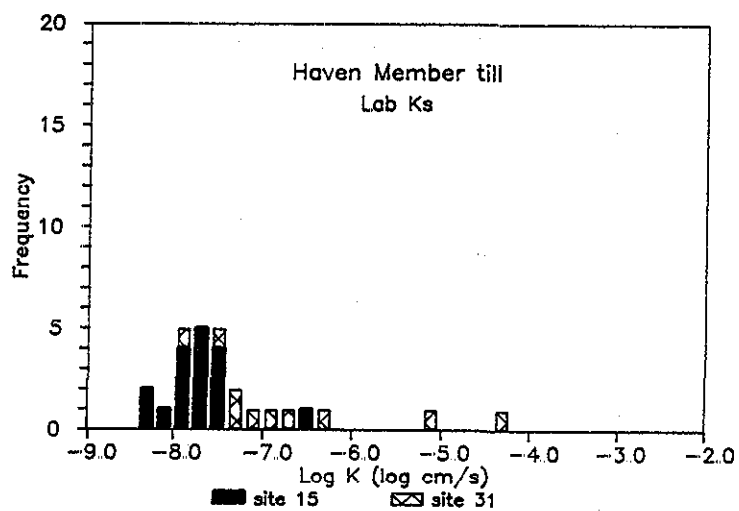
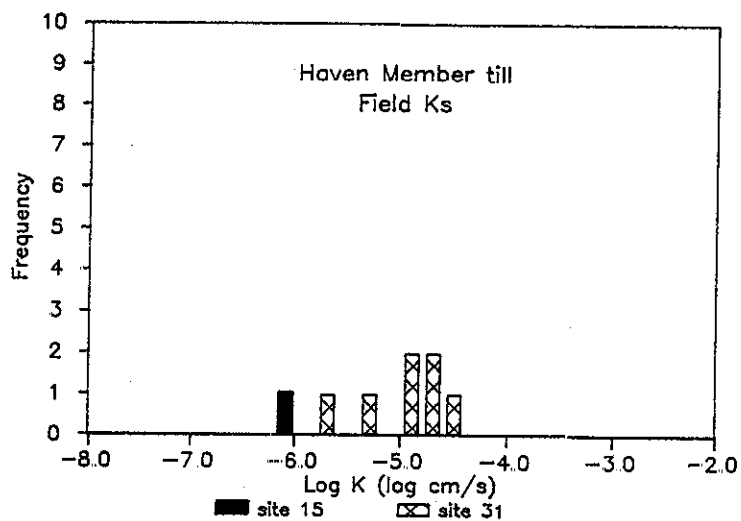


Figure 8g. Data for till in the Haven Member of the Kewaunee Formation. Field K means hydraulic conductivity measured in the field. Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.

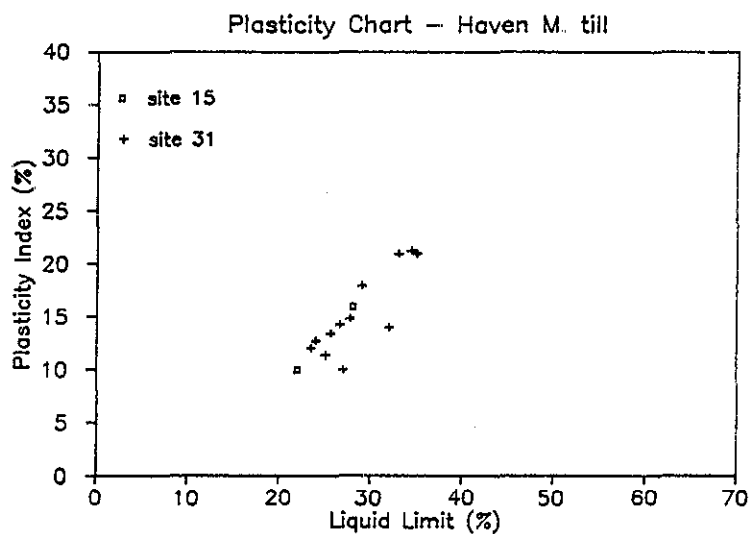
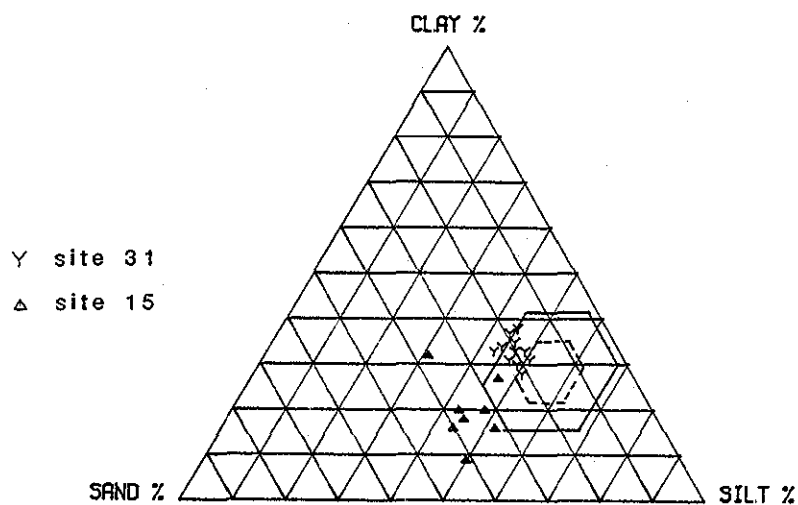


Figure 8g, cont. Data for till in the Haven Member of the Kewaunee Formation. Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the source.

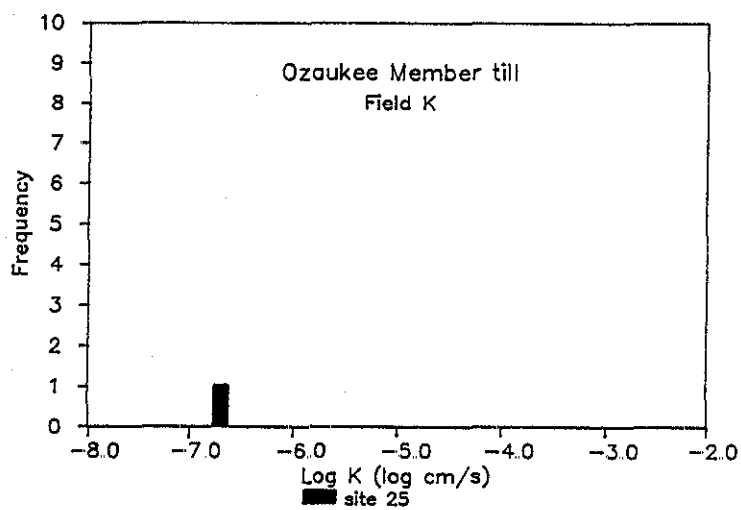


Figure 8h. Data for till in the Ozaukee Member of the Kewaunee Formation. Field K means hydraulic conductivity measured in the field. No values of hydraulic conductivity measured in the laboratory were compiled.

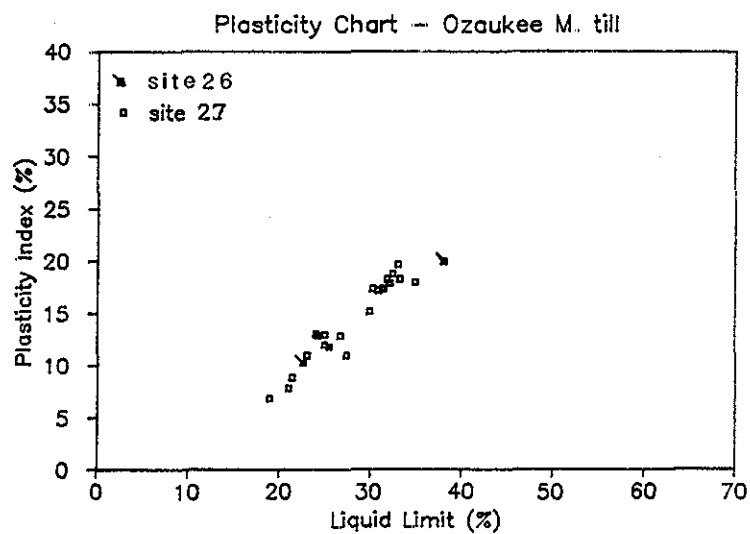
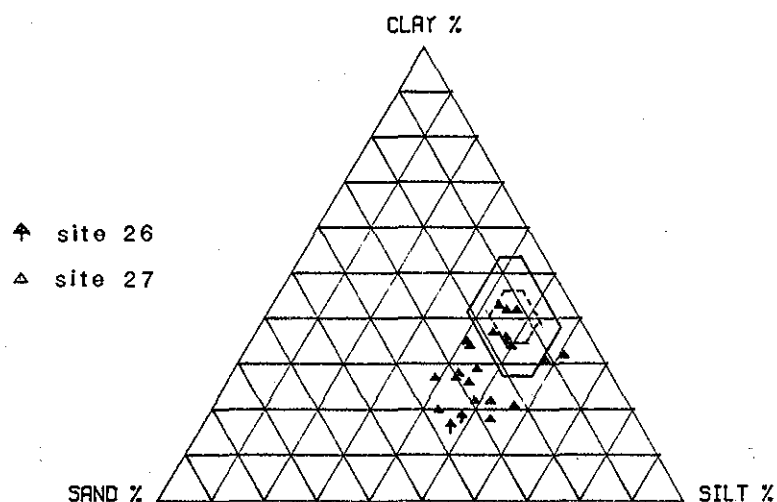


Figure 8h, cont. Data for till in the Ozaukee Member of the Kewaunee Formation. Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the source.

identical populations (Walpole and Myers, 1978, p. 495). There was insufficient evidence to reject the same null hypothesis in the Kirby Lake Member for sites 12, 40, and 41 (figure 8b).

b. Hydraulic conductivities measured in the laboratory

Values of hydraulic conductivity measured in the laboratory range over at least two orders of magnitude in the Kewaunee Formation tills, and range over four orders of magnitude in both the Middle Inlet (figure 8b) and Haven Members (figure 8g). Sufficient data are available in the Haven, Glenmore, and Kirby Lake Members for the Kruskal-Wallis test. I rejected the null hypothesis that two independent samples are from identical populations in the Haven (sites 15 and 31, figure 8g) and Kirby Lake Members (sites 38 and 40, figure 8a), but there was not sufficient evidence to reject the null hypothesis for the Glenmore Member (sites 1 and 10, figure 8c).

c. Textural triangles

I used statistical summaries from McCartney and Mickelson (1982) and Acomb, Mickelson, and Evenson (1982) to construct the envelopes drawn on the textural triangles. The dashed lines represent one standard deviation and the solid lines represent two standard deviations from a mean. The compiled data clearly do not always plot within the confidence levels for each unit determined by previous authors. This is conspicuously true for tills in the Kirby Lake (figure 8a), Middle Inlet (figure 8b), Glenmore (figure 8c), and Ozaukee (figure 8h) Members.

d. Plasticity charts

The plasticity charts illustrate consistent trends at individual sites within each unit. Tills tend to plot in a long cluster with a positive slope. I regressed plasticity index on liquid limit for sites 12, 30, 38, and 40 in the Kirby Lake Member (figure 8b). At these sites, approximately 95, 74, 86, and 84% of the variation in plasticity index was accounted for by a straight line regression equation with liquid limit. The regressed lines for sites 12 and 30 are nearly identical. The 95% confidence levels for all the lines overlap.

2. Oak Creek Formation

Data for tills of the Oak Creek Formation are summarized in figure 9.

a. Hydraulic conductivities measured in the field

Field hydraulic conductivities in the Oak Creek Formation range over four orders of magnitude, but at least two subgroups can be distinguished by looking carefully at the histogram (figure 9a). Sites 35, 37 and 55 have generally greater hydraulic conductivity than sites 14, 21 and 53, for example. An analysis of variance test at the 95% confidence level resulted in rejection of the null hypothesis that all site medians are equal.

b. Hydraulic conductivities measured in the laboratory

Hydraulic conductivities measured in the laboratory for samples of till from the Oak Creek Formation range over nearly three orders of magnitude, but subgroups are not as easily seen in the histogram (figure 9b) as for hydraulic conductivity measured in the field

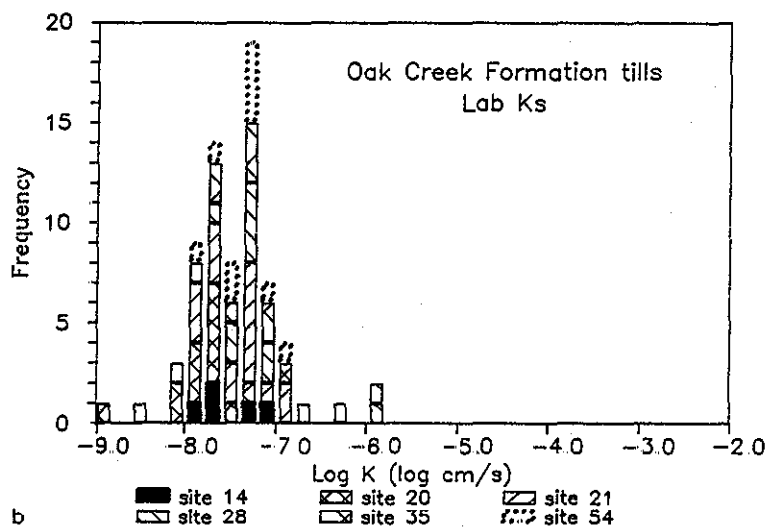
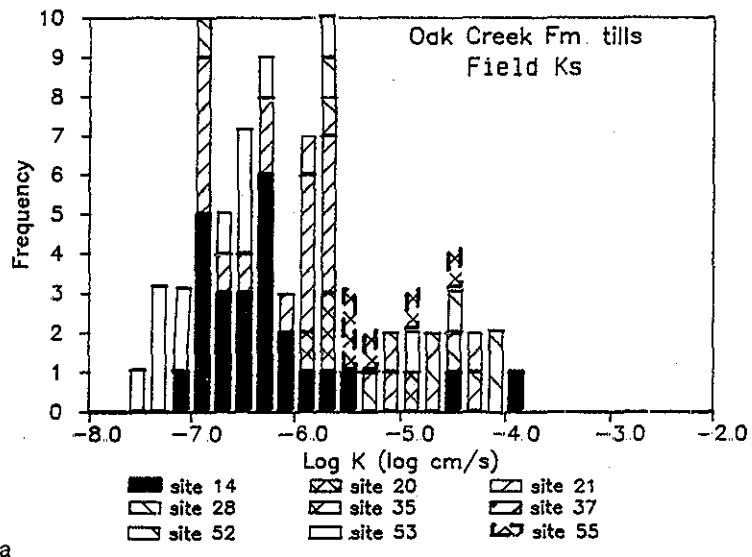
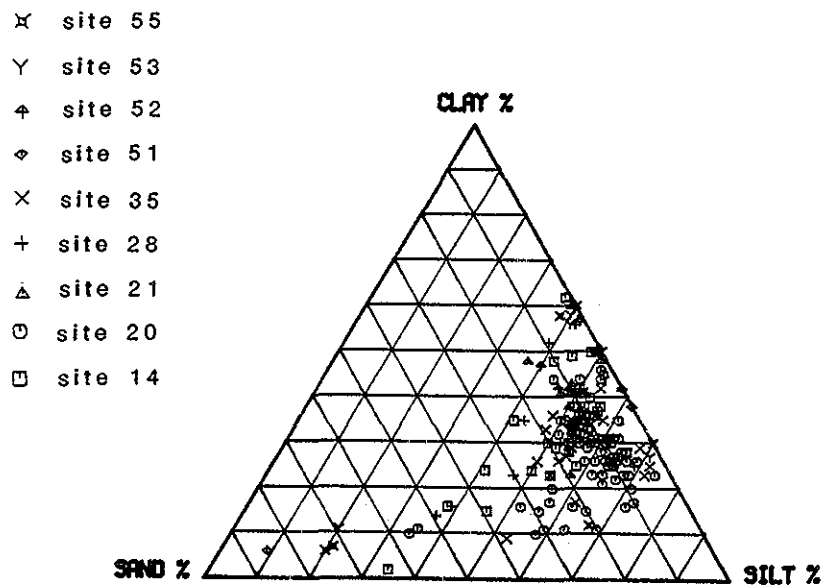
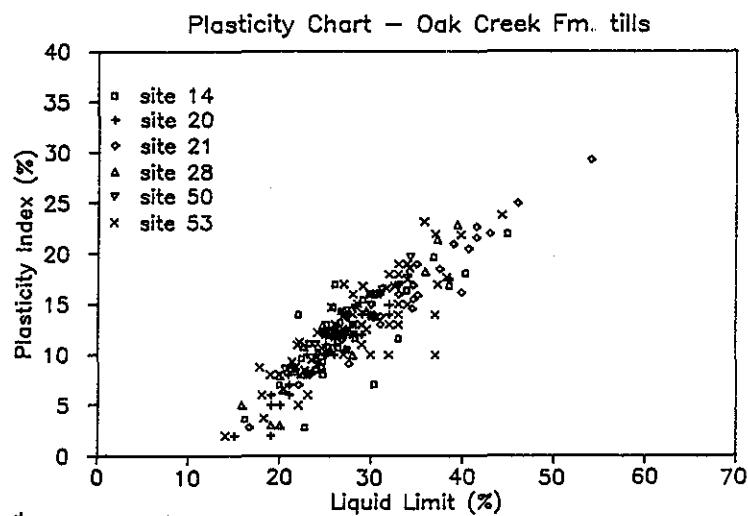


Figure 9. Data for till of the Oak Creek Formation. a) Field K means hydraulic conductivity measured in the field. b) Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.





c



d

Figure 9, cont. Data for till of the Oak Creek Formation. c) Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the source.

(figure 9a). The results of an ANOVA test indicate that separate populations do exist, however. The null hypothesis that six independent samples (sites 14, 20, 21, 28, 35, and 54) are from the same population was rejected at a 99.5% confidence level.

c. Textural triangle

The particle size distribution of till in the Oak Creek Formation has not been statistically summarized, but ". . . the average composition is about 12 percent sand, 43 percent silt, and 45 percent clay . . . The texture of the till ranges from silty clay through clay loam and silty clay loam to silt loam" (Mickelson and others, 1984, p. A8-2). The data in figure 9c exhibit a quite similar distribution (refer to figure 2 for textural terms). The numerous analyses from site 20 cover nearly the entire range.

d. Plasticity chart

The plasticity chart (figure 9d) shows that data for till from different sites in the Oak Creek Formation plot within the same cluster. I regressed plasticity index on liquid limit and plotted the least squares regression lines for sites 14, 21, 28, 35, 37, 50, 52, 53, and 54. At these sites, 59, 93, 94, 89, 69, 79, 96, 90, 98, and 89% of the variation in plasticity index was accounted for by a regressed straight line equation with liquid limit. The lines for sites 14, 52, 21, and 35 have lower slopes than the others, but all the lines cross one another between liquid limits of 20 and 45. They are not significantly different.

e. Pocket penetrometer

Pocket penetrometer measurements on Oak Creek Formation tills range over the entire discrete scale, from 0.5 to 4.5 tsf. Pocket penetrometer data are not presented graphically except for comparison between lithostratigraphic units in a later section; the data are discussed here because there are sufficient values to statistically analyze variation within the till unit. Measurements at sites 21 and 28 yield relatively low values, with medians of 2.5 and 2.6 tsf. Medians at the other sites are between 3.0 and 3.3 tsf. Site 31 has the highest median, 4.0 tsf. The Kruskal-Wallis ANOVA test (95% confidence) indicated that the medians at independent sites are not from the same population.

f. Dry unit weight

Dry unit weights range from 89.0 to 140.0 pcf in tills of the Oak Creek Formation. Dry unit weight data are not presented graphically except for comparison between lithostratigraphic units in a later section; the data are discussed here because there are sufficient values to statistically analyze variation within the till of the Oak Creek Formation. Median values at individual sites range from 115.0 to 120.8 pcf at sites with greater than 5 samples. A Kruskal-Wallis test at the 95% confidence level did not indicate that separate populations exist at sites 21, 28, 35, and 54.

### 3. Horicon Formation

Figure 10 includes graphical summaries of values of hydraulic conductivity, grain size analyses, and a plasticity chart for till of the Horicon Formation.

#### a. Hydraulic conductivities measured in the field

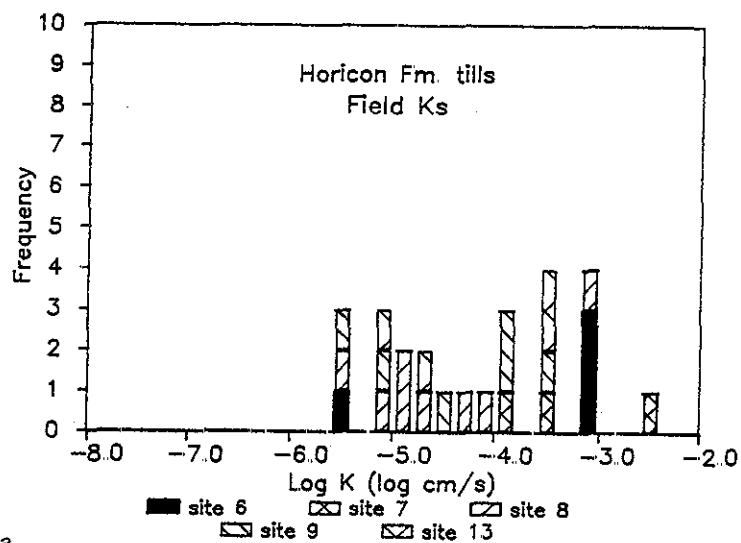
Field hydraulic conductivities range over three orders of magnitude (figure 10a). Nearly the entire range is present at sites 8 and 9. Sufficient data were available at these two sites for a Kruskal-Wallis ANOVA test. Insufficient data are available to reject the null hypothesis of equal medians at the two sites.

#### b. Hydraulic conductivities measured in the laboratory

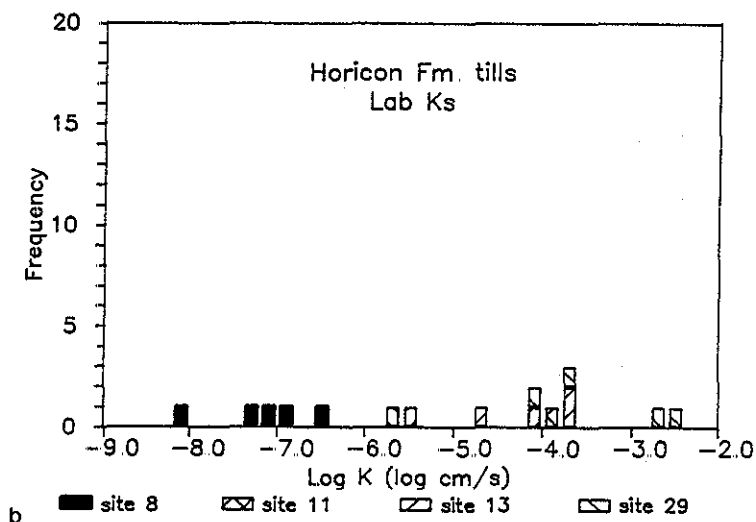
Since the Horicon Formation till matrix is typically 60-80% sand (Mickelson *et al.*, 1984, p. A9-2), the collection of an undisturbed sample for a laboratory hydraulic conductivity test is difficult. I suspect that the values of hydraulic conductivity measured in the laboratory for site 8 may be recompact, molded samples unrepresentative of *in-situ* conditions (figure 10b). These samples are included here because they were not recorded as recompact. Sites 8, 13, and 29 have five samples each, enough for a Kruskal-Wallis ANOVA test. The test resulted in a rejection of the null hypothesis of equal median hydraulic conductivity values at all sites.

#### c. Textural triangle

Relatively few analyses of till were completed to the clay size fraction (figure 10c). This lack of data results from the mandated

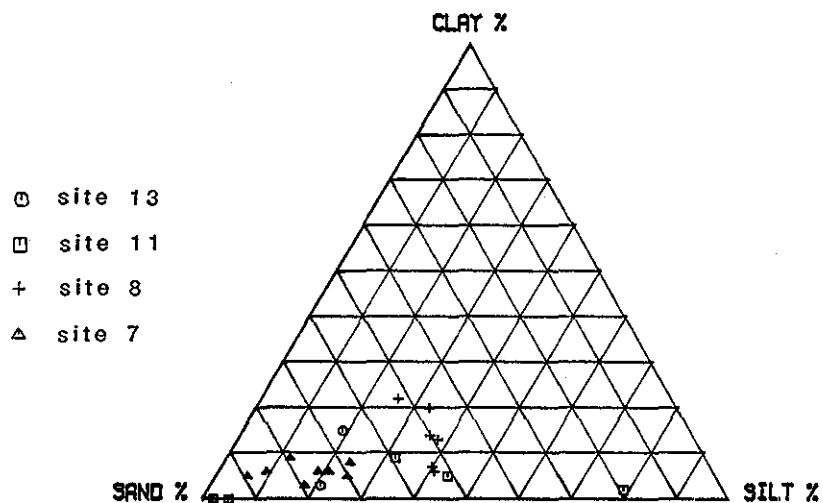


a

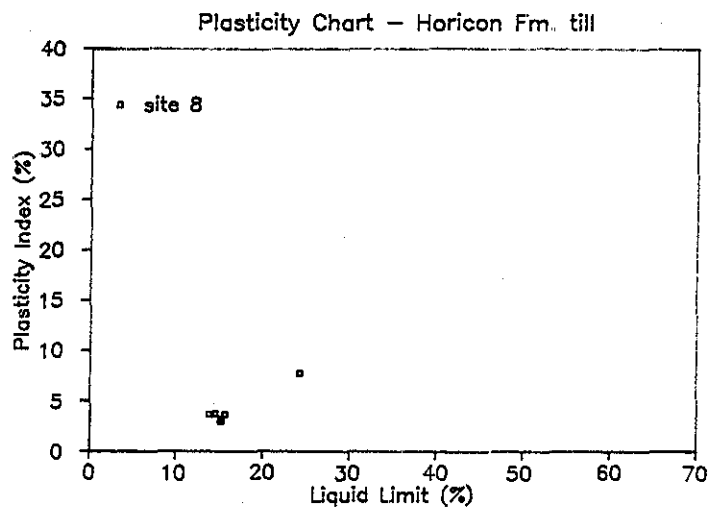


b

Figure 10. Data for till of the Horicon Formation. a) Field K means hydraulic conductivity measured in the field. b) Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.



c



d

Figure 10, cont. Data for till of the Horicon Formation. c) Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the source.

use of the unified soil classification system (USCS). The dotted lines represent two standard deviations from sand, silt, and clay means determined by McCartney (1979, p. 11) for basal till in the Mapleview Member of the Horicon Formation. Statistical summaries are not available for the Liberty Grove Member, but the analyses at sites 7, 8, and 13 are similar texturally to the Mapleview Member.

d. Plasticity chart

Few samples of Horicon till (figure 10d) are so fine-grained that completion of liquid limit and plastic limit tests and plotting on a plasticity chart is necessary for classification in the USCS. The samples with Atterberg limits plot in a small cluster with a lone point indicating the same general trend seen in other tills.

4. Unnamed unit

A material similar to till of the Horicon Formation but much siltier than the Mapleview and Liberty Grove Members was identified at several sites near Lake Winnebago. Figure 11 contains graphs of the data. This material may represent a member of the Horicon Formation. A geologic investigation is required to determine the nature of its occurrence.

a. Hydraulic conductivity measured in the field

The range of field hydraulic conductivity values measured in the field covers four orders of magnitude (figure 11a). Application of an ANOVA test to data from sites 40 and 41 resulted in rejection of the null hypothesis of equal medians at a 95% confidence level.

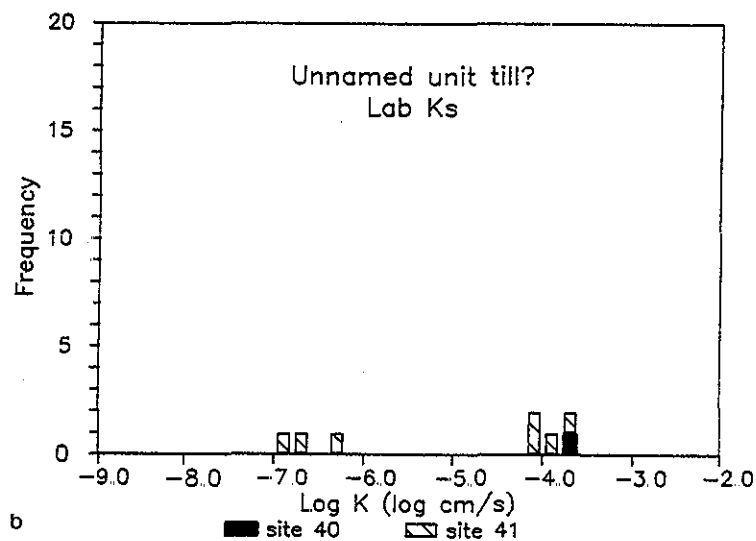
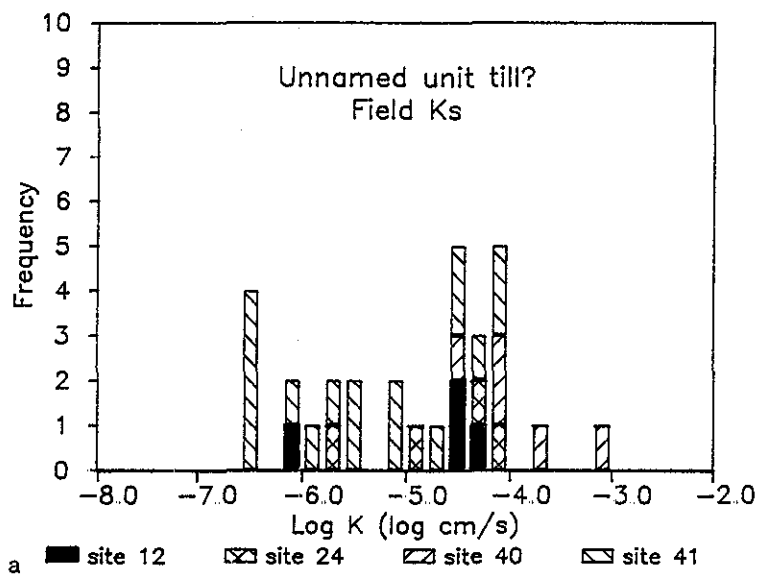
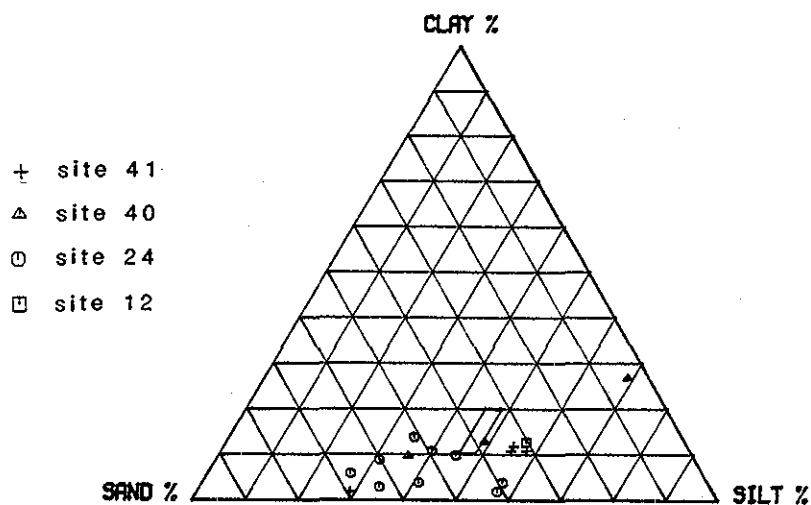
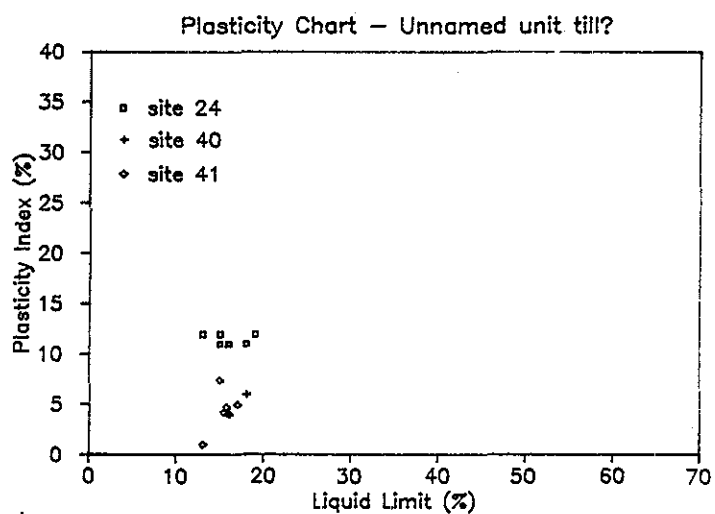


Figure 11. Data for an unnamed unit, possibly till of the Horicon Formation. a) Field K means hydraulic conductivity measured in the field. b) Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.





c



d

Figure 11, cont. Data for an unnamed unit, possibly till of the Horicon Formation. c) Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the source.

b. Hydraulic conductivity measured in the laboratory

The data here appear bimodal (figure 11b), and I again suspect that some of the hydraulic conductivity values measured in the laboratory may be for recompacted samples although they were not recorded as such.

c. Textural triangle

Textures for samples analyzed to 0.002 mm include sandy loam, loam, and silt loam (figure 11c). An envelope of texture for till of the Wayside Member of the Horicon Formation in Brown County described by Need (1985) is included for comparison.

d. Plasticity chart

The unnamed unit is roughly 30% stone (over 2 mm diameter) so that few samples have values of P200 greater than 50% by weight. Consequently, determination of Atterberg limits is not necessary for classification in the USCS. Data from sites 40 and 41 plot in the pattern expected for tills (figure 11d). Although the liquid limits at site 24 have the same range as sites 40 and 41, the data cluster separately.

5. New Berlin Formation

Few hydraulic conductivity data for till of the New Berlin Formation were compiled (figures 12a and 12b), and no statistical analysis of variation within the unit is possible. The particle size analyses compiled graph in a fairly tight cluster except for the Washington County sites (34 and 36, figure 12d).

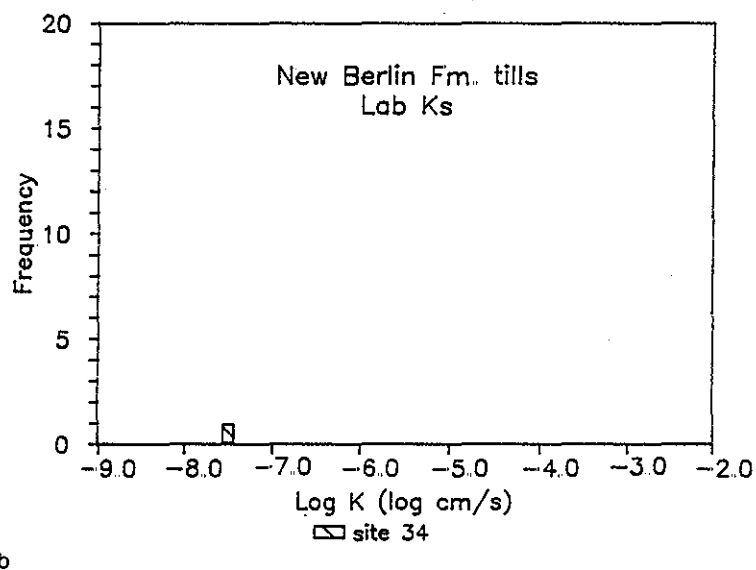
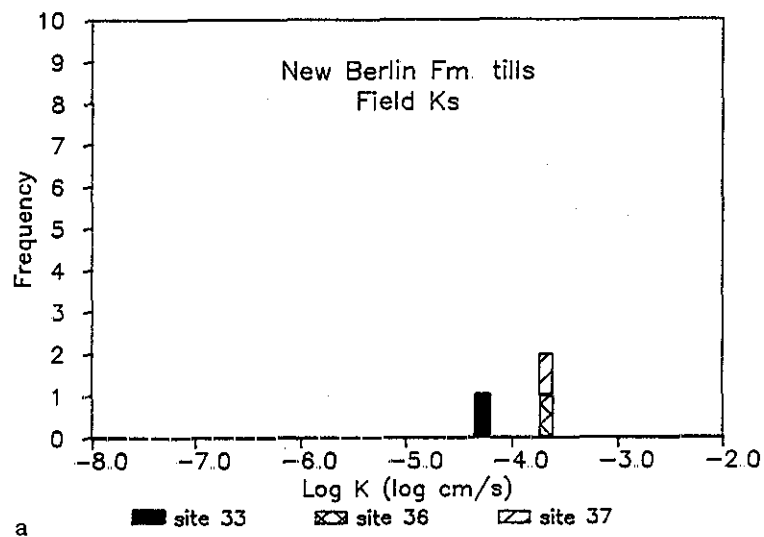
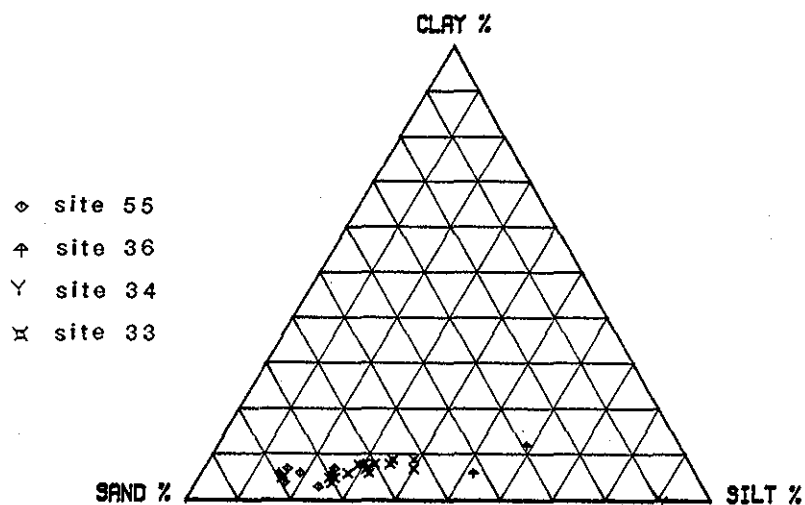
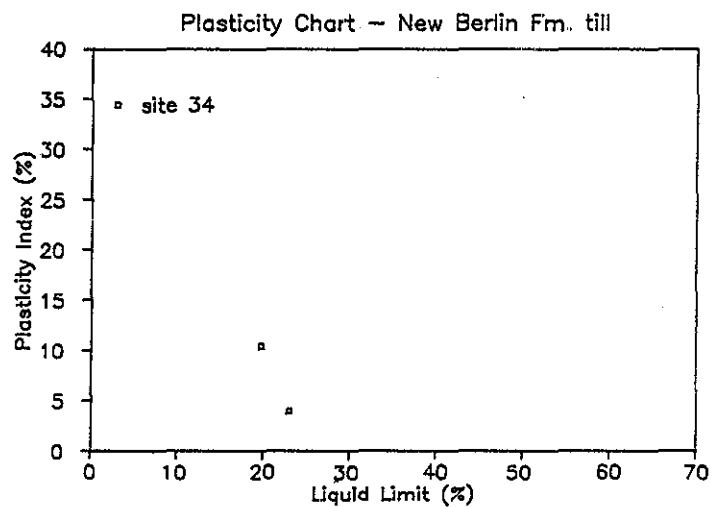


Figure 12. Data for till of the New Berlin Formation. a) Field K means hydraulic conductivity measured in the field. b) Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.



c



d

Figure 12, cont. Data for till of the New Berlin Formation. c) Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the site.

## 6. Tiskilwa Member of the Zenda Formation

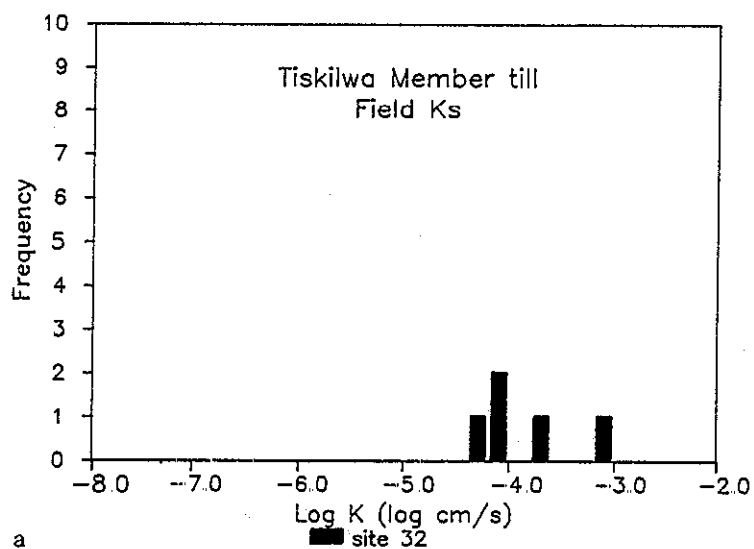
Data for the Tiskilwa Member were collected from only one site in the Lake Michigan Lobe, so no analysis of variance within the member from one site to another is possible. The available data are summarized graphically in figure 13. Hydraulic conductivities measured in the field range over 1 1/2 orders of magnitude at site 32 (figure 13a). Only one value of hydraulic conductivity was measured in the laboratory for till of the Tiskilwa Member (figure 13b). On the plasticity chart, till of the Tiskilwa Member plots in an elongate cluster with positive slope (figure 13d).

### B. Variation between tills of lithostratigraphic units

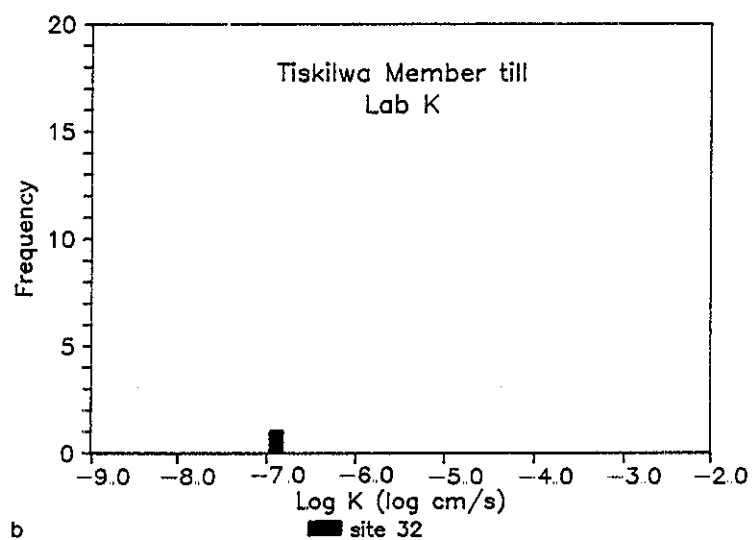
#### 1. Interunit comparisons of hydraulic conductivity measured in the field

##### a. The Green Bay Lobe

There is a statistically significant difference in hydraulic conductivity between till of the Middle Inlet and Kirby Lake Members of the Green Bay Lobe. I rejected the null hypothesis that the median log values of hydraulic conductivity measured in the field for till in the Middle Inlet Member and for till in the Kirby Lake Member are equal at the 99.5% confidence level. It is apparent from the boxplots in figure 14 that portions of the fourth spread overlap for these till units. The median hydraulic conductivity measured in the field for till of the Middle Inlet Member is about an order of magnitude greater than the median value for till of the Kirby Lake Member.



a



b

Figure 13. Data for till of the Tiskilwa Member of the Zenda Formation. a) Field K means hydraulic conductivity measured in the field. b) Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.

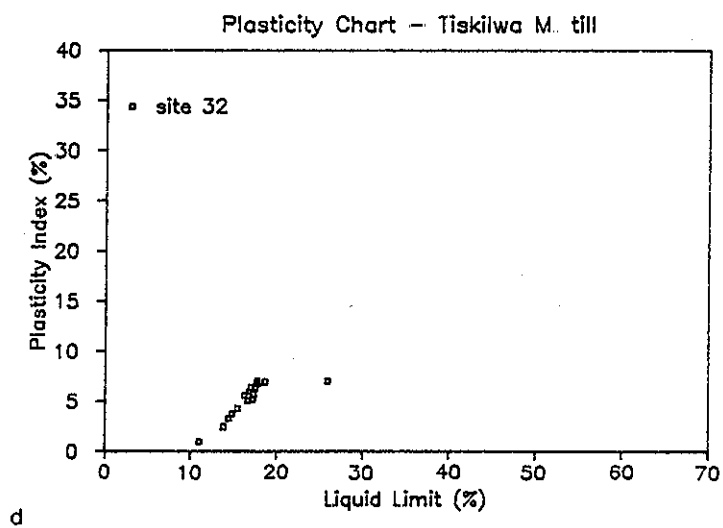
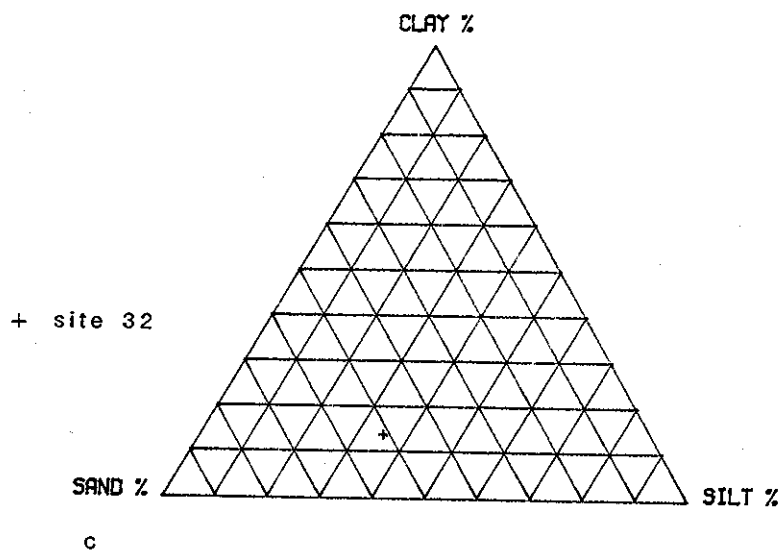


Figure 13, cont. Data for till of the Tiskilwa Member of the Zenda Formation. c) Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the source.

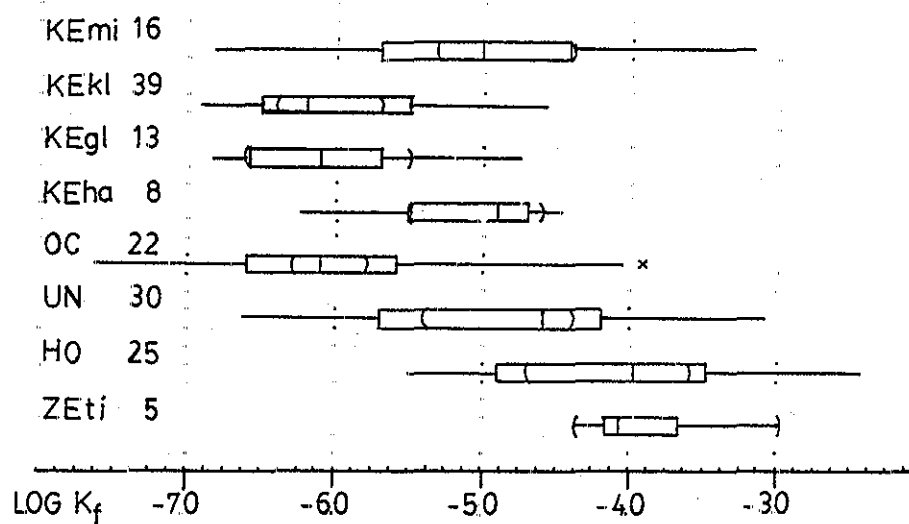


Figure 14. Boxplots for interunit comparison of hydraulic conductivity measured in the field ( $K_f$ ). Boxplots are constructed for till units with at least 5 values. The number of values is given with the abbreviated unit name.



As mentioned in the section on variation within units, the unnamed unit stratigraphically below the Kewaunee Formation could be a member of the Horicon Formation. I rejected the null hypothesis that the medians of log hydraulic conductivity measured in the field in till of the unnamed unit and in till of the Horicon Formation are equal with a confidence level of 99%. Median log hydraulic conductivity measured in the field for these two tills differ by 0.6 order of magnitude.

To the east, the location of the batch median for the Glenmore Member may be compared to the data available for till of the Chilton Member (figure 14 and figure 8d). Each of the four measurements in till of the Chilton Member are within the 95% confidence limits for till of the Glenmore Member. The unnamed unit discussed in the preceding paragraph may also underlie the Kewaunee Formation on the eastern side of the Green Bay Lobe. The Horicon Formation does extend eastward to the Lake Michigan Lobe (see Plate 1).

b. Lake Michigan Lobe

Hydraulic conductivity data from field measurements are not available for till in each member of the Kewaunee Formation. Insufficient data (fewer than 5 samples) are available for tills in the Haven and Ozaukee Members to test a null hypothesis, but the boxplot for till of the Haven Member in figure 14 may be compared to data for the Ozaukee Member in figure 8h. The single value for till

of the Ozaukee Member lies outside the range of 95% confidence for the median value of field hydraulic conductivity in the Haven Member.

Hydraulic conductivity data from field measurements of till in the Oak Creek Formation are relatively plentiful. In spite of the range over four orders of magnitude (figure 9), the range of the 95% confidence level for the median is only half an order of magnitude wide (figure 14).

Data compiled for the New Berlin Formation contain only four values of hydraulic conductivity measured with field tests (figure 12). Hydraulic conductivity values in till of the New Berlin Formation are 3 to 4 orders of magnitude greater than the median value for tills of the Oak Creek Formation in figure 14. Values of hydraulic conductivity measured in the field in tills of the New Berlin Formation have a range similar to till in the Tiskilwa Member of the Zenda Formation. A boxplot of hydraulic conductivity values measured in the field for till in the Tiskilwa Member is included in figure 14.

## 2. Interunit comparison of hydraulic conductivity measured in the laboratory

The median values hydraulic conductivity measured in the laboratory for each till have narrower approximate 95% confidence intervals than do the median values of hydraulic conductivity measured in the laboratory (note the scale differences before comparing figures 14 and 15). As for values of hydraulic conductivity measured in the field, boxplots have been constructed for tills with five or more

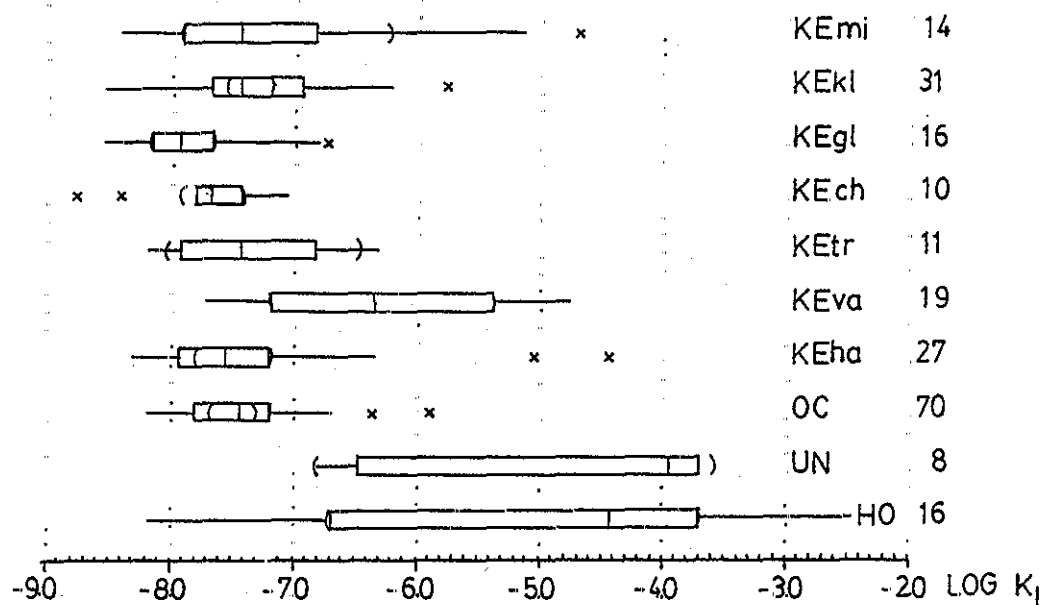


Figure 15. Boxplots for interunit comparison of hydraulic conductivity measured in the laboratory ( $K_1$ ). Boxplots are constructed for till units with at least 5 values. The number of values is given with the abbreviated unit name.

values available. ANOVA tests were applied to tills of overlying members. Refer back to figures 12 and 13 for the New Berlin and Zenda Formations.

In the Green Bay Lobe, insufficient data were available to reject the null hypothesis of equal median values of hydraulic conductivity measured in the laboratory for tills of these stratigraphically superposed lithostratigraphic units: Middle Inlet and Kirby Lake Members, Glenmore and Chilton Members, and the unnamed unit and the Horicon Formation. In the Lake Michigan Lobe, I rejected the same null hypothesis at a 99.5% confidence level for tills in both the Two Rivers and Valders Members and the Valders and Haven Members.

### 3. Vertical differences in texture

#### a. Green Bay Lobe

The tills of superposed members have similar textural ranges on both the east and west sides of the Green Bay Lobe. On the west side, the Middle Inlet Member analyses show greater scatter than those of the Kirby Lake Member below and include some samples that are much sandier than till of the Kirby Lake Member. On the east side of Green Bay, the till unit in the Glenmore Member is also slightly sandier than till of the underlying Chilton Member. Tills of the Horicon Formation are distinguished from tills in the Kewaunee Formation by their abundant sand content.

#### b. Lake Michigan Lobe

As in the Green Bay Lobe, till of the Two Rivers Member (figure 8e) is texturally very similar to till of the underlying Valders

Member (figure 8f). The cluster of points for till of the Two Rivers Member illustrates a sandier 'average' texture than the cluster of till analyses for the Valders Member. Thus, texture in the upper two tills in the Green Bay and Lake Michigan Lobes changes in the same way, with increasing sand content upwards. The textures determined for till of the Haven Member (figure 8g) are less silty but otherwise very similar to till of the Valders Member (figure 8f). Till of the Ozaukee Member (figure 8h) contains more silt and clay than till of the Haven Member.

Below the Kewaunee Formation, till of the Oak Creek Formation is very similar to till in the Ozaukee Member. Many more particle size analyses are available for the Oak Creek Formation tills, and a wide range in texture is apparent. The tills of the New Berlin Formation, like till in the Horicon Formation, is distinctively sandy with a very low clay content. Only one complete analysis for till in the Tiskilwa Member was recorded. This single sample contains more clay than the 'average' till samples from the New Berlin Formation.

#### 4. Interunit comparison of plasticity charts

Scatterplots of plastic index and liquid limit for the till units overlap. If the mean liquid limit and plastic index are used to represent each till as in figure 16, the same general trend emerges as from the individual plots with finer grained units farther from the origin.

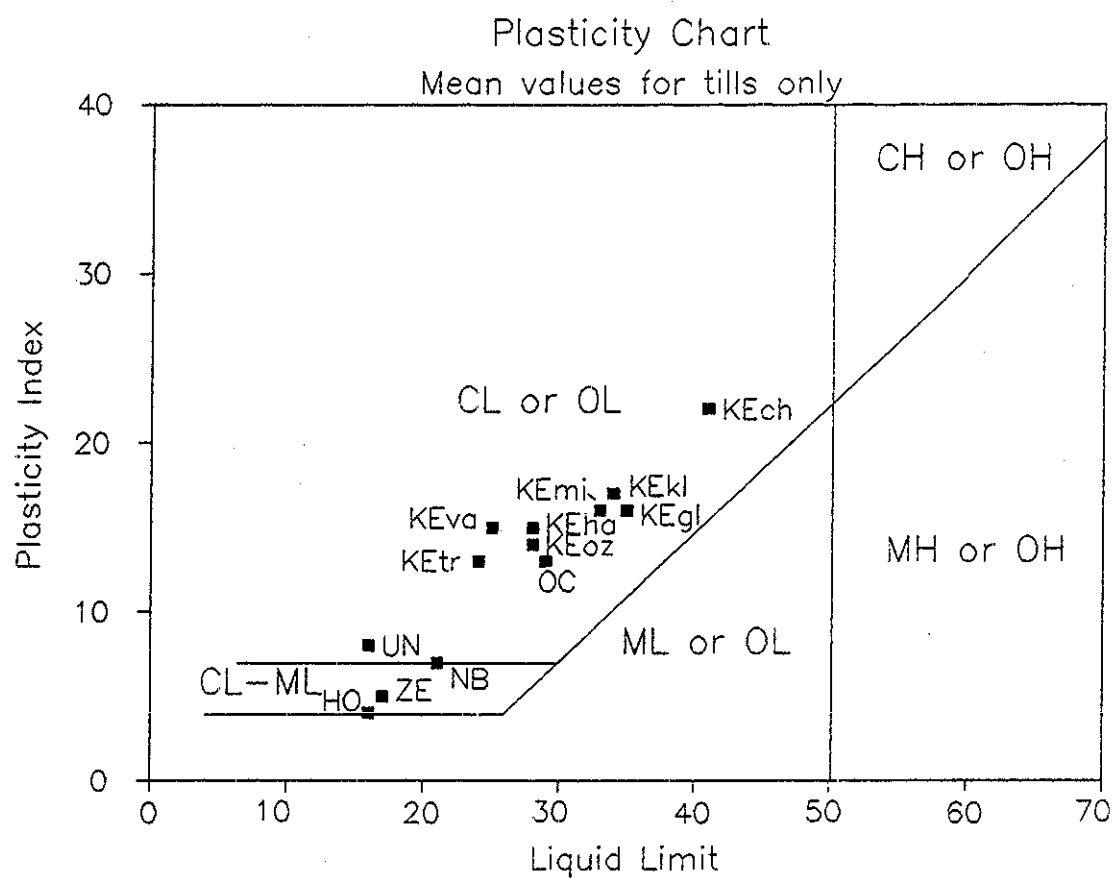


Figure 16. Plasticity chart with mean values of plasticity index and liquid limit for tills of lithostratigraphic units.

### 5. Interunit comparison of dry unit weight

Figure 17 consists of boxplots of dry unit weight for those units with five or more measurements. Dry unit weight data are summarized in table 4. The median dry unit weight of tills are very similar in superposed members of the Kewaunee Formation on the west side of the Green Bay Lobe (Middle Inlet and Kirby Lake Members) and in the Lake Michigan Lobe (Two Rivers, Valders, and Haven Members). Till of the Ozaukee Member is more similar to till of the Oak Creek Formation than to other Kewaunee Formation tills with respect to dry unit weight. A null hypothesis of equal median dry unit weights for the Haven and Ozaukee Member tills was rejected at a level of 99% confidence. The same null hypothesis could not be rejected for tills of the Ozaukee Member and the Oak Creek Formation or for other members in the Kewaunee Formation.

The median dry unit weight for the Horicon Formation exceeds all other medians by 15 pounds per cubic foot. This is most likely due to the unit lithology since the specific gravity of dolomite is greater than the specific gravity typically assumed for soils. Alternatively, the difference may be caused by the coarse particle size. No dry unit weight data were compiled for the New Berlin Formation, but it probably also has a relatively high dry unit weight because its lithology and particle size distribution resembles that of the Horicon Formation.

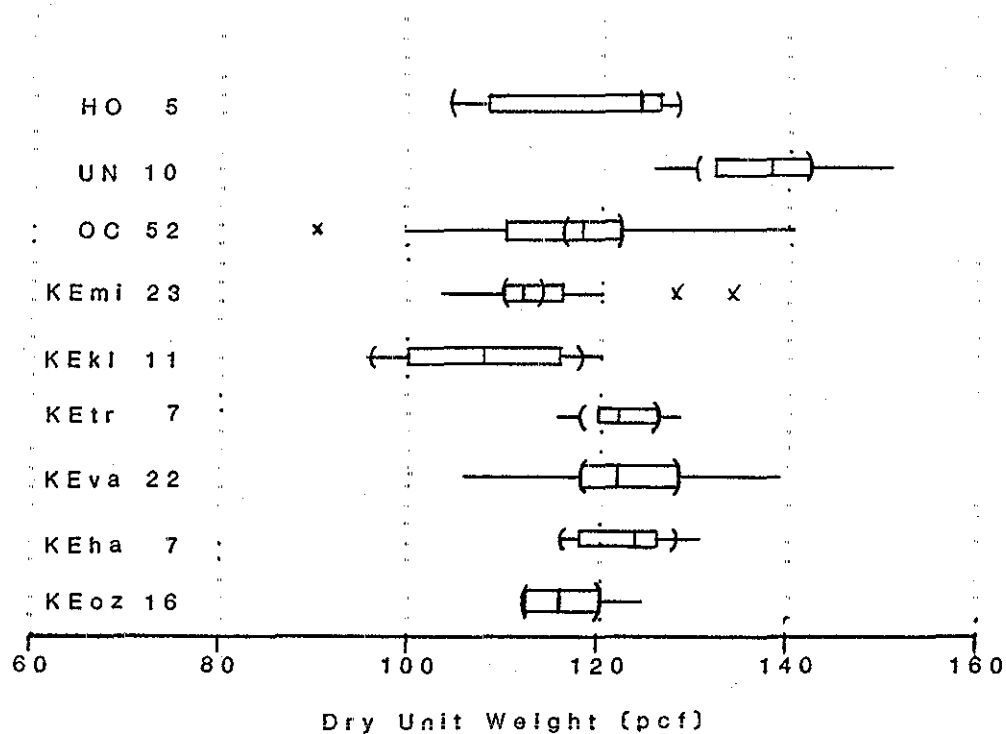


Figure 17. Boxplots for interunit comparison of dry unit weight. Boxplots are constructed for till units with at least 5 values. The number of values used to construct the boxplot is given with the abbreviated unit name.



## Dry unit weight (pounds per cubic foot)

<u>till</u>	<u>N</u>	<u>Median</u>	<u>Minimum</u>	<u>Maximum</u>
KEmi	23	112.0	103.2	133.1
KEkl	11	107.0	61.1	119.8
KEgl	2	114.5	114.0	115.0
KEch	0	-	-	-
KEtr	7	122.0	115.5	127.9
KEva	22	122.4	99.7	138.5
KEha	7	123.0	115.4	129.7
KEoz	16	116.1	111.1	123.0
OC	52	117.8	89.0	140.0
NB	0	-	-	-
ZEti	0	-	-	-
HO	10	138.7	125.8	150.6
UN	5	123.9	104.7	128.1

Table 4. Statistical summary of dry unit weights in pounds per cubic foot for tills in lithostratigraphic units (except for 'UN') with number of samples (N), median values, minimum value, and maximum value.

## 6. Pocket Penetrometer

Surprisingly, the median pocket penetrometer measurement is significantly different for Lake Michigan Lobe tills in superposed lithostratigraphic units. Pocket penetrometer data is presented graphically in figure 18. The ranges are almost identical for all units. I tested and rejected the null hypothesis of equal medians for one way ANOVA of tills in the Two Rivers and Valders Members (97.5% confidence level), the Valders and Haven Members (99.5% confidence level), the Haven and Ozaukee Members (99.5% confidence level), and the Ozaukee Member and the Oak Creek Formation (99.5% confidence level). The same null hypothesis could not be rejected for tills of superposed members in the Green Bay Lobe.

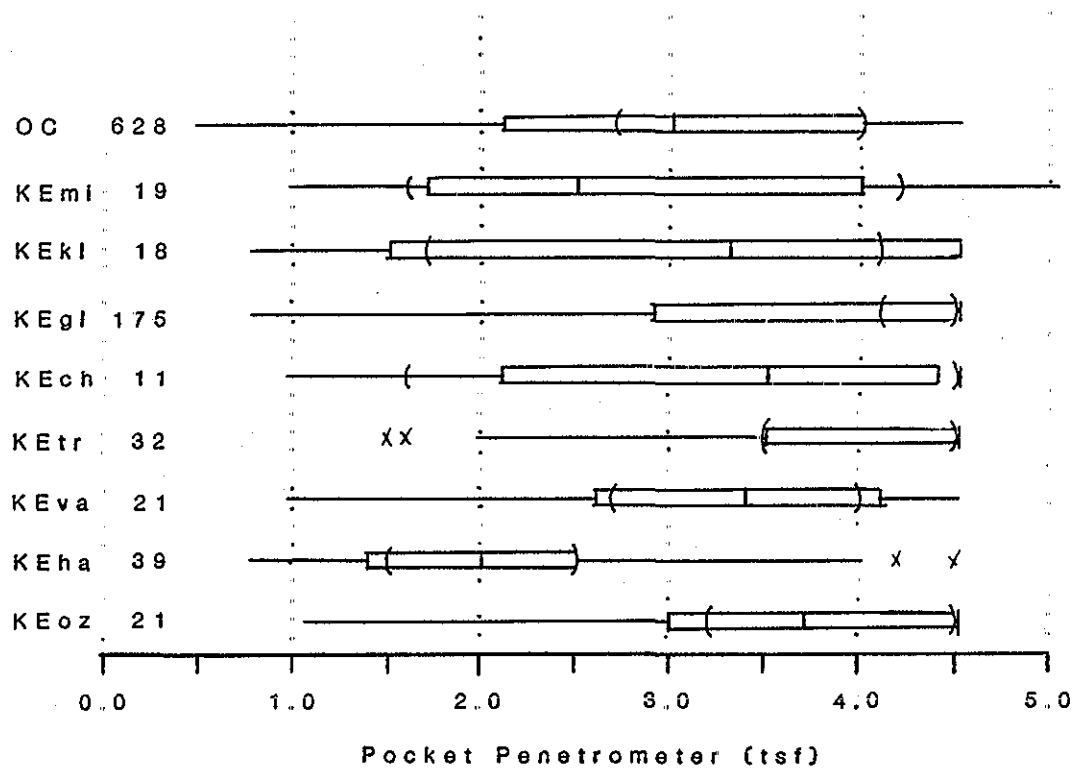


Figure 18. Boxplots for interunit comparison of pocket penetrometer measurements. Boxplots are constructed for till units with at least 5 values. The number of values is given with the abbreviated unit name.

## V. Discussion of data

This section contains a discussion of the data presented in part IV, emphasizing the test methods and relations to other tests in till units. I use correlation and regression analysis to determine which tests are meaningful to hydrologic or geologic interpretation. These correlations and regressions do not imply cause and effect relationships.

### A. Approximations of strength

#### 1. Standard penetration test

There is a great deal of disagreement over how useful the standard penetration test is to hydrogeologists. Blow counts (N) from the Standard Penetration Test (SPT) (D1586-84, ASTM, pp. 298-303) have been used with limited success as an index test of strength and a predictor of deformation. Blow counts have been correlated with the Dutch Cone Test, the friction angle of sand, density of sands, shear strength in clay, modulus of compressibility of sands, and liquefaction potential with some success (Douglas, 1983; Dept. of the Navy, 1982; Dunn, Anderson, and Kiefer, 1980). However, ASTM D1586-84 states,

"Variations in N-values of 100% or more have been observed when using different standard penetration test apparatus and drillers for adjacent borings in the same formation. Current opinion, based on field experience, indicates that when using the same apparatus and driller, N-values in the same soil can be reproduced with a coefficient of variation of about 10%" (ASTM, 1986, p. 299).

Similarly, Baecher attributed 50% of observed scatter in SPT data to measurement noise (1984, p.11). Little emphasis was placed on

collection of SPT data for this study because different test apparatus and drillers generated the data and because glacial tills are known to contain boulders that inflate SPT estimates of strength.

## 2. Pocket penetrometer

Pocket penetrometer readings are commonly reported (in tons per square foot, tsf) for fine-grained sediments but rarely correlated with any other parameters. They are a relative measure of the unconfined compressive strength of a material. The ASTM has not published a standard method for use of the pocket penetrometer; use of a vane shear device is preferred and has been quantitatively correlated with other tests. The Dept. of the Navy Soil Mechanics Design Manual includes the following brief statement about pocket penetrometers: "The tool is an aid to obtaining uniform classification of soils. It does not replace other field tests or laboratory tests" (1982, p. 7.1-97). Pocket penetrometer measurements were typically recorded only for samples having hydraulic conductivity or grain size analyses.

## 3. Applications of approximations of strength

Strength data is relevant to geologic interpretation, but most authors who refer to it combine it with data not included in this study's database. For example, Scott and St-Onge (1969) recommend use of the pocket penetrometer to estimate the compactness of till. They write, "Compactness . . . embodies concepts of cohesion, consolidation, shear strength, and, because of the range in grain size of till, also relative density and consistency" (1969, p. 4). They

define a compactness ratio,  $C_r$ , equal to bulk density divided by void ratio and apparently then use the compactness ratio to characterize till units (1969, p. 6). Other authors have related shear strength to geologic stress history (Mickelson, Acomb, and Edil, 1979), deposition of cementing agents from the ground water (Baracos *et al.*, 1983), clay mineralogy (Grim, 1962), density (Lutenegger, Kemmis, and Hallberg, 1981), and weathering profiles in till (Eyles and Sladen, 1981). It is important to note that these authors used laboratory determinations of shear strength, not a field approximation like the pocket penetrometer or a method characterized by high variation, like the standard penetration test. Although median pocket penetrometer measurements differ for individual till units, the data give little information about specific characteristics of the tills.

I investigated the relationship between density from SPT blow counts and hydraulic conductivity. One engineering firm implied that increasing blow counts correlate with decreasing field measurements of hydraulic conductivity. The data for till units are not suitable for correlation because they are not paired--blow counts vary over the screened interval used to determine field hydraulic conductivity.

SPT data show no correlation between blow counts and depth. From soil mechanics theory, I expect blow counts to increase with depth as the thickness of material over the interval measured increases. Figure 19, a scatterplot of SPT blow counts versus depth in the Oak Creek Formation, illustrates no correlation for these till,

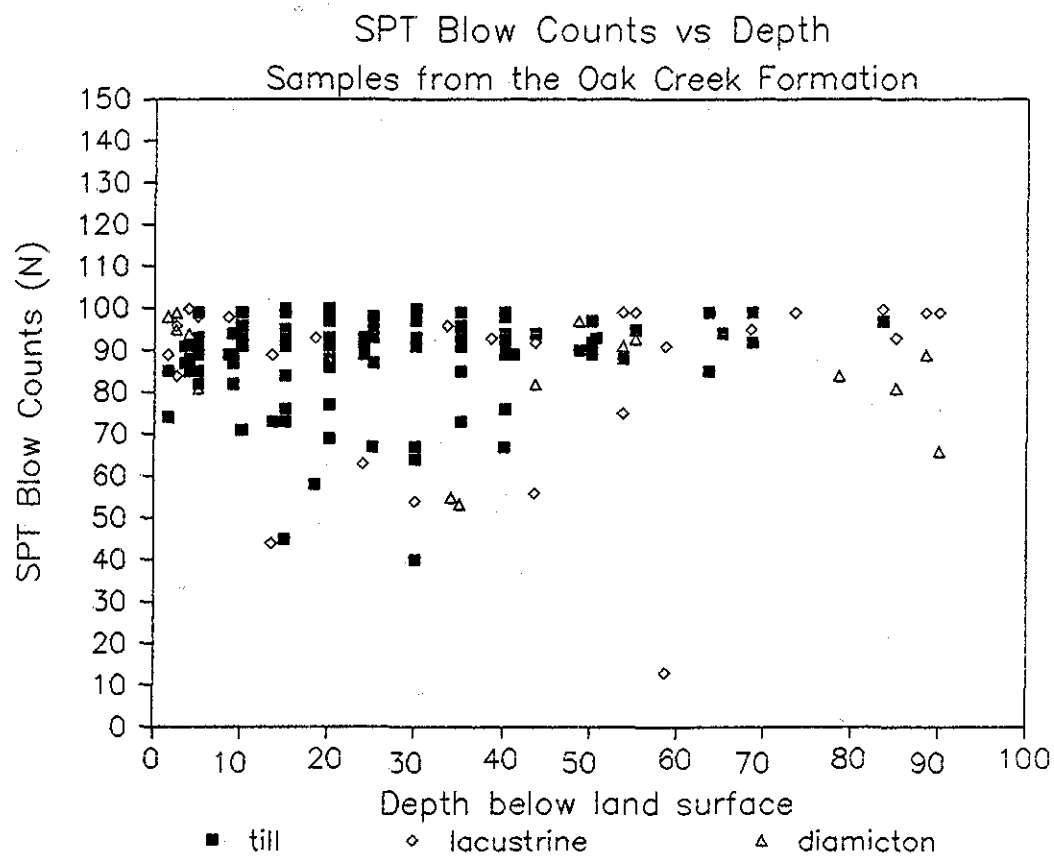


Figure 19. Plot of SPT blow counts as a function of depth below the land surface for sediments in the Oak Creek Formation.

lacustrine, or diamicton sediments, possibly because ". . . the test is conducted in a dynamic form and while the limited volume of material is in a state of failure and high disturbance" (Johnston, 1983, p. 12).

SPT blow counts have been correlated with shear strength in clay (e.g., Stroud and Butler, 1975) and pocket penetrometer measurements approximate unconfined compressive strength. However, a plot of SPT blow counts versus pocket penetrometer measurements for 453 samples of till from the Oak Creek Formation (figure 20) shows that a wide range of SPT blow counts may be anticipated for any pocket penetrometer measurement. Clearly, SPT blow counts and pocket penetrometer measurements are not directly related. A straight line, least squares regression indicates that 19% of the variation in blow counts may be explained by variation in pocket penetrometer measurements. Similar but not identical variables probably affect the two tests.

In individual boreholes considered in this study, pocket penetrometer readings tend to reach a maximum within several feet of the land surface. This maximum may reflect overconsolidation due to repeated wetting and drying within the capillary fringe, but appropriate consolidation data are not available to confirm this relationship. Moreover, pocket penetrometer readings should not be used to determine the elevation of the modern water table since the climate has changed following deposition of the sediment, and the zone of higher readings may represent past conditions.



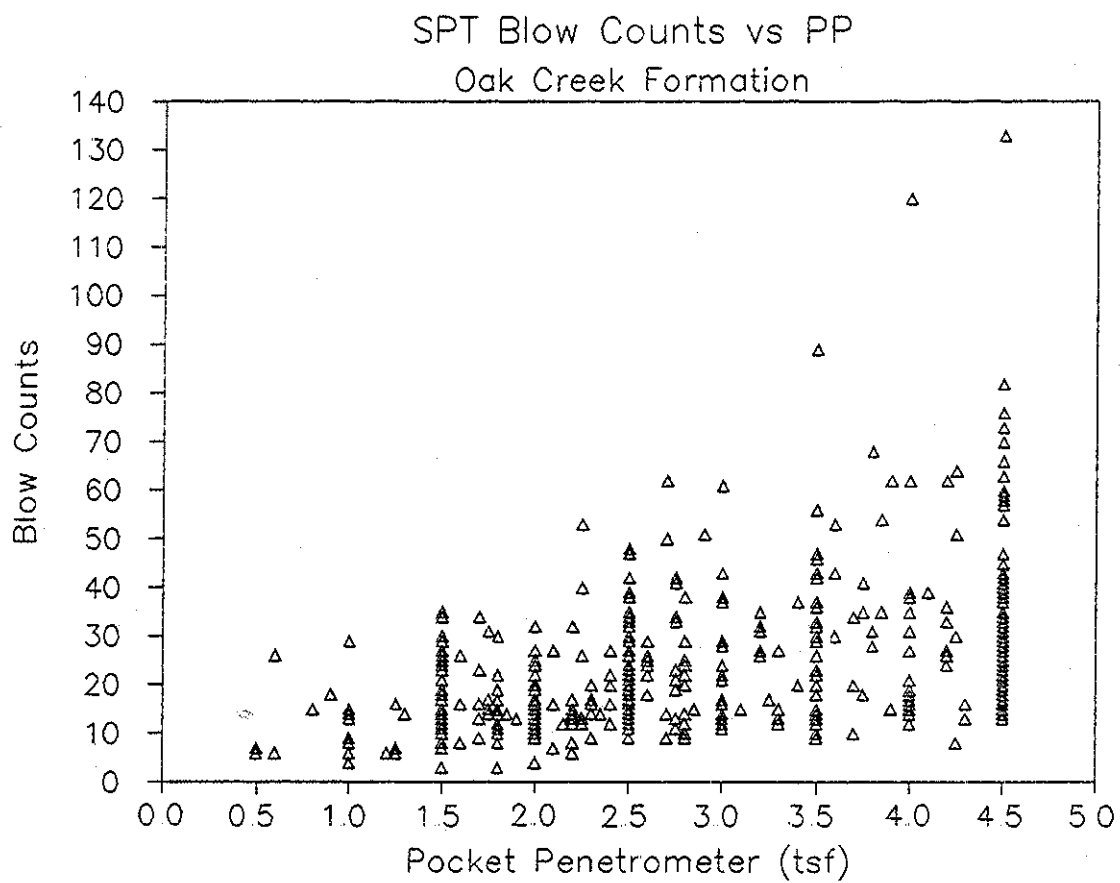


Figure 20. Plot of SPT blow counts as a function of pocket penetrometer measurements for samples of till in the Oak Creek Formation.

May and Thomson found higher strengths to be associated with lower moisture contents for selected till units of the Edmonton area (1978, p. 368). Figure 21 illustrates the relationship between natural moisture and log pocket penetrometer measurements for fine-grained till units included in this study. The individual units scatter throughout the large cluster without any indication of a trend characteristic of a single till or site. Similarly, Muldoon (1987), working with pre-late Wisconsin fine-grained till units in central Wisconsin, found no significant relationships between log pocket penetrometer and moisture content. Muldoon reported that other authors described a strong relationship between natural moisture and log pocket penetrometer for different Wisconsin till units.

#### B. Particle size analysis

The particle size divisions entered to the database include the percent of the sample greater than 2 mm, the percent sand, silt, and clay of the less than 2 mm fraction, and the P200 (percent passing the #200 sieve, 0.075 mm diameter). These categories were chosen to accommodate the different classification systems used by engineers and geologists. I recorded P200 values because this percentage is necessary for classification in the USCS and because analyses frequently are not completed beyond this particle size. Values of P200 are not presented except in the appendices because this percentage varies considerably with measurement technique. Values of P200 determined by dry sieving tend to be lower than those determined

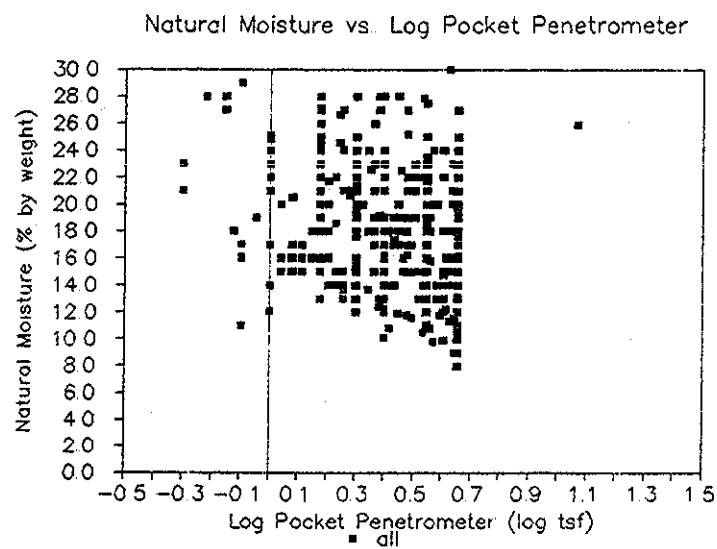
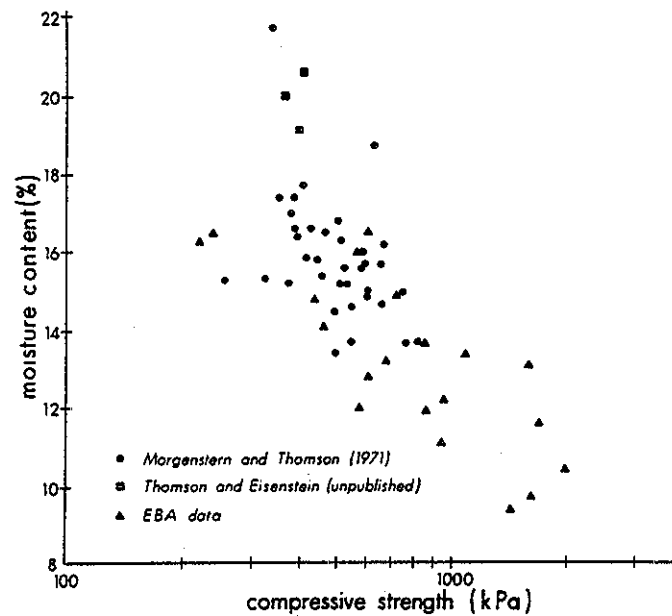


Figure 21. Relationship between natural moisture content and log pocket penetrometer. a) From May and Thomson (1978, p. 368). b) For fine-grained till units in eastern Wisconsin.

by wet sieving, and hydrometer analysis measurements of P200 tend to be greater than those determined by sieving. P200s may be used to check the USCS group symbol.

Wisconsin Geological and Natural History Survey (WGNHS) reports use the sand, silt, and clay divisions indicated in figure 3. Percentages of these particle sizes are reported as matrix percent (that is, percent of the less than 2mm fraction of the sample) to normalize samples collected by different methods because the distribution of particles larger than 2 mm has a much greater spatial variability than the matrix percent in basal till. Furthermore, most sedimentological work uses these sand, silt, and clay classes and they are compatible with terms used in the geologic literature (see Folk, 1958, p. 5). Both sedimentologists and engineers, however, present grain size analysis in graphs of cumulative percent versus grain size diameter. Geologists who study Quaternary materials in Wisconsin adopted use of the textural triangle because early soil surveys placed a greater emphasis on soil parent material.

Considerable geologic interpretation was necessary to assign data to lithostratigraphic units. Frequently, the only type of information common to the definition of the lithostratigraphic units and the geotechnical data was particle size analyses. Discussion of particle size analyses will be limited to till units with observable trends or in which the texture of the matrix can be related to geologic processes or local sources. Sites are consistently identified by

number throughout the figures in part IV, on plate 1, in the appendices, and in the following text.

1. Till of the Middle Inlet Member of the Kewaunee Formation

As noted in the data presentation section, the textural analyses compiled for this study do not always plot within the confidence levels determined by the geologist who originally defined the lithostratigraphic unit associated with the till. For example, in the Middle Inlet Member, only two of the data points fall within the 95 percent confidence interval determined by McCartney (1979). I attribute this difference to the limited area from which data was collected in this study. McCartney based her definition of the Middle Inlet Member on particle size analyses of basal till samples from Marinette and Oconto Counties. Later analyses completed in the Quaternary Laboratory at the University of Wisconsin-Madison for till of the Middle Inlet Member farther southeast more closely resemble the data plotted in figure 8a. Need (1985) reported textural analyses for till of the Middle Inlet Member in Brown County. The mean sand, silt, and clay percentages in Brown County are 40, 40, and 20 for till of the Middle Inlet Member, compared to 22, 47, and 30 at site 24 (32 samples) in this study.

Within till of the Middle Inlet Member in Marinette and Oconto Counties, to the northwest of site 24 (plate 1), McCartney noted an increase in silt content which she attributed to the "incorporation of loess and weathered dolomite over Paleozoic rock in the southeast" (1979, p. 62). McCartney also noted that a similar trend of

increasing carbonate to the south may have the same cause as the increasing silt content to the southeast:

"... the carbonate increases to the south with increasing incorporation of the fine-grained, carbonate-rich material as the ice moved south into the lake-filled basin. This may also be the cause of the increase in silt content to the south" (1979, p. 86).

Initially, interpretation of the stratigraphy at site 24 was blocked by the marked difference between the textures at the site and the published definition. The location of site 24 is between McCartney and Mickelson's (1982) solid line border of the Middle Inlet Member and the Fox River. Site stratigraphy affirms the identification as till of the Middle Inlet Member: the Two Creeks Forest Bed underlies this till at site 24. Site 24 is a good example of how tills of lithostratigraphic units may be identified using the criteria listed in table 1a (stratigraphic position and particle size analysis/texture) and familiarity with the literature.

## 2. Till of the Kirby Lake Member of the Kewaunee Formation

The same deviation from McCartney's statistical summary is seen in till of the Kirby Lake Member, especially at sites 40 and 12 (plate 1 and figure 8b), which are farther south and closer to the Fox River than the type and reference sections. The mean sand, silt, and clay percentages for each site with till of the Kirby Lake Member are presented in table 5 with the number of analyses, N.

McCartney noted that till in the Kirby Lake Member appears texturally to be a reworked lake sediment that experienced little reduction in particle size due to glacial crushing before deposition (1979, p. 55, 73). Another investigator of till in the Kirby Lake

## Till of the Kirby Lake Member

	West							East
Site	38	39	22	23	30	40	41	12
N	24	4	2	4	1	13	1	8
% > 2 mm	7	4	11	40	1	1	7	9
% sand	33	34	33	27	35	3	38	13
% silt	46	45	42	46	51	31	52	40
% clay	21	22	25	27	17	67	11	48

## Till of the Oak Creek Formation

	West							East
Site	55	35	53	21	14	51	52	20
N	7	23	8	16	29	4	2	81
% > 2 mm	16	4	1	2	6	13	0	2
% sand	28	14	11	7	16	21	13	13
% silt	47	56	43	49	50	48	43	59
% clay	25	29	45	44	34	31	45	27

## Till of the Horicon Formation

	North		South	
Site	11	8	13	7
N	5	7	2	8
% > 2 mm	32	17	6	11
% sand	64	51	71	77
% silt	33	36	20	17
% clay	3	14	9	6

## Till of the New Berlin Formation

	West	East
Site	33	36
N	15	3
% > 2 mm	30	18
% sand	64	27
% silt	29	67
% clay	6	6

Table 5. Mean values of % greater than 2 mm, matrix percent sand, matrix percent silt, and matrix percent clay for till units by site. The maximum, minimum, and median are just as important as the mean, and reference to the plot in figure 8b (Kirby Lake Member), figure 9 (Oak Creek Formation), figure 10 (Horicon Formation), and figure 12 (New Berlin Formation) should be made. Site locations are plotted on plate 1.

Member (Piette, 1963) experienced difficulty distinguishing the till from lacustrine sediment even with good field exposures in Brown County. Need characterized till of the Kirby Lake Member as composed of 16% sand, 46% silt, and 38% clay in Brown County (1985, p. 10). This statistical summary is considerably different from the summary determined by McCartney for Marinette and Oconto Counties (and plotted in figure 8b). Like Piette, I found it very difficult to distinguish between massive, clay-rich lacustrine sediment and till in the Kirby Lake Member, and I relied on the sorting evident in complete particle size analyses to distinguish the two.

Assuming that the till in the Kirby Lake Member is indeed reworked glaciolacustrine sediment, it is reasonable to assume that it would become finer in the Green Bay lowland with increasing distance from the ice front. The particle size data summarized above indicates that till of the Kirby Lake Member is much finer in the Green Bay lowland than in Waupaca (sites 38 and 39), Oconto (sites 22 and 23), and Shawano (site 30) Counties to the north and west. Finer-textured till in the Kirby Lake Member should be expected near Lake Winnebago than to the north and west.

### 3. Till of the Glenmore Member of the Kewaunee Formation

Need (1985) and McCartney and Mickelson (1982) present statistical summaries of till in the Glenmore Member that differ by only one percent in the sand and clay fractions. Till of the Glenmore Member is siltier at site 1 and sandier at site 10 with less clay than the mean (plate 1 and figure 8c). Site 1 is in western Brown County



near the Niagaran escarpment and overlies a gray, stony, silty till (possibly the Wayside Member of Need (1985)). Thus, at site 1, the siltier till in the Glenmore Member may be attributed to local incorporation of the underlying silty till. At site 10, in Door County, till of the Glenmore Member is lodged against the Niagaran escarpment of the Door Peninsula. Higher sand content at site 10 may be due to glacial erosion and mechanical weathering of bedrock or to incorporation of sand beaches.

#### 4. Till units of the Chilton, Two Rivers, Valders, Haven, and Ozaukee Members of the Kewaunee Formation

Data for till units of the Chilton, Two Rivers, Valders, Haven, and Ozaukee Members are plotted in figures 8c through 8h. Although some of these particle size analyses plot outside the confidence intervals determined by the geologist who defined the lithostratigraphic units, I could not attribute the differences to geologic process or to provenance. In fact, particle size analyses of till from the Chilton Member are from the northern and southern extremes of the Chilton Member's mapped extent, but the few data do not illustrate trends like those in till units of the west side of the Green Bay Lobe. As previously mentioned, discrepancies between published particle sizes and data compiled here may be due to use of only basal till in the definition of the lithostratigraphic unit.

#### 5. Till of the Oak Creek Formation

Schneider and Need (1985) discuss the texture of glacial sediments in the Oak Creek Formation, but use 0.004 mm as the division

between silt and clay size fractions. Thus, the textural envelope provided by Schneider and Need has not been reproduced in figure 9. Schneider and Need report average grain-size composition of till units equivalent to Oak Creek Formation till units from Wisconsin and Illinois. In Wisconsin, the mean of 68 samples was 12% sand, 44% silt, and 44% clay ( $<0.004$  mm) (Schneider and Need, 1985, p. 58). The very sandy outliers apparent in figure 9 probably represent blocks of sandy sediment locally incorporated into till. Means of sand, silt, and clay for the data plotted in figure 9 are summarized in table 5 by site with left-to-right representing west-to-east. Unlike the particle size analyses for till of the Kirby Lake Member, no clear trend is apparent in till units of the Oak Creek Formation at this scale, and variability at one site, 20, covers nearly the entire range (figure 9). Interbedded silty or sandy sediments and till were recorded as '99' during data collection and were not genetically interpreted.

#### 6. Till of the Horicon Formation

The southern extent of the Horicon Formation has not been geologically studied and divided into members, so few references on particle size analyses are available. The analyses plotted in figure 10 may not be representative of the till because only relatively fine-grained samples would have particle size analyses completed to 0.002 mm for classification purposes at landfill sites. Sand, silt, and clay means are presented in table 5 by site with north to south approximately represented by left to right. Site 11 in Brown County

and probably contains till of the Wayside Member (Need, 1985). Sites 8, 13, and 7 are in Dodge, Green Lake, and Dane Counties, respectively; these sites show a progressive fining to the south. This could result from deposition by a glacier that readvanced over proglacial or post glacial lake sediments in the Green Bay lowland, or it could indicate that debris entrained in the glacier was more thoroughly reduced in size before it was deposited during ice wasting and glacial retreat to the north.

#### 7. Till of the unnamed unit

Particle size analyses of till from sites 12, 24, 40, and 41 in Fond du Lac, Outagamie, and Winnebago Counties (figure 11) demonstrate the existence of a till unit much siltier than expected in the Horicon Formation and stratigraphically below the Kewaunee Formation.

McCartney and Mickelson assert that there are no till units correlative to the Oak Creek Formation till units in the Green Bay lowland (1985, p. 301). Their research did not provide sufficient data to support this contention because it did not extend farther south than the north end of Lake Winnebago. The data compiled for this study are not adequate to test the hypothesis that the sediments at these sites (and possibly at site 1 in Brown County) represent a unit correlative with the Oak Creek Formation in the Lake Michigan basin. In support of this hypothesis, ice in the two lobes seems to have behaved similarly during deposition of the Horicon and New Berlin Formations and during deposition of the Kewaunee Formation as indicated by interlobate moraines and outwash surfaces. I know of no

evidence indicating that ice in the two lobes did not behave similarly during retreat from a middle Woodfordian maximum.

#### 8. Till of the New Berlin Formation

Schneider and Need report the following average texture for till of the New Berlin Formation: 58% sand, 29% silt, 13% clay ( $<0.004$  mm) for 15 samples (1985, p. 58). The envelope they plot for till has not been reproduced in figure 12 because of the difference in size classes. The textures of samples from all the sites contain less clay than those reported by Schneider and Need. Presumably, this is due to the differing definitions of clay since no obvious trend is apparent when data from the three sites are separated. Mean size classes are presented in table 5 with left to right representing west to east. Sites 33, 36, and 55 are in Walworth, Washington, and Waukesha Counties, respectively. The large variation in mean particle size class from site to site may be due to local influences or may result from an unrepresentative, small number of analyses.

#### 9. Till of the Tiskilwa Member of the Zenda Formation

The single textural analysis of till at site 32 (figure 13) indicated a composition between the "typical" (42% sand, 35% silt, and 23% clay) and "sandy phase" (65% sand, 24% silt, 11% clay) (Mickelson *et al.*, 1984, p. A6-6).

## C. Atterberg Limits

### 1. Background

Atterberg limits have been used primarily as an aid to classification in the Unified Soil Classification System (USCS), but this classification is of little use to glacial geologists or to hydrogeologists except in a very general way. Complete particle size analyses give much more information about depositional process than Atterberg Limits as they are determined for use in the USCS. I studied the references available on Atterberg Limits to determine whether the limits and indices derived from them could be of use to hydrogeologists or geologists.

A. Atterberg, a Swedish scientist, established his "limits of consistency" in 1911 in an attempt to classify soils in their plastic state by their water content. Of Atterberg's original six consistency limits, only the liquid limit (LL), plastic limit (PL), and shrinkage limit (SL) have been incorporated into geotechnical practice. The liquid limit is the lower limit of viscous flow, and the plastic limit is the lower limit of the plastic state. (See Casagrande, 1932 for a more detailed summary of Atterberg limits.) Figure 22 illustrates the physical meaning of these three limits. Atterberg also defined the plasticity index as the difference between the liquid limit and plastic limit ( $PI = LL - PL$ ). The ASTM standard method for determining Atterberg limits specifies use of the less than 0.425 mm fraction of the sample (D4318-84, ASTM, 1986).

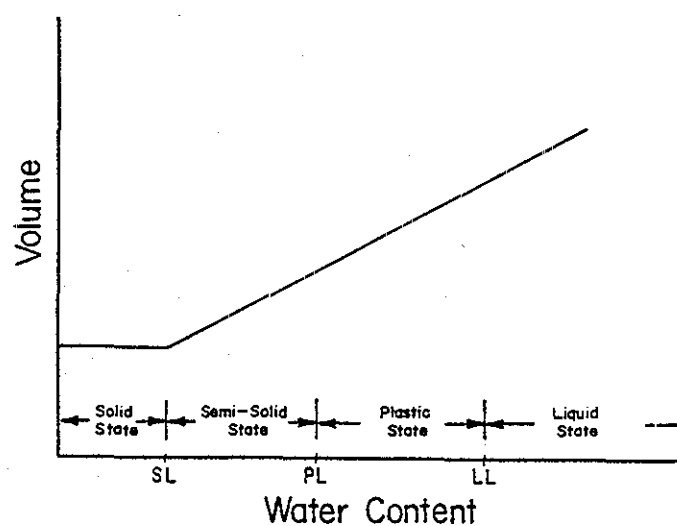


Figure 22. Atterberg limits related to volume and water content. The increase in volume from the shrinkage limit to the plastic limit is part air- and part water-filled void space. The soil is saturated at the plastic limit and increases in volume from the plastic limit consist of water. (From Dunn, Anderson, and Kiefer, 1980, p. 28.)

Atterberg limits have received considerable attention in the geotechnical and soils literature, but are sometimes used inappropriately in contexts for which they were not developed. For example, they have been interpreted to indicate pollutant attenuation potential or cation exchange capacity when too little information is available for such inferences. Atterberg limits have been correlated with compressibility, compactability, shrink-swell, shear strength (ASTM, 1986), specific surface area, geometric properties of clay, physical-chemical factors (Nagaraj and Jayadeva, 1981), organic matter content, percent clay, and clay mineralogy (Odell, Thornburn, and McKenzie, 1960). Farrar and Coleman (1967) found a high correlation between liquid limit and cation exchange capacity and specific surface area. Atterberg limits are influenced by mixing and drying of the sample, particle size distribution, presence of organic matter (Casagrande, 1932), mineralogy, and pore fluid chemistry (Yong and Warkentin, 1975), and a concise interpretation depends on an accurate definition of the variables in the soil-water system. Moreover, the determination of Atterberg limits destroys the soil's structure so that Atterberg limits yield information about material properties which are not necessarily the same as *in-situ* properties.

## 2. Plasticity charts

Casagrande, or plasticity, charts consist of liquid limit on the x-axis and plasticity index on the y-axis. Casagrande plotted an "A-line" on the chart to classify soils. Glacial sediments, like any other sediments, should plot in an elongate cluster parallel to the A-

line. Decreasing particle size within the fraction tested increases both the liquid limit and plastic limit, but increases the liquid limit more (White, 1949). An elongate cluster of data with positive slope results from the variation in particle size distribution within the fractions tested. Muldoon found that increasing matrix percent sand correlated negatively with Atterberg limits (1987, p. 86); the presence of fine sand in the less than .425 mm fraction for the Atterberg limits test suppressed limit values. Chassefiere and Monaco (1983) found the location of sediments along the A-line to be a function of the degree of evolution of the sedimentary facies (sorting) and the smectite content. Figure 23 shows the general relationship between liquid limit and plastic index for several sediment and soil types.

Boulton and Paul (1976) tried to relate Atterberg limits to glacial sediments and introduced a "T-line" for tills which they plot on plasticity charts. Boulton and Paul found that melt out tills occupy a field on the plasticity chart similar to that for englacial debris and lodgement till from the same glacier. Given an understanding of why sediments and soils plot in elongate clusters on a plasticity chart, the T-line is superfluous—especially since it does not differentiate between glacial facies and is not part of a classification system.



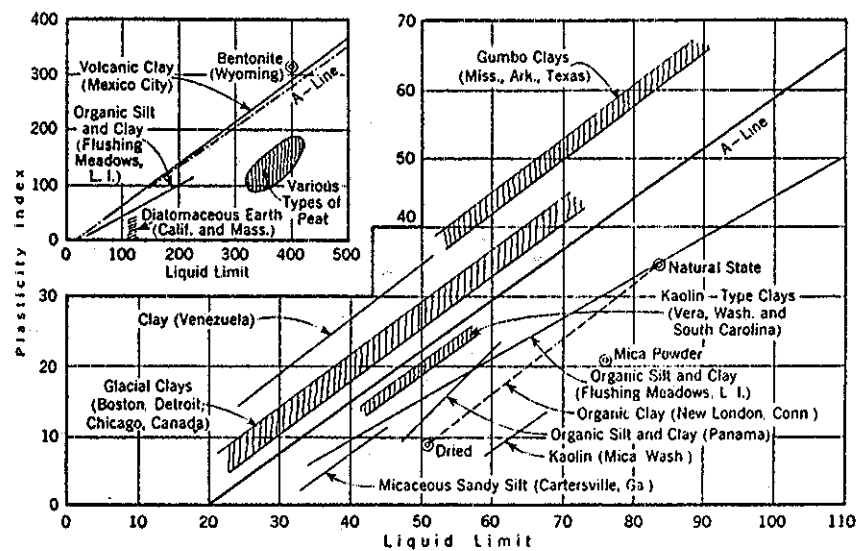


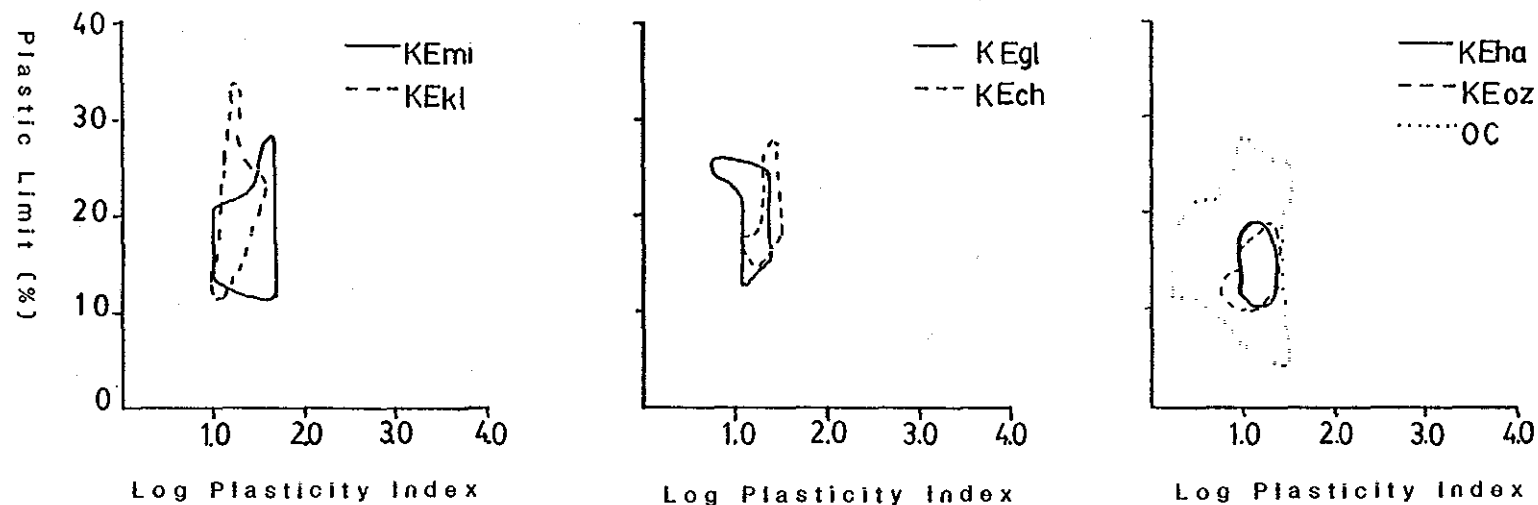
Figure 23. Plasticity chart for a variety of soils. (From Casagrande, 1947, p. 803.)

### 3. Clay mineralogy

Atterberg limits may be related to geology in a way not illustrated by the plasticity chart and have been used to identify clay minerals. For example, Bain (1971) plots plastic limit on the y-axis against plasticity index on a log x-axis to separate clay mineral clusters. Figure 24 shows plots of this type for till units from eastern Wisconsin. Mickelson et al. (1984) report semi-quantitative x-ray diffraction analyses for clay minerals in some of eastern Wisconsin's till units; these are included in the same figure. These plots indicate agreement with published clay mineral analyses. Till in the Oak Creek Formation has the highest illite content and since illite has low plasticity, plots closer to the y-axis. Although clay mineral analyses are not available for the Kirby Lake, Glenmore, and Chilton Members, I infer from the plots that the mineralogy of these till units resembles the other members in the Kewaunee Formation. The influence of fine sand and silt in the less than 0.425 mm fraction complicates interpretation of these plots.

### 4. Activity

Atterberg limits have been used to derive indices in addition to the plasticity index. For example, *activity* is defined as the plasticity index divided by the percent less than 0.002 mm ( $A = PI / \% \text{ clay}$ ). Sediments with activities less than 0.75, between 0.75 and 1.25, and greater than 1.25 are classified as inactive, normal, and active (Grim, 1962). Professionals concerned with the suitability of material for liners and caps would prefer to use materials that are



<u>Till unit</u>	<u>Illite</u>	<u>Exp.</u>	<u>Kaol. + Chlor.</u>	<u>Reference</u>
Middle Inlet Member	49%	33%	19%	Mickelson et al., 1984
Haven Member	56%	25%	19%	Acomb, Mickelson, & Evenson, 1982
Ozaukee Member	60%	20%	20%	Acomb, Mickelson, & Evenson, 1982
Oak Creek Formation	72%	15%	13%	Schneider & Need, 1985

Figure 24. Plots of plastic limit versus log plasticity index for till units in superposed lithostratigraphic units. These plots (after Bain, 1971) indicate agreement with the published clay mineral analysis for till units--only the till in the Oak Creek Formation is considerably different. I infer from the plots that the clay mineralogy of the Green Bay lobe till units in the Kewaunee Formation is similar to those analyzed.

inactive and unlikely to heave or shrink and swell. According to Terzaghi (1955), activity varies with particle size, adsorption complex, and mineralogy. Activities for samples of till with both plasticity indices and percent clay are summarized in table 6. Only till units in the Kirby Lake and Middle Inlet Members of the Kewaunee Formation included samples that were classified as active. These two till units also included proportionally more samples classified as normal. Most of the late Wisconsin till units in eastern Wisconsin are inactive.

Grim (1962) associates the following qualities with active clays: relatively high water holding capacity, high compaction under load, high cation exchange capacity, variation in properties with variation in exchangeable cations, high thixotropy, low permeability, low resistance to shear, and strength dependent on cohesion (p. 219).

Uehara and Gilman find that tropical soils with low activity

" . . . do not shrink or swell greatly, are generally well aggregated, and therefore have higher water intake rates, which in turn reduces hazards from erosion. They can accommodate traffic more readily after heavy rains and offer less resistance to tillage implements than do soils with high-activity clays of comparable textures" (1981, pp. 99-100).

Presumably Uehara and Gilman's observations about activity are not limited to the tropics, and most late Wisconsin till units in the eastern third of Wisconsin are not expected to cause problems for the geotechnical engineer. If Atterberg limits are determined for the entire sample rather than for the fraction less than 0.425 mm, the sample may be classified by its potential for volume change (Dept. of the Navy, 1982, p. 7.1-38).

<u>Till unit</u>	<u>Activity classification</u>				<u>Liquidity index classification</u>				<u>Consistency index</u>		
	<u>N</u>	<u>Inactive</u>	<u>Normal</u>	<u>Active</u>	<u>N</u>	<u>Solid</u>	<u>Plastic</u>	<u>Thixotropic</u>	<u>N</u>	<u>mean</u>	<u>std. dev.</u>
KEmi	23	18	2	3	23	17	6	0	23	1.8	0.8
KEkl	67	51	14	2	67	47	20	0	67	1.6	0.7
KEgl	4	4	-	-	4	4	0	0	4	1.9	0.
KEch	8	6	2	-	8	8	0	0	8	1.9	0.2
KEtr	0	-	-	-	0	0	0	0	0	-	-
KEva	53	48	5	-	53	29	24	0	53	1.3	0.5
KEha	13	12	1	-	13	13	0	0	13	1.9	0.3
KEoz	22	21	1	-	22	5	17	0	22	1.0	0.6
HO	6	6	-	-	6	6	0	0	6	4.1	0.7
OC	106	105	1	-	102	81	21	0	104	2.2	1.4
NB	1	1	-	-	1	1	0	0	1	5.8	-
Zeti	1	1	-	-	1	1	0	0	1	2.9	-

Table 6. Summary of classification using activity and liquidity index with N, total number of samples representing the till of a lithostratigraphic unit, and the number of samples in each category. Summary of consistency index with number of samples per till (N) in a lithostratigraphic unit, mean, and standard deviation.

## 5. Liquidity index

The liquidity index is also derived from Atterberg limits. Liquidity index is defined as the quantity natural moisture content minus plastic limit divided by plasticity index ( $LI = (nm\% - PL) / PI$ ). If the liquidity index is less than 0, between 0 and 1, or greater than 1, then the material is solid, plastic, or thixotropic (regains strength over time), respectively (Chassefiere and Monaco, 1982, p. 174). A high liquidity index is probable in highly porous, fine-grained sediments with high natural moisture. Such conditions might be met by a clay-sized material that flocculated to silt-size sediment—for example, by a water-laid till or lacustrine sediment—but are more likely in an aqueous than a sub-ice environment.

Boswell (1961) associated decreasing liquidity indices with increasing geologic age. He suggested that the liquidity index would be negative in Paleozoic clays and shales and occasionally negative in Cenozoic and Mesozoic clays. Boswell expected glacial and recent clays to have liquidity indices equal to 2.0 or 3.0 (p. 68). In contrast to Boswell, Skempton and Northey (1952) explain that glacially overconsolidated clays don't regain strength because their liquidity index roughly equals zero. Thus, there is no possibility for age-hardening.

Liquidity indices for the till units included in this study are summarized in table 6. As might be expected, most till units were classified as solid, but a significant proportion of the till samples in the Middle Inlet, Kirby Lake, Valdres and Ozaukee Members and in

the Oak Creek Formation are plastic. Since consolidation is really a dewatering process that doesn't affect Atterberg limits (water is added to the sample to determine Atterberg limits), higher liquidity indices should be associated with less well consolidated sediments regardless of their age.

#### 6. Consistency index

Boswell (1961) defines another index derived from Atterberg limits, the consistency index,  $CI = (LL - \% nm) / PI$ . Boswell writes, "In high moisture sediments it becomes zero or negative and tends to increase as deposits become older and to possess lower Atterberg limits" (1961, p. 68). It is clear from the equation that the consistency index approaches zero and negative values when the natural moisture content is high. Values of the consistency index are given in table 6. The consistency index increases with geologic age of the sediments only if the natural moisture content decreases and all the variables affecting Atterberg limits remain constant. The consistency index appears to have no applications for geotechnical engineers or geologists.

#### D. Classification in the Unified Soil Classification System

The only benefit of using the USCS appears to be establishment of a common language among professionals, but lack of a common reference restricts this benefit. I recorded USCS group symbols from grain size curves or descriptions of samples given on lab sheets and from boring log descriptions when a more specific source was not available. Even

though these symbols are "standardized", not all the engineering consulting firms use the USCS in a consistent way. Group symbols are reported combined by hyphens, slashes, commas, and 'and'. The Casagrande chart typically used in textbook descriptions of the USCS shows only one combined symbol, CL-ML, although the ASTM references (D2487-85 and D2488-84) include discussions of when hyphenated symbols and symbols with a slash may be used. The USCS, a revised version of the Airfield Classification (AC) System developed in 1947 by Casagrande, was not specifically intended for hydrogeologic assessment.

A sixty-page discussion of the AC system in Casagrande's 1948 publication documents a variety of misgivings about application of the system for all purposes. In fact, Casagrande emphasized that group symbols are no substitute for detailed descriptions (1948, p. 917). The system was intended for field classification under circumstances such that only manual techniques are practical. Criticisms of the AC system include: that the system ignores fundamental soil properties (Hough, p. 987), that the system is actually a plasticity classification for fine-grained soils and a textural classification for coarse-grained soils (Lane, p. 952), that further confusion of plasticity and consistency would result from its use (Sowers, p. 959), and that it is frequently appropriate to use at least several classifications for describing soils (Spangler, p. 978; all in Casagrande, 1948).



Figure 16 clearly shows that the USCS can not distinguish between till units in the Kewaunee Formation or Oak Creek Formation. The USCS usually does differentiate between outwash and fine-grained till in the Kewaunee and Oak Creek Formations, but does not differentiate between till and outwash in the sandier Horicon Formation. Batches of hydraulic conductivity data for till of lithostratigraphic members have been compared, and ANOVA tests indicate that the hydraulic conductivity values are from populations with statistically significant differences. The USCS does not distinguish between genetic units; thus it gives no clues about geometry of the soil material (on the scale of this study). Neither the USCS nor the lithostratigraphic classification distinguish materials with statistically significant different hydraulic conductivities.

#### E. Hydraulic conductivity

Hydraulic conductivity is the most important material parameter determined during assessment of site conditions for waste disposal systems. Accordingly, assembling available hydraulic conductivity data for the various geologic units has been a major focus of this project. Recompact samples were not included in the hydraulic conductivity data collection because the project focuses on characterization of *in-situ* materials. Other investigators (Muldoon, 1987; Herzog and Morse, 1984; Olson and Daniel, 1981) have reported that various methods of hydraulic conductivity measurement can yield widely varying results, and that laboratory and field measurements of

hydraulic conductivity may vary from each other due to problems of scale and disturbance.

In a thorough review article, Olson and Daniel (1981) list six major causes for higher field than lab hydraulic conductivity:

"(1) a tendency to run laboratory tests on more clayey samples; (2) the presence of sand seams, fissures, and other macrostructures in the field which are not represented properly in laboratory tests; (3) the use of lab  $k$  values back-calculated from consolidation theory rather than directly measured values; (4) measurement of vertical flow  $k$  in the laboratory and horizontal flow  $k$  in the field; (5) the use of distilled water in the laboratory; (6) air entrapment in laboratory samples" (p. 54).

When laboratory and field hydraulic conductivity data compiled for this study are sorted by till units, the laboratory and field data differ by at least an order of magnitude for a combination of all these reasons. Many of the landfill studies are for proposed zone of saturation sites. Thus, consultants may have been concerned with finding a material suitable for use as clay liner material and may have selected finer-grained samples for laboratory testing. Connell (1984) and Fleming (1986) document the existence of fractures and/or joints in the clayey till units included in this study. Written descriptions of samples used for laboratory measurement of hydraulic conductivity almost never include these structures. Relatively few of the lab hydraulic conductivity data were determined using a method derived from Terzaghi's consolidation theory. Olson and Daniel (1982) ascribe the discrepancies between conventional permeability tests and consolidation theory to "... the fact that the classical theory of consolidation makes no adjustment for the structural viscosity of the soil" (p. 25). In contrast, Houston and Kasim (1982) write that the

consolidation test is usually the most satisfactory method for clays with low hydraulic conductivity and high compressibility of the material skeleton (p. 152).

Scale is perhaps the most important factor influencing the differences between lab and field hydraulic conductivity in this study. There is little or no evidence that vertically oriented samples of less than 5 inches diameter taken from a borehole and tested for hydraulic conductivity in a laboratory yield values of vertical hydraulic conductivity appropriate for use in the field at a site of many acres. The fractures and/or joints evident in the field (sometimes identified by gleyed colors, oxidized rims, manganese precipitate, calcite crystals, or silt coats) most likely have a profound, positive influence on vertical hydraulic conductivity and rate of groundwater recharge. These fractures may account for much of the discrepancy between lab and field values.

Unfortunately, neither field nor lab hydraulic conductivity data are suitable for a quantitative comparison of the accuracy of measurement methods. I attempted a two-way analysis of variance test for hydraulic conductivities measured in the laboratory for samples of till from the Oak Creek Formation. Till properties vary from site to site, and I had hoped to determine whether one test method consistently gave higher or lower values at individual sites. However, consistent test methods are usually used at single sites, and two-way analysis of variance requires the same variety of methods at all sites.

Direct comparison of lab and field hydraulic conductivity and comparison of measured hydraulic conductivity with grain size methods of estimating hydraulic conductivity require that the tests and measurements be made on paired samples. Very few lab hydraulic conductivity tests were performed on samples opposite piezometer screened intervals with field test data. Complete grain size data were not available for many samples with hydraulic conductivity data. Muldoon (1987) controlled the selection of samples for testing and was able to regress many variables, including grain size data, against hydraulic conductivity.

#### 1. Field hydraulic conductivity

Using dissimilar sources of hydraulic conductivity data presents several inherent problems. First, the choice between rising and falling head tests could induce variation by a factor of 500 according to Milligan (Houston and Kasim, 1982). Second, several reports included more than one value of hydraulic conductivity for the same well or piezometer, and some values of hydraulic conductivity were determined by Bureau of Solid Waste Management tests and calculations. In these cases, both values are reported in the appendices, but Bureau of Solid Waste Management values were used for the statistical analysis of hydraulic conductivity. Third, a lack of consistently organized raw data in the database prevented consistent recalculation of all hydraulic conductivity values.

The nature of the geotechnical investigations limits the choice of a field method. Many of the piezometers with hydraulic

conductivity determinations are also used to detect changes in static water level or for water quality monitoring. Consultants are reluctant to introduce water to such wells, and prefer to bail down the water level for rising head tests. Thus the removal of the 'slug' of water is not instantaneous. Piezometers with ten-foot-long screened intervals were common. Shorter screened lengths, such as three feet, are preferred for better resolution of head (a 'point' measurement) and to prevent down- and up- hole dilution and/or contamination in the event of leachate movement.

The implementation of field methods has changed rapidly since 1980. In particular, the use of field measurements of hydraulic conductivity has become a legal necessity and improved implementation of the technique may have been concurrent. Most of the data included here are from baildown tests. Whether the same values would result from use of a pressure transducer and continuous recorder is not known. Firms referred to journal articles (Bouwer, 1961; Bouwer and Rice, 1976; Cooper, Bredehoeft, and Papadopoulos, 1967; Papadopoulos, Bredehoeft, and Cooper, 1973) and standard references (Department of the Navy, 1971; Chow, 1964; Freeze and Cherry, 1979; Hvorslev, 1951) to document their methods. These references focus primarily on choice of an appropriate equation for data analysis, and little attention is devoted to the technique of performing the field test, well construction techniques, or analysis of experimental error.

Scarrow (1985) discussed the effect of screen length on field determinations of hydraulic conductivity and concluded that longer

screen lengths give lower values of hydraulic conductivity (pp. 65, 66). The data compiled for this study do not support Scarrow's assertion. Figure 25 indicates that the length of the saturated interval tested does not have a dominant influence on the value of hydraulic conductivity. Scarrow also concluded that "the method chosen to analyze slug test data does not have any measurable impact on the accuracy of the subsequent conductivity estimate" (1985, p. 72). The several orders of magnitude variation seen within till units, then, must reflect variation within the till units according to Scarrow's analysis.

## 2. Laboratory measurements

Laboratory measurements of hydraulic conductivity are used in several phases of the landfill siting and approval process, and it was necessary to read the consultants' reports to determine whether reported laboratory measurements of hydraulic conductivity represented 'undisturbed' conditions. Nearly all the reports lack a description of the laboratory equipment used. The frequent absence of references for the laboratory hydraulic conductivity method used indicates that standard methods for laboratory measurement of natural materials in their native state do not exist. Herzog and Morse (1984) and Muldoon (1987) emphasize description of the laboratory apparatus for this reason. Most laboratory data were labelled as rising or falling head but recompacted samples from clay liners were not always clearly identified. I avoided errors in interpretation of the data by reading the accompanying text. Reading errors could be eliminated by

## Till of the Oak Creek Formation

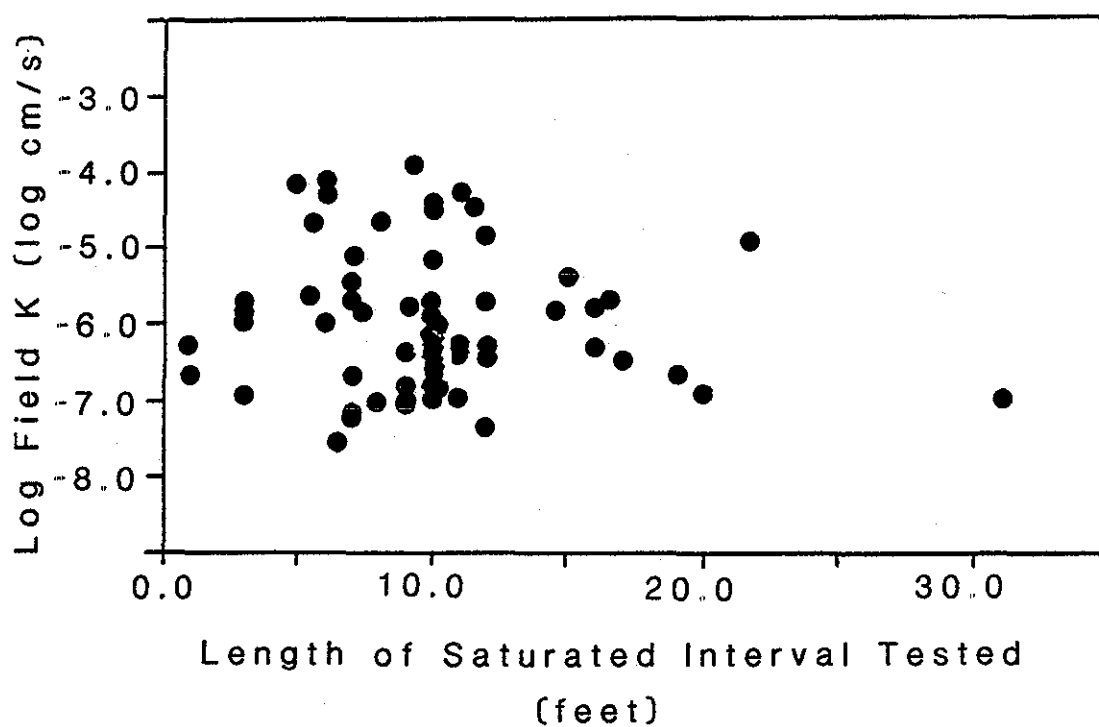


Figure 25. Log hydraulic conductivity from field measurements versus length of the saturated interval tested.

reporting field compacted (liner), lab recompacted, and *in-situ* values in separate columns or tables.

#### F. Dry unit weight

Hydrogeologic assessments do not require determination of dry or moist unit weight but hydrologic use may be made of the data. Materials frequently tested for dry unit weight include potential lining materials for which standard or modified proctor compaction tests are run. The relationship between dry unit weight and porosity should follow weight-volume equations established by soil mechanics theory. The equations of interest are in figure 26. Assuming a specific gravity for the glacial sediment, the void ratio and porosity may be calculated from the dry unit weight. Porosities are needed to calculate average linear velocity and travel times (Feinstein and Anderson, 1987, p. 95).

Samples are typically removed from below the water table. Then, assuming saturation, natural moisture content should equal porosity and be related to void ratio. At low porosity, dry unit weights should be higher. Plotted data illustrate this relationship (figure 26). The straight-line fitted equation explains 80% of the variation in natural moisture content for samples from the Oak Creek Formation. For example, the 95% confidence interval for an individual natural moisture content ranges from 14.9 to 21.7% when the dry unit weight equals 115 pcf. The 95% confidence interval for the *mean* of all natural moisture contents ranges from 17.9 to 18.8% when the dry unit



$$\gamma_d = \frac{G}{1 + e} \quad e = \frac{G * \gamma_w}{\gamma_d} - 1$$

$$e = \frac{n}{1 - n} \quad n = \frac{e}{1 + e}$$

Where:  $G$  = specific gravity, unitless

$\gamma_d$  = dry unit weight, from data

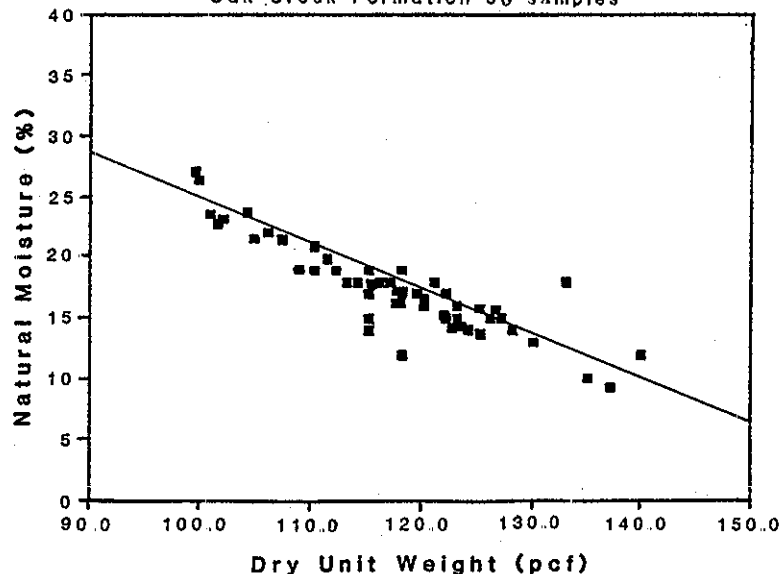
$\gamma_w$  = unit weight of water, 62.5 pcf

$e$  = void ratio

$n$  = porosity

a

**NATURAL MOISTURE VERSUS DRY UNIT WEIGHT**  
Oak Creek Formation 58 samples



b

The regression equation is  
nm % = 60.0 - ( 0.36 \* dry pcf )

	Coef.	Std. dev. of the Coef.	t-ratio
A (y)	60.01	2.82	21.28
b (x)	- 0.36	0.02	-15.15

$s = 1.726$        $R^2 = 80.4\%$        $R^2 \text{ (adj.)} = 80.0\%$   
The t-value corresponding to 56 degrees of freedom and 95% confidence is 1.96.

Figure 26. a) Equations for the calculation of porosity from dry unit weight. Specific gravity is usually estimated as 2.65 (Dunn, Anderson, and Kiefer, 1980, p. 19). b) Natural moisture versus dry unit weight.

weight equals 115 pcf. A regression of dry unit weight on natural moisture content also indicates a statistically significant relationship. The regression results are included in figure 26.

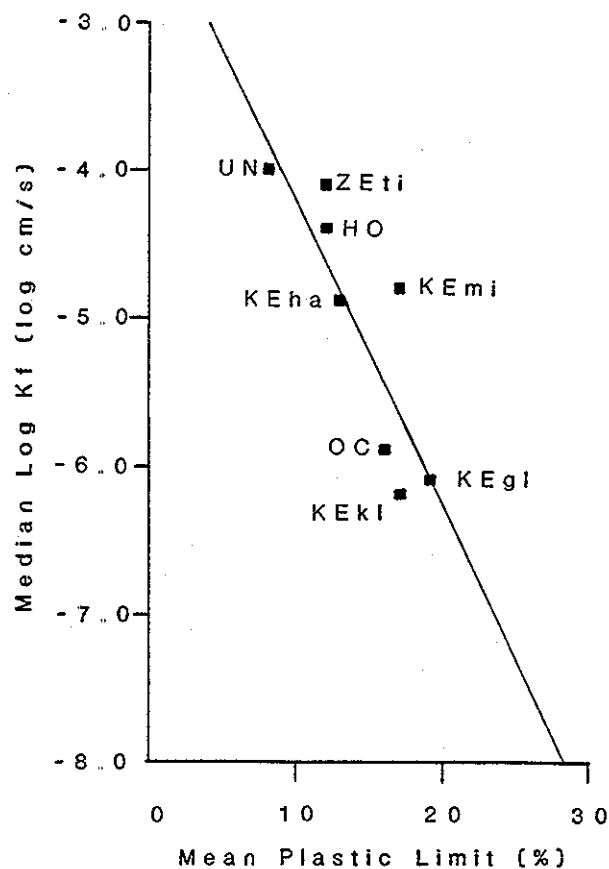
G. Relationships between hydraulic conductivity and other tests.

As previously stated, investigation of the relationship between textures and hydraulic conductivity using correlation and regression is not possible because the data are not paired. For the same reasons, exploratory data analysis of relationships between hydraulic conductivity and other data parameters is limited to plots of median values for lithostratigraphic units.

1. Hydraulic conductivity and plastic limit

Previous work suggests that a relationship may exist between plastic limit and hydraulic conductivities measured in the field. Connell (1984) observed a weak negative correlation between plastic limit and the frequency of vertical joints. A good correlation between the log of hydraulic conductivities measured in the field and plastic limit would be expected if a relationship exists between plastic limit, fracture frequency, and field hydraulic conductivity in these data. I plotted the median value of hydraulic conductivities measured in the field versus the mean plastic limit for till units with more than 5 values of each.

Although the data in figure 27 appear to illustrate a trend and the straight line regression equation explains 67% of the variation in log median hydraulic conductivity measured in the field, the



The regression equation is

$$\text{Log } K_f = -2.14 - (0.206 * \text{PL})$$

	Coef.	Std. dev. of the Coef.	t-ratio
A (y)	-2.14	0.779	-2.75
B (x)	-0.21	0.053	-3.88

$$s = 0.509 \quad R^2 = 71.4\% \quad R^2 (\text{adj.}) = 66.7\%$$

The t value corresponding to 6 degrees of freedom and 95% confidence is 2.45.

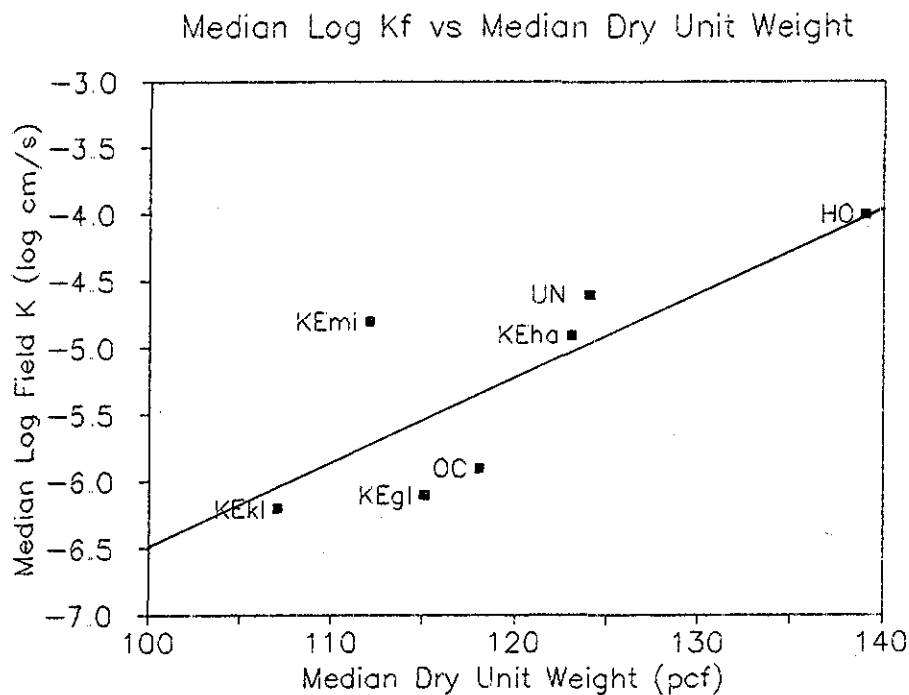
Figure 27. Regression of median log hydraulic conductivity measured in the field on mean plastic limit.

relationship has limited practical applications because medians and means are used. Despite this, the results of the statistical analysis can be used to predict field hydraulic conductivity from plastic limit. For example, the 95% confidence interval for a single hydraulic conductivity (median) value when (mean) plastic limit equals 17% ranges from  $5.0 \times 10^{-5}$  to  $1.0 \times 10^{-7}$  cm/s.

## 2. Hydraulic conductivity and dry unit weight

Hydraulic conductivity is intuitively related to dry unit weight (bulk density) because fluid flow requires permeability and porosity, and more porous soils are expected to have lower bulk density. Porosity and hydraulic conductivity are commonly thought to be related, especially in granular porous media: porosity is included in the parameter 'C' in Darcy's equation and as 'n' in the Kozeny-Carmen and Fair-Hatch equations (Freeze and Cherry, 1979, pp. 27, 351).

I plotted median field hydraulic conductivity against median dry unit weight for each till unit with greater than five data values to determine whether such a relationship deserves further attention (figure 28). (Like many other parameters in the database, measurements of hydraulic conductivity and density are not paired.) The median dry unit weights are lower for finer grained till units with higher natural moisture contents, as suggested by figure 26b for sediments in the Oak Creek Formation. High porosity is associated with fine-grained materials but high porosity does not always result in greater values of hydraulic conductivity. High permeability is



The regression equation is

$$\text{Log } K_f = -13.0 + (0.065 * \text{dry pcf})$$

	Coef.	Std. dev. of the Coef.	t-ratio
A (y)	-12.96	2.67	-4.85
B (x)	0.06	0.02	2.91

$$s = 0.569 \quad R^2 = 62.8\% \quad R^2 (\text{adj.}) = 55.4\%$$

The t value corresponding to 5 degrees of freedom and 95% confidence is 2.56.

Figure 28. Regression of median log hydraulic conductivity measured in the field on median dry unit weight for till units.

required in addition to high porosity for high hydraulic conductivity. Figure 28 indicates that coarser-grained units have greater permeability. The poor fit of the regressed equation confirms that multiple variables influence the value of hydraulic conductivity.

According to straight-line linear regression results, 55% of the variation in median log hydraulic conductivity from field measurements can be explained by the fitted equation. As was the case for plastic limit, the regression of median log hydraulic conductivity on median dry unit weight has limited practical applications. For example, the 95% confidence interval for a single median hydraulic conductivity field measured value corresponding to a dry unit weight of 112 pcf ranges from  $1.1 \times 10^{-4}$  to  $3.5 \times 10^{-8}$  cm/s. A more narrow range of values can be predicted for the mean median log hydraulic conductivity at a given dry unit weight (Ryan, Joiner, and Ryan, 1985, p. 233).

### 3. Hydraulic conductivity and pocket penetrometer measurements

I also investigated the relationship between hydraulic conductivities measured in the field and pocket penetrometer measurements because pocket penetrometer data has been thought to indicate density. A similar correlation coefficient ( $r^2=0.64$ ) resulted from a straight line linear regression of the median log field hydraulic conductivity on the median pocket penetrometer measurement for till units. Despite the value of  $r^2$ , statistical analysis (a t-test of the null hypothesis that  $B=0$  (Ryan, Joiner, and Ryan, 1985, p. 292)) implies that the pocket penetrometer is not a

useful predictor of log hydraulic conductivities measured in the field.

#### H. Relationships between lithostratigraphic units and hydrostratigraphic units

Laney and Davidson (1986) discuss the definition of the hydrogeologic framework in much the same way as Mickelson *et al.* (1984) discuss the lithostratigraphic framework. Laney and Davidson write:

"In hydrogeologic studies, as in purely geologic investigations, the orderly, consistent designations of pertinent parts of the geologic framework is essential to a clear reporting and understanding of the study results. In ground-water studies, this involves definition and correlation of water-yielding rock materials, and relating those rock materials to established rock-stratigraphic units" (p. 9).

In this study, the hydrologic and geotechnical properties of till units were emphasized although data for both local and extensive sand and gravel bodies and till units were compiled.

Till units function as aquifers or aquitards depending on local conditions that frequently are a function of the unconformities and depositional environments noted in sections II-D and III-A. The till units are heterogeneous since hydraulic conductivity values at separate sites differ significantly within a single till and since a wide range of values is present at single sites.

Similarly, Feinstein and Anderson (1987) did not use formal lithostratigraphic units but did use genetic terms to define hydrostratigraphic units in Brown County, within the area glaciated by the Green Bay Lobe in late Wisconsin time. Feinstein and Anderson

divided till of single lithostratigraphic units into separate hydrostratigraphic units (clayey, loamy, or stony till; clayey or silty lacustrine; silty sand; sand, gravel, some silt) on the basis of piezometer tests of hydraulic conductivity. That approach was not possible for this study because the entire study area has not been mapped in the same detail as Brown County was by Need (1985). The lack of control over placement of piezometers also restricted application of this approach. Feinstein and Anderson combined Need's map units into hydrostratigraphic units.

#### I. Recommendations for sampling and testing procedures

Following Laney and Davidson's lead, I recommend that both geologic interpretation (genesis) and USCS classification be required on boring logs. The USCS can provide a common language for communication of observations if a standard reference is used, such as ASTM D2488-84 (ASTM, 1986, pp.411-424), and it provides information of interest to geotechnical engineers. The geologic interpretation is critical to inferences regarding the geometry of the materials. Use of the USCS alone to identify major soil layers and to determine the number of samples required means that two till units or a till unit and a clayey lacustrine unit could be present at one site, but only one would be sampled. Complete particle size analyses are necessary for geologic interpretation. Thorough description of samples, including notes on lithologies, structures, mottling, evidence of leaching, reaction, staining, and Munsell color would aid



identification of lithostratigraphic units considerably. Continuous sampling methods and continuous cores are preferable to split spoon samples at five foot intervals because continuous samples are more likely to indicate the presence of small sand layers affecting the flow of groundwater.

The variability of field measurements of hydraulic conductivity within one till requires further investigation. Error analysis of hydraulic conductivities requires documentation of sampling, measurement, and calculation methodology. Placement of the screened interval of a piezometer should be within only one genetic unit. Piezometers screened in silty or sandy sediments and finer-grained till units probably result in values of hydraulic conductivity representative of the non-till sediments. Until thorough error analysis of hydraulic conductivity tests has been completed, short piezometer screens located in one genetic unit are preferred. A carefully designed experiment should be completed to assess the effects of different field measurement techniques.

Several methods for the calculation of hydraulic conductivity from field tests require selection of data points and regression of a best-fit least-squares line. The selection of data points introduces individual bias to test results. Muldoon (1987) and Feinstein and Anderson (1987) calculate hydraulic conductivity between each recorded measurement during a field test, then report a geometric mean for the entire test. This reduces the subjectivity of data interpretation, but the method would be more resistant to the influence of very high

initial changes in head (possibly caused by the well screen's sand pack) if the median value rather than the mean is reported.

Throughout the data collection phase of this study, I was impressed with the number of borings completed at individual sites. I was also surprised by how few tests of hydraulic conductivity and complete grain size analyses are completed. Presumably, a large number of borings will provide data necessary to assess on-site stratigraphy, but the boring descriptions yield little information about hydraulic conductivity. The purpose of the geotechnical investigation is to determine the hydrogeologic setting and availability of suitable materials for landfill construction, but remarkably few hydrogeologic data results. This study indicates that there is a great deal of on-site variability, and the three values of hydraulic conductivity required by Wisconsin Administrative Code NR 180.13 for each major soil layer do not necessarily represent the range in hydraulic conductivity of a single stratum. Many of the data used in this study resulted from remedial action investigations at sites established prior to 1980. In modern waste disposal, the engineering design of sites is emphasized and relied upon to protect groundwater and surface water from contamination. These engineered sites have been in operation for a relatively short time and have provided geotechnical surprises in terms of gas build-up, leachate generation, and settlement. Incorporation of site-specific data into a more regional context can help resource managers anticipate problems at sites that otherwise seem to have nothing in common.

## VI. Summary and Conclusions

### A. Summary

This study was carried out in response to the long term objectives listed in the introduction. Compilation of the database used in this study addressed the first objective, to identify the hydrogeologic and geotechnical properties of Pleistocene materials in eastern Wisconsin. Hydraulic conductivity values, particle size analyses, Atterberg limits, approximations of strength, and dry unit weights have been compiled from reports on file at the Wisconsin Department of Natural Resources and assigned to one of five formations (one formation includes ten lithostratigraphic members) in eastern Wisconsin.

Association of the data with extensive lithostratigraphic units that have been associated with mapped ice margin positions partially meets the second objective--to associate the properties with mappable, extensive hydrostratigraphic units that can be identified in the field. The lithostratigraphic units are characterized with values of hydraulic conductivity, but are not divided into hydrostratigraphic units. No hydrostratigraphic units are designated because sources of data are not evenly distributed throughout the units and because an appropriate scale for the definition of hydrostratigraphic units has not been defined.

The data have been statistically analyzed to assess the variability and expected range of values within the individual till

units, accomplishing the third objective. Several till units are demonstrably heterogeneous, both with respect to grain size and to hydraulic conductivity, and statistically significant differences within a single till are documented.

The fourth objective is to develop field and laboratory methodologies for the evaluation of hydrogeologic and geotechnical properties in previously untested areas. Several recommendations follow the conclusions.

#### B. Conclusions

This study leads to the following general conclusions.

1. The quality of geotechnical investigations has improved in response to recent modifications of Wisconsin Administrative Code. However, the three values of hydraulic conductivity required by Wisconsin Administrative Code Chapter NR 180 for each major soil layer do not necessarily represent the range in hydraulic conductivity and grain size of a single stratum at a single site. This study indicates that more testing of samples is necessary for characterization of variability.
2. Field measurements of hydraulic conductivity in one of the most variable tills, the till in the Middle Inlet Member, range from  $10^{-7}$  to  $10^{-3}$  cm/s while less variable tills such as the till in the Haven Member range over only two orders of magnitude.
3. Median field measurements of hydraulic conductivity are at least an order of magnitude greater than laboratory measurements in fine-

grained till units. In coarse-grained till units, median field measurements of hydraulic conductivity are half an order of magnitude greater than the median laboratory measurements.

4. Compilation of geotechnical data makes it more accessible and provides a reference database. Incorporation of site-specific data into a more regional context can help resource managers anticipate problems at sites that otherwise seem to have nothing in common.

5. Particle size analysis to .002 mm is necessary for confident determination of sediment genesis. Geologists should provide complete grain size curves in addition to textural classification so that individuals familiar with other classifications can use geologic data. Textures of till samples from specific sites deviate from the published lithostratigraphic definition, but in some cases consideration of local sediment sources and glacial processes may explain the deviation.

6. Geotechnical index tests, such as Atterberg limits, can be used as lithic criteria to characterize lithostratigraphic units, but like other criteria used by geologists, can not distinguish lithostratigraphic units in all cases.

7. Atterberg limits plotted on plasticity charts do not distinguish till units from each other. Glacial sediments plot in elongate clusters on a plasticity chart. Most till units in the study are "inactive" and "solid," but some are "normal" and "plastic."

8. No meaningful relationships were found between standard penetration test data and depth or pocket penetrometer measurements.

The pocket penetrometer correlations found by previous investigators were not corroborated in this study.

9. Dry unit weight data may be used in calculations of void ratio, porosity, and average linear velocity of advective flow. A weak linear relationship exists between median log hydraulic conductivity measured in the field and median dry unit weight for till units.
10. Values of plastic limit may be used to constrain the predicted range in values of hydraulic conductivity measured in the field for till units.
11. Incorporation of more refined genetic terms into a geotechnical and hydrogeologic data base like the one used in this project could provide data for facies models and perhaps improve prediction of hydrogeologic conditions at sites prior to investigation.

#### C. Recommendations

1. All new data submitted to DNR for report approval should be compiled in a summary form similar to the database used for this study.
2. Data in geotechnical reports would be more easily accessed if boring locations were reported using a global coordinate system that follows simple, consistent rules of orientation. If only 3 points at each site had global coordinates, the remainder could be easily digitized.
3. More than one classification system (USCS, geologic, and possibly

others) should be used to describe samples with standard terminology from a reference cited in Wisconsin Administrative Code.

4. Shorter piezometer screens should be installed to improve point measurements of hydraulic head and to avoid potential movement of contaminants between units. Piezometers should be screened in only one genetic unit.

5. Standard references for determining the hydraulic conductivity of undisturbed fine-grained samples in the laboratory should be developed if such tests continue to be used. Laboratory values of hydraulic conductivity are of questionable value to hydrogeologic assessments of *in-situ* conditions.

6. No improvement in the precision of hydraulic conductivity testing should be expected until the experimental error and variation in field tests has been analyzed. Without such an analysis, the variation in hydraulic conductivity values is usually attributed to variation in the materials tested. To test this assumption, a carefully designed experiment should be completed in which data are recorded from field tests that use different methods of lowering and raising the water level in correctly placed and constructed piezometers and different methods of recording the data (continuous strip recorders vs. taped measurements). If one aspect of the experiment is changed while holding all others constant, values of hydraulic conductivity could be statistically analyzed using two-way analysis of variance. The method of calculating hydraulic conductivity from field test data should be

standardized, and a variation of the method reported by Muldoon (1987) could be used.

7. A more refined definition of hydrogeologic units requires complete definition of the lithostratigraphy, particularly in the central portion of the Green Bay lowland (from Green Bay to south of Lake Winnebago). Units of extensive lake sediments and outwash should be mapped in the areas glaciated by the Green Bay and Lake Michigan lobes.



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- Yong, R. and B. Warkentin (1975). "Soil properties and behaviour." Developments in geotechnical engineering 5. Elsevier Scientific Publishing Company, New York.

## Appendix 1 Data required by Wisconsin Administrative Code

NR 51.10 (1)(c) states that

"A report shall accompany the plans indicating: . . . (3) Geological formations and ground water elevations to a depth of at least 10 feet below proposed excavation and lowest elevation of the site. Such data shall be obtained by soil borings or other appropriate means."

The same phrasing was used in NR 151.10(1)(c); apparently, only the numbering was changed.

NR 151.12(5) (1976) indicates growing concern in the Department of Natural Resources and reflects the influence of federal and state statutory laws. The requirements for geotechnical information are more specific:

NR 151.12(5)(c): "An acceptable report on geological formations based on soil borings. The minimum number of borings to be taken is based on site size according to the following schedule:

1. 3 borings for a site of up to 5 acres in size.
2. 1 boring for each additional 5 acres or portion thereof up to 50 acres.
3. 1 boring for each additional 10 acres or portion thereof over 50 acres.

Borings shall be arranged as nearly as possible to form a grid pattern over the site, to provide a subsurface investigation representing the entire site, and to facilitate analysis. When information is insufficient to adequately evaluate the site, additional deeper borings may be required. All borings shall extend to a depth of at least 15 feet below the lowest proposed elevation of waste disposal in the areas of the borings. Boring holes shall be refilled with a bentonite-earth slurry prior to disposal of solid waste." (Register, June 1976, No. 246, Environmental Protection, p. 118-2)

Both NR 51 and NR 151 required only one phase of investigation prior to site development. As the expense of more detailed investigations became a factor, the code changed to require two phases of investigation--initial site reports (ISRs) and feasibility reports,

completed at different levels of detail--prior to approval and prior to further investment in the proposed site.

NR 180 (1980) requires that submitted ISRs and feasibility reports be prepared in the following manner: under the direction of a registered professional engineer, using standard procedures approved by the department, in a standard format, using a site-specific grid and containing appendices listing all references, all necessary data, procedures, and calculations (Register, February, 1980, No. 290, Environmental Protection, pp.686-9 to 10). Both initial site and feasibility reports must contain regional geotechnical information including topography, hydrology, geology, hydrogeology, and water quality (Register, March, 1984, No. 339, Environmental Protection, p. 686-34). The code clearly states the minimum field and lab investigations required for a feasibility report:

NR 180.13(6)3a.: "Sufficient soil borings to adequately define the soil, bedrock, and groundwater conditions at the site. Under most site conditions, 5 soil borings for the first 5 acres and 3 borings for each additional 5 acres or portion thereof should be performed. A lesser number of borings may be made based on specific site conditions and site design. The borings shall be located in a grid pattern such that there is a minimum of one boring in each major geomorphic feature (e.g. ridges, lowlands and drainage swales). All borings shall extend a minimum of 25 feet below the anticipated site base grade or to bedrock, whichever is less."

NR 180.13(6)3b.: "Where soil conditions permit, soil samples shall be collected utilizing standard undisturbed soil sampling techniques. Samples shall not be composited for testing purposes. Soil samples shall be collected from each major soil layer encountered and at maximum 5-foot intervals. All soil samples shall be described."

NR180.13(6)3c.: "Boring logs shall be recorded for all borings. Each log shall include soil and rock descriptions and method of sampling, sample depth, date of boring, water level measurements and dates, and soil test data. All elevations shall be corrected to USGS datum."

NR180.13(6)3d.: "For each major soil layer encountered, at least 3 soil samples shall be analyzed for grain size distribution (mechanical and/or hydrometer as appropriate to the soil type) and classified according to the unified soil classification system."

NR180.13(6)3e.: "A minimum of 3 permeability tests shall be conducted for each major soil layer. At least one of the 3 tests shall be performed utilizing in-field testing procedures."

NR180.13(6)4a.: "All raw data such as boring logs, well logs, soil tests and water level measurements shall be included in the report appendix."

(Register, February, 1980, No. 290, Environmental Protection, pp. 686-36 to 686-37)

In addition to the data collection outlined above, the BSWM requires an investigation to document the availability of a suitable fine-grained material for use as a recompacted liner if no fine-grained sediment is available on-site. These "clay liner investigations" typically include boring logs of the same quality as required for feasibility reports and complete grain size analyses.

## Appendix 2 Location summary by site: latitude and longitude

Site #	minimum latitude	maximum latitude	minimum longitude	maximum longitude	default latitude	default longitude
1	443021	443029	875010	875045	443099	875099
2	443041	443103	880913	880940	443099	880999
3	442409	442439	880019	880059	442499	880099
4	443142	443153	875949	880016		
5	440609	460619	881128	881137		
6	430434	430445	891142	891156		
7	430105	430131	892007	892055		
8	431854	432333	885133	890145	432399	885299
9	432729	432808	883304	883335		
10	445145	445150	872638	872709		
11	452305	452310	835608	865304	452399	865399
12	434917	434932	883138	883201		
13	435728	435744	885426	885452	435799	885499
14	423506	423550	880213	880247		
15	442822	442835	873440	873515		
16	441004	441046	874937	875012	441099	874999
17	451411	451429	880532	880542	451499	880599
18	not assigned					
19	434703	434716	892841	892858		
20	425007	425031	875017	875052	425099	875099
21	425037	425112	880329	880410	425199	880499
22	445142	445154	880923	880940		
23	443921	445026	880602	881027		
24	441717	441755	882003	882107	441799	882199
25	432141	432151	875427	875429		
26	432539	432600	875104	875121		
27	432647	432702	875138	875156		
28	424218	424240	875120	875154		
29	432041	432247	894250	894557	432199	894499
30	444608	444821	883330	883345	444699	883399
30	(Clay source)				444899	883699
31	434136	434157	874703	874725		
32	424529	424610	882440	882511	424699	882599
33	413918	423910	884305	884329	423999	884399
34	431744	431756	881128	881158		
35	431115	431157	880315	880453	431199	880499
36	431747	431755	881037	881041		
37	430245	450258	880847	880911		
38	442621	442630	885822	885837		
39	442017	442034	885655	885706		
40	440500	440523	883215	883327	440599	883399
41	470330	470354	883327	883407	470399	883499

41-49 not assigned. Bill Simpkins provided data for sites 50-55.

50	425145	425216	875041	875106
51	425206	425215	875245	875258
52	425503	425524	875152	875201
53	425115	425131	880246	880452
54	425005	425029	875019	875050
55	425324	425356	881029	881109

Appendix 2 Location summary by site: topographic quadrangle,  
section, township, & range

<u>County</u>	<u>Site</u>	<u>Site name</u>	<u>7.5' map name</u>	<u>Sec., Township, &amp; Range</u>
Brown	1	Baeton	New Franken	Sec. 33, T24N, R22E
Brown	2	Decaster	Oneida North	Sec. 25 & 26, T24N, R19E
Brown	3	Decleene	DePere	Sec. 1 & 6, T23N, R20&21E
Brown	4	Northland Sludge	Green Bay E. and W.	T24N, R21E
Calumet	5	Calumet Co. LF	Chilton	Sec. 23, T19N, R19E
Dane	6	Hydrite Chemical Corp.	Cottage Grove	Sec. 16, T7N, R10E
Dane	7	Libby Road	Madison East	Sec. 32, T7N, R10E
Dodge	8	Carl Schmitt	Lost Lake	Sec. 30, T11N, R14E
Dodge	9	Hechimovich & clay source	Mayville South	Sec. 35, T12N, R16E
Door	10	Door Co. Balefill	Sturgeon Bay West	Sec. 34, T28N, R25E
Door	11	Town of Washington	Washington Island NW	Sec. 32, T34N, R30E
Fond du Lac	12	Eldorado	Eldorado	Sec. 25, T16N, R16E
Green Lake	13	Green Lake Co. LF	Berlin	Sec. 11, T17N, R13E
Kenosha	14	Pheasant Run	Paddock Lake	Sec. 32, T2N, R21E
Kewaunee	15	Kewaunee Co. LF	Kewaunee	Sec. 9, T23N, R24E
Manitowoc	16	Lemberger	Whitelaw	Sec. 26, T20N, R22E
Manitowoc	16	Proposed Co. LF	Whitelaw	Sec. 26, T20N, R22E
Manitowoc	16	Ridgeview	Whitelaw	Sec. 26, T20N, R22E
Marinette	17	Proposed Co. LF	Crivitz	Sec. 23, T32N, R19E
	18	not assigned		
Marquette	19	Marquette Co. LF	Packwaukee	Sec. 8, T15N, R9E
Racine	20	Caledonia (WEPCO)	Racine North	Sec. 1, T4N, R22E
Milwaukee	21	Metro	North Cape	Sec. 31, T5N, R21E
Oconto	22	City of Oconto Falls	Oconto Falls South	Sec. 35, T28N, R19E
Brown	23a	Oconto Co. LF	Pulaski	Sec. 11, T25N, R19E
Oconto	23b	Oconto Co. LF	Abrams	Sec. 5, T27N, R20E
Oconto	23c	Oconto Co. LF	Pulaski	Sec. 35, T26N, R19E
Outagamie	24	Outagamie Co. LF	Kaukauna	Sec. 7, T21N, R18E
Ozaukee	25	Anderson ISR	Cedarburg	Sec. 5, T10N, R22E
Ozaukee	26	Didier ISR	Port Washington East	Sec. 10, T11N, R22E
Ozaukee	27	WEPCO ISR	Port Washington East	Sec. 4, T11N, R22E
Racine	28	Land Reclamation	Racine South	Sec. 23, T3N, R22E
Sauk	29	Badger Army Amm. Plant	Baraboo	Sec. 6, T10N, R7E
Sauk	29	Badger Army Amm. Plant	Sauk Prairie	Sec. 14, T10N, R6E
Sauk	29	Badger Army Amm. Plant	Sauk City	Sec. 1 & 14, T10N, R6E
Shawano	30	Shawano Co. LF	Shawano	Sec. 19 & 33, T27N, R16E
Sheboygan	31	Sheboygan Co. LF	Sheboygan Falls	Sec. 7, T14N, R23E
Walworth	32	East Troy	East Troy	Sec. 31, T4N, R18E
Walworth	33	Greidanus	Delavan	Sec. 4 & 9, T2N, R15E
Washington	34	Mertens ISR	Jackson	Sec. 25, T10N, R19E
Washington	35	Omega Hills	Menominee Falls	Sec. 36, T9N, R20E
Waukesha	35	Omega Hills	Menominee Falls	Sec. 1, T8N, R20E
Washington	36	Schowalter ISR	Jackson	Sec. 30, T10N, R20E
Waukesha	37	Brookfield	Waukesha	Sec. 20, T7N, R20E
Waupaca	38	Kempf	Manawa	Sec. 30, T23N, R13E
Waupaca	39	Town of Royalton	Weyauwaga	Sec. 32, T22N, R13E

Winnebago	40 Bartlett	Oshkosh	Sec. 26, T19N, R16E
Winnebago	41 Winnebago Co. LF	Oshkosh	Sec. 2 & 3, T18N, R16E
Milwaukee	50 Bender Park	Racine North	Sec. 25, T5N, R22E
Milwaukee	51 Derosso ISR	Franksville	Sec. 27, T5N, R22E
Milwaukee	52 Falk LF	S. Milwaukee	Sec. 2, T5N, R22E
Waukesha	53 Future Parkland	North Cape	Sec. 36, T5N, R20E
Milwaukee	54 WEPCO2	Racine North	Sec. 1, T4N, R22E
Milwaukee	55 Muskego	Muskego	Sec. 18, T5N, R20E

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Bill Simpkins collected data for sites 50-55.

ISR stands for initial site report.

LF stands for landfill.



## APPENDIX 3 DATA REFERENCES AND DATA

Site 1

Donohue and Associates, Inc. (1980). Initial site report for Wisconsin Public Service Baeton Site STS Job 81085.

Donohue and Associates, Inc. (1982). Feasibility report for Wisconsin Public Service Baeton Site. STS Job 11119-A.

Site 2

Robert E. Lee and Associates (1973). Soils investigation for cell DC 3.

\_\_\_\_\_ (1974). Soils investigation for cells DC 4 and DC 5.

Soils Testing Services, Inc. (1978). Soils report for Module 2. Job 8929.

Foundation Engineering, Inc. (1976). Subgrade and earth berm data and in place subgrade data. Job FE 76157.

Foundation Engineering, Inc. (1979). Northern periphery of module 1 and southern periphery of module 2. Supplemental soils investigation. Job 7913.

Site 3

Brown County Brown County East Landfill monitoring well inventory.

Soil Testing Services (1983). Plan of Operation Approval Conditions.

Robert E. Lee and Associates (1984). Plan of Operation.

Site 4

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Site 5

Robert E. Lee and Associates, Inc. (1981). Calumet County initial site report - Behnke property. STS borings, Job 11513.

\_\_\_\_\_ (1982). Calumet County feasibility report - Behnke property. STS Job 11513A.

Site 6

Warzyn Engineering, Inc. (1982). Preliminary in-field conditions report Hydrite Chemical Company solvent processing facility, Cottage Grove, Wisconsin. Includes data from jobs C9555 and C10497.

Warzyn Engineering, Inc. (1983). Phase II subsurface investigation Hydrite Chemical solvent processing facility, Cottage Grove, Wisconsin. Job C10834.

Warzyn Engineering, Inc. (1984). Report to Hydrite dated Jan. 9, 1984 including pump test results from Roy F. Weston, Inc..

Site 7

Residuals Management Technology, Inc. (1986). Madison Landfills, Inc. - Libby site.

Site 8

Warzyn Engineering, Inc. (1984). Feasibility study. Job C10863.

Warzyn Engineering, Inc. (1982). Addendum to the initial site report. Job C9670B.

Warzyn Engineering, Inc. (1981). Initial site report. Job 9670.

Warzyn Engineering, Inc. (1985). Clay soils investigation, Carl Schmidt landfill, Town of Lowell, Dodge County, Wisconsin. Job 10863.

Site 10

Soil Testing Services of Wisconsin, Inc. (1980). Hydrogeologic study for proposed Door County landfill. STS Job 8774.

Robert E. Lee and Associates (1979). STS borings.

Becher-Hoppe Engineers, Inc. (1973). Idlewood project, Sturgeon Bay, Wisconsin. STS borings.

Site 11

Becher-Hoppe Engineers (1977). STS grain size analyses, 1976-1977.

Site 12

Foth and Van Dyke and Associates, Inc. (1983). Feasibility study, Job FU 8301. Twin City Testing logs.

Foth and Van Dyke and Associates, Inc. (1985). Addendum to the Feasibility study. Job FU 8301. Twin City Testing logs.

Site 13

Foth and Van Dyke and Associates, Inc. (1982). Feasibility report for the proposed Green Lake Landfill, Inc. horizontal expansion.

Foth and Van Dyke and Associates, Inc. (1983). Green Lake Landfill Feasibility Report Additional Information.

Residuals Management Technology, Inc. (1985). Green Lake sanitary landfill south and east expansion no. 1, NR 180.13 feasibility study prepared for Green Lake Landfill Company, Inc.

Site 14

Warzyn Engineering, Inc. (1985). Feasibility for northern expansion area of Pheasant Run sanitary landfill, Waste Management of Wisconsin, Inc. Job C12812 and 10812.

Residuals Management Technology, Inc. (1978). In-field conditions and feasibility study for site expansion and partial abandonment of a landfill site owned by Keno Trucking, Inc.

Site 15

Robert E. Lee and Associates, Inc. (1981) Kewaunee County solid waste management system balefill and processing facility feasibility report. STS job 10877

Robert E. Lee and Associates, Inc. (1982) Report of "as-built" conditions. STS Job 10877.

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Residuals Management Technology, Inc (1981) Lemberger landfill site, horizontal expansion, feasibility report.

Residuals Management Technology, Inc. (1980) Revised in-field conditions analysis and addendum to the site operations plan for the Lemberger landfill in the W 1/2, Sec. 26, T20N, R22E, Town of Franklin, Manitowoc County, Wisconsin. STS Job 5858E.

Poth and Van Dyke and Associates, Inc. (1983) Ridgeview regional sanitary landfill horizontal expansion - plan of operation, Town of Franklin, Manitowoc County, Wisconsin. Volume I Design report/operations manual. Volume II Appendices. Prepared for Waste Management of Wisconsin, Inc.

Site 17

Poth and Van Dyke and Associates, Inc. (1981) Feasibility report for the proposed Marinette County sanitary landfill. STS Job 11330.

Poth and Van Dyke and Associates, Inc. (1981) Initial site report for the proposed Marinette County sanitary landfill. Giles Engineering Associates, Inc. job #810118.

Site 19

Warzyn Engineering, Inc. (1980) Documentation of partial site preparations Marquette County sanitary landfill. Job C7204B.

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Site 20

Wisconsin Electric Power Company, Inc. (1985) Ash disposal feasibility report, Caledonia site, Town of Caledonia, Racine County, Wisconsin.

Site 21

Warzyn Engineering, Inc. (1981) Bound reference file feasibility data

Warzyn Engineering, Inc. (1982) Western expansion feasibility study, Metro landfill development project, Franklin, Wisconsin. Job C11272

Hydrosearch, Inc (1986) Hydrogeologic characterization and ground water quality program, Metro landfill and development project, Franklin, Wisconsin, Phase II.

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Twin City Testing. Letter to Mr. Michael Marsden, Sept. 2, 1981. Subject: Field and laboratory tests, landfill expansion Outagamie County.

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Donohue and Associates, Inc. Letter to Mr. Peter Kmet, March 26, 1980. Subject: Outagamie County landfill site expansion (Job 40021.0)

Donohue and Associates, Inc. (1979). Site feasibility and design investigations, Outagamie County, Wisconsin, sanitary landfill expansion plan

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Robert E. Lee and Associates, Inc. (1981). Ozaukee County, initial site report, Anderson property.

Site 26

Robert E. Lee and Associates, Inc. (1982). Ozaukee County, initial site report, Didier property.

Site 27

Robert E. Lee and Associates, Inc. (1984). Ozaukee County, initial site report, WEPCO property.

Site 28

Mead and Hunt (1976). Hydrogeologic feasibility study.

Residuals Management Technology, Inc. (1981). Addendum to the feasibility study for Land Reclamation, Ltd.

Foth and Van Dyke and Associates, Inc. (1985). Initial site report (expansion).

Site 29

Warzyn Engineering, Inc. (1982). Geological and soils survey and groundwater monitoring program, Badger Army Ammunition Plant

Site 30

Nordin, S. and R. Pedersen (1985). Plan of operation, Shawano landfill, Phase 2, Shawano, Wisconsin.

Pedersen, R. W. (1984). Remedial action plan, Shawano landfill - Phase I, Shawano, Wisconsin.

Pedersen, R. W. (1984). Feasibility report, Shawano landfill, Phase 2 expansion (revised)

Pedersen, R. W. (1983). Feasibility report, Shawano landfill, Phase 2 expansion.

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Donohue and Associates, Inc. (1981). Initial site report for sanitary landfill, Bock/Grieg property, Town of Wilson, Sheboygan County, Wisconsin.

Donohue and Associates, Inc. (1982). Landfill feasibility investigation former Bock/Grieg site, Town of Wilson (revised 1984).

Site 32

Residuals Management Technology, Inc. (1982). Troy area landfill, NR 180.13 feasibility report for the Troy area landfill located in Sec. 31, T4N, R18E, Town of East Troy, Walworth County, Wisconsin.

Residuals Management Technology, Inc. (1986). Troy Area Landfill, Inc. plan of operation.

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Foth and Van Dyke and Associates, Inc. (1983). Plan of operation: Greidanus Enterprises, Inc. sanitary landfill horizontal expansion.

Foth and Van Dyke and Associates, Inc. (1983). Initial site report for the proposed northeast landfill expansion, Greidanus Enterprises, Inc., Walworth County, Wisconsin.

Residuals Management Technology, Inc. (1982). Feasibility report horizontal expansion to the existing Greidanus Enterprises, Inc. Landfill, Walworth County.

Warzyn Engineering, Inc. (1978). Additional feasibility information proposed Greidanus sanitary landfill expansion.

Warzyn Engineering, Inc. (1977). In-field conditions report and geologic study, Greidanus landfill site, Delavan, Wisconsin.

Site 34

Robert E. Lee and Associates, Inc. (1981). Washington County initial site report, Mertens property.

Site 35

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Warzyn Engineering, Inc. (1986). Environmental improvements northwest sand seam/northern triangle Omega Hills North landfill, Germantown, Wisconsin.

Warzyn Engineering, Inc. (1985). Northern area investigation, Omega Hills North Landfill.

Warzyn Engineering, Inc. (1985). Conceptual plan modification proposal, Omega Hills South Landfill, Waste Management of Wisconsin, Inc., Village of Menominee Falls, Wisconsin.

Site 36

Robert E. Lee and Associates, Inc. (1981). Washington County initial site report, Schowalter property.

Site 37

Warzyn Engineering, Inc. (1983). Brookfield sanitary landfill interim groundwater investigation.

Emcon Associates (1976). Geotechnical investigation, Brookfield sanitary landfill, Waukesha County, Wisconsin.

Site 38

Donohue and Associates, Inc. (1984). Landfill feasibility report, Kempf property - Town of Little Wolf, Waupaca County, Wisconsin.

Site 39

Donohue and Associates, Inc. (1982). Initial site report Waupaca County property - Town of Royalton, Waupaca County, Wisconsin.

Site 40

Donohue and Associates, Inc. (1985). Landfill feasibility report Bartlett property - Town of Oshkosh, Winnebago County, Wisconsin. 3 Volumes.

Donohue and Associates, Inc. (1985). Bartlett property - Town of Oshkosh, Winnebago County, Wisconsin (initial site report).

Site 41

Soil Testing Services of Wisconsin, Inc. Data from Jobs 7801A (1977) through 7801K (1982).

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR BROWN COUNTY - BROWN SITE

+ IDENTITY	+ County	+ Litho- strat.	+ Mat. Site (code) No.	+ Lat.	+ Long.	+ Elev. no. (ft)	+ Surf. Elev. (ft)	+ Sample Top (ft)	+ Sample Bottom (ft)	+ CONDUCTIVITY Lab K Meth (c/s)	+ HYDRAULIC Lab K Meth (c/s)	+ Grain Size Percentages Matrix 1 (2.0 to 0.0625 mm) Matrix 2 (0.0625 to 0.0075 mm) Matrix 3 (0.0075 to 0.0025 mm)	+ Engineering Properties Unified Soil Class. P200 (pcf)	+ Built Dev Percent Unit Wt. SPT Moist. Liquid Plastic. UC	+ (NO cont. (t) limit index (tst) +	
BN 1980 KEE1	3	1	443048	875045	B1	791.4	5.0	6.5							35	2.5
BN 1980 KEE1	3	1	443048	875045	B1	791.4	10.0	11.0							400	4.5
BN 1980 KEE1	3	1	443048	875045	B1	791.4	15.0	15.5								4.5
BN 1980 KEE1	3	1	443048	875045	B1	791.4	20.0	21.5							63	1.0
BN 1980 KEE1	3	1	443048	875045	B1	791.4	25.0	26.5							30	2.0
BN 1980 KEE1	3	1	443048	875045	B1	791.4	30.0	31.5							18	1.0
BN 1980 UN	4	1	443048	875045	B1	791.4	35.0	36.5							75	
BN 1980 KEE1	3	1	443048	875045	B1	791.4	40.0	40.5							400	
BN 1980 KEE1	3	1	443048	875045	B1	791.4	45.0	45.5							35	3.0
BN 1980 KEE1	3	1	443048	875045	B2	798.3	10.0	10.5							600	4.5
BN 1980 KEE1	3	1	443048	875045	B2	798.3	15.0	15.5							200	4.5
BN 1980 KEE1	3	1	443048	875045	B2	798.3	20.0	21.5							35	1.5
BN 1980 KEE1	3	1	443048	875045	B2	798.3	25.0	26.5							25	1.0
BN 1980 KEE1	3	1	443048	875045	B2	798.3	30.0	31.5							30	1.5
BN 1980 KEE1	3	1	443048	875045	B2	798.3	35.0	36.5							25	1.4
BN 1980 UN	4	1	443048	875045	B2	798.3	40.0	40.5							200	
BN 1980 KEE1	3	1	443034	875028	B3	794.4	5.0	6.5							22	3.5
BN 1980 UN	3	1	443034	875028	B3	794.4	10.0	12.0								4.5
BN 1980 UN	3	1	443034	875028	B3	794.4	15.0	15.5								
BN 1980 UN	3	1	443034	875028	B3	794.4	20.0	21.5								
BN 1980 UN	3	1	443034	875028	B3	794.4	25.0	25.5								
BN 1980 UN	3	1	443034	875028	B3	794.4	30.0	35.5								
BN 1980 UN	3	1	443034	875028	B3	794.4	35.0	35.5								
BN 1980 UN	3	1	443022	875045	B4	788.8	5.0	6.5								
BN 1980 KEE1	3	1	443022	875045	B4	788.8	10.0	11.5								4.0
BN 1980 UN	3	1	443022	875045	B4	788.8	15.0	16.5								3.5
BN 1980 UN	3	1	443022	875045	B4	788.8	20.0	21.5								3.0
BN 1980 UN	3	1	443022	875045	B4	788.8	25.0	25.5								
BN 1980 UN	3	1	443022	875045	B4	788.8	30.0	30.5								
BN 1980 UN	3	1	443022	875045	B4	788.8	35.0	35.5								
BN 1980 KEE1	3	1	443022	875015	B5	800.9	2.0	4.0								
BN 1980 KEE1	3	1	443022	875015	B5	800.9	4.0	6.0								
BN 1980 KEE1	3	1	443022	875015	B5	800.9	6.0	8.0								
BN 1980 KEE1	3	1	443022	875015	B5	800.9	8.0	8.5								
BN 1980 KEE1	3	1	443022	875015	B5	800.9	10.0	11.5								
BN 1980 KEE1	3	1	443022	875015	B5	800.9	15.0	16.5								
BN 1980 KEE1	3	1	443022	875015	B5	800.9	20.0	21.5								
BN 1980 KEE1	3	1	443022	875015	B5	800.9	25.0	27.0								
BN 1980 UN	3	1	443022	875015	B5	800.9	30.0	32.0								
BN 1980 UN	3	1	443022	875015	B5	800.9	35.0	37.0								
BN 1982 KEE1	3	1	443047	875042	B1A	792.3	0.5	5.0								
BN 1982 KEE1	3	1	443047	875042	B1A	792.3	5.0	7.0								
BN 1982 KEE1	3	1	443047	875042	B1A	792.3	10.0	12.0								



[illegible]

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR BROWN COUNTY - BAYTON SITE

+ IDENTITY	+ Country	+ Litho- unit	+ Mat. Site (code)	+ No.	+ Lat.	+ Long.	+ Brng. no.	+ Surt. Elev. (ft)	+ Sample (ft)	+ Top (ft)	+ Bottom (ft)	+ Hydraulic + Conductivity (cm/s)	+ Lab K code	+ Meth (cm/s)	+ Fld K code	+ Matrix I sand (2.0 to 0.0625 to 0.002mm)	+ Matrix II silt (0.0625 to 0.002mm)	+ Matrix III clay (<0.002mm)	+ Unified Soil Class.	+ P200 pcf	+ Bulk Percent Unit Wt.	+ Dry SPT Moist. (lb)	+ Liquid Plastic. Index (%)	+ Plastic. Index (%)
BN 1982 KES1	3				443045	875035	B6	793.0	0.5	5.0														
BN 1982 KES1	3				443045	875035	B6	793.0	5.0	6.0														
BN 1982 KES1	3				443045	875035	B6	793.0	10.0	11.5														
BN 1982 UN	3				443045	875035	B6	793.0	15.0	16.0														
BN 1982 UN	3				443045	875035	B6	793.0	20.0	21.0														
BN 1982 UN	3				443045	875035	B6	793.0	25.0	26.0														
BN 1982 UN	3				443045	875035	B6	793.0	30.0	30.5														
BN 1982 UN	3				443045	875035	B6	793.0	35.0	36.0														
BN 1982 UN	3				443045	875035	B6	793.0	40.0	40.5														
BN 1982 KES1	3				443039	875035	B7	790.0	1.0	5.0														
BN 1982 KES1	3				443039	875035	B7	790.0	5.0	4.5														
BN 1982 KES1	3				443039	875035	B7	790.0	10.0	11.5														
BN 1982 KES1	3				443039	875035	B7	790.0	15.0	16.0														
BN 1982 UN	3				443039	875035	B7	790.0	20.0	21.5														
BN 1982 UN	3				443039	875035	B7	790.0	25.0	25.5														
BN 1982 UN	3				443039	875035	B7	790.0	30.0	31.5														
BN 1982 UN	3				443039	875035	B7	790.0	35.0	35.5														
BN 1982 UN	3				443039	875035	B7	790.0	40.0	40.5														
BN 1982 KES1	3				443030	875035	B8	794.8	1.0	5.0														
BN 1982 KES1	3				443030	875035	B8	794.8	5.0	6.5														
BN 1982 KES1	3				443030	875035	B8	794.8	10.0	11.5														
BN 1982 KES1	3				443030	875035	B8	794.8	15.0	15.5														
BN 1982 KES1	3				443030	875035	B8	794.8	20.0	21.5														
BN 1982 KES1	3				443030	875035	B8	794.8	25.0	26.5														
BN 1982 UN	3				443030	875035	B8	794.8	30.0	31.5														
BN 1982 UN	3				443030	875035	B8	794.8	35.0	36.5														
BN 1982 UN	3				443030	875035	B8	794.8	40.0	41.5														
BN 1982 KES1	3				443025	875035	B9	786.5	5.0	7.0														
BN 1982 KES1	3				443025	875035	B9	786.5	10.0	12.0														
BN 1982 KES1	3				443025	875035	B9	786.5	15.0	17.0														
BN 1982 KES1	3				443025	875035	B9	786.5	20.0	22.0														
BN 1982 UN	513				443025	875035	B9	786.5	25.0	26.0														
BN 1982 UN	5				443025	875035	B9	786.5	30.0	31.5														
BN 1982 UN	3				443025	875035	B9	786.5	35.0	35.5														
BN 1982 KES1	3				443099	875099	B10	788.5	1.0	5.5														
BN 1982 UN	99				443099	875099	B10	788.5	5.5	7.5														
BN 1982 UN	3				443099	875099	B10	788.5	10.0	11.5														
BN 1982 UN	3				443099	875099	B10	788.5	15.0	16.5														
BN 1982 UN	3				443099	875099	B10	788.5	20.0	20.7														
BN 1982 UN	3				443099	875099	B10	788.5	25.0	26.0														
BN 1982 UN	3				443099	875099	B10	788.5	30.0	30.6														
BN 1982 KES1	35				443047	875028	B11	788.5	5.5	20.3														
BN 1982 KES1	3				443047	875028	B11A	788.5	1.0	5.0														
BN 1982 KES1	3				443047	875028	B11A	788.5	5.0	5.5														
BN 1982 KES1	3				443047	875028	B11A	788.5	10.0	11.5														

4.01E-06

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Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR BROWN COUNTY - BAYTON SITE

+ IDENTITY + + + County + (code) Year (code) (code) No.	Litho- strat. unit	Bat. Site	Lat.	Long.	Bndg. no.	Surf. Elev. top (ft)	Sample depth bottom (ft)	+ CONDUCTIVITY + Lab K + (cm/s)	+ HYDRAULIC + Meth + (cm/s) code	+ + + Fid K Meth + (cm/s) code	+ GRAIN SIZE PERCENTAGES + Matrix I + sand + (2.0 to 0.075mm) + 0.0075mm	+ ENGINEERING PROPERTIES + Matrix I + clay + (0.002mm) + 0.0075mm	+ Unified + Soil + Percent Unit Wt. + P200 (pcf)	Dry + Bulk + Moist. + Liquid Plasticity, NC + (MI) cont. (I) Limit + index (IPI) +
BN 1982 KES1	3	1	413047	875028	B11A	798.5	15.0	17.0						
BN 1982 UN	3	1	413047	875028	B11A	798.5	19.5	21.5						21.0
BN 1982 UN	3	1	413047	875028	B11A	798.5	25.0	26.2						31
BN 1982 UN	3	1	413047	875028	B11A	798.5	30.0	31.0						
BN 1982 UN	3	1	413047	875028	B11A	798.5	35.0	35.2						
BN 1982 UN	3	1	413047	875028	B11A	798.5	34.7	39.7	5.12E-06	8				
BN 1982 KES1	3	1	413041	875028	B12	794.0	1.0	5.0						
BN 1982 KES1	3	1	413041	875028	B12	794.0	5.0	6.5						
BN 1982 KES1	3	1	413041	875028	B12	794.0	10.0	11.5						
BN 1982 KES1	3	1	413041	875028	B12	794.0	15.0	17.0						
BN 1982 UN	3	1	413041	875028	B12	794.0	20.0	21.5	1.50E-05	23	56	44		26.0
BN 1982 UN	3	1	413041	875028	B12	794.0	25.0	26.5						
BN 1982 UN	3	1	413041	875028	B12	794.0	30.0	31.5						
BN 1982 UN	3	1	413036	875028	B13	792.0	1.0	5.0						
BN 1982 KES1	3	1	413036	875028	B13	792.0	5.0	7.0						
BN 1982 KES1	3	1	413036	875028	B13	792.0	10.0	12.0						
BN 1982 KES1	3	1	413036	875028	B13	792.0	15.0	17.0						
BN 1982 UN	3	1	413036	875028	B13	792.0	20.0	22.0						
BN 1982 UN	3	1	413036	875028	B13	792.0	25.0	26.5						
BN 1982 UN	3	1	413036	875028	B13	792.0	30.0	31.0						
BN 1982 UN	3	1	413031	875028	B14	794.0	1.0	2.5						
BN 1982 KES1	3	1	413031	875028	B14	794.0	5.0	6.5						
BN 1982 KES1	3	1	413031	875028	B14	794.0	10.0	11.5						
BN 1982 UN	3	1	413031	875028	B14	794.0	15.0	16.0						
BN 1982 UN	3	1	413031	875028	B14	794.0	20.0	21.0						
BN 1982 UN	3	1	413031	875028	B14	794.0	25.0	26.0						
BN 1982 UN	3	1	413031	875028	B14	794.0	30.0	30.6						
BN 1982 UN	99	1	413026	875028	B15	792.0	1.2	5.0						
BN 1982 KES1	3	1	413026	875028	B15	792.0	5.0	7.0						
BN 1982 KES1	3	1	413026	875028	B15	792.0	10.0	11.5						
BN 1982 UN	3	1	413026	875028	B15	792.0	15.0	16.0						
BN 1982 UN	3	1	413026	875028	B15	792.0	20.0	21.5						
BN 1982 UN	3	1	413026	875028	B15	792.0	25.0	26.0						
BN 1982 UN	3	1	413026	875028	B15	792.0	30.0	30.2						
BN 1982 UN	3	1	413021	875028	B16A	792.8	1.0	5.0						
BN 1982 KES1	3	1	413021	875028	B16A	792.8	5.0	7.0						
BN 1982 KES1	3	1	413021	875028	B16A	792.8	10.0	12.0						
BN 1982 KES1	3	1	413021	875028	B16A	792.8	15.0	17.0						
BN 1982 KES1	3	1	413021	875028	B16A	792.8	20.0	22.0						
BN 1982 KES1	3	1	413021	875028	B16A	792.8	25.0	27.0						
BN 1982 KES1	3	1	413021	875028	B16A	792.8	30.0	32.0						
BN 1982 UN	3	1	413021	875028	B16A	792.8	35.0	36.0						

[illegible]

+ IDENTITY	+ County	+ Litho-unit	+ Mat. Site	+ (code) Year	+ (code) No.	+ Lat.	+ Long.	+ Brno. no.	+ Elev. (ft)	+ Sample top	+ (ft)	+ HYDRAULIC		+ BRAINISIE PERCENTAGES		+ ENGINEERING PROPERTIES		+ SPT	+ Moist.	+ Liquid Plastic. (sf)	+ Index (sf)				
												+ Lab K	+ Meth	+ Fld K	+ Meth	+ Bulk	+ Unit								
												+ (cm/s)	+ code	+ (cm/s)	+ code	+ (cm/s)	+ code								
												+ (ft)	+ (ft)	+ (ft)	+ (ft)	+ (ft)	+ (ft)								
												+ Matrix I		+ Matrix II		+ Matrix III									
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Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR BROWN COUNTY - BAYTON SITE

+ IDENTITY		+ HYDRAULIC			+ GRAIN SIZE PERCENTAGES			+ ENGINEERING PROPERTIES										
+ County	+ (code)	Year	Litho- strat.	Nat. Site (code)/(code) No.	Lat.	Long. no.	Elev. top (ft)	Sample depth bottom (ft)	Lab K (cm/s)	Meth code	Fid K Meth (cm/s)	Bolt I (2.0 to 0.0025 to 0.0025)	Sand (0.0025 to 0.0025)	Matrix I clay	Matrix I clay	Unified Soil Class.	Bulk Percent Unit Wt. P200 (pcf)	Drv SPF Moist. Liquid Plastic. UC (in cont. (2) limit index (tsf) +
BN 1982	KE61	3		443029	875010	831	795.0	5.0	6.5							CL	23	3.5
BN 1982	KE61	3		443029	875010	831	795.0	10.0	11.5							CL	11.0	3.5
BN 1982	KE61	3		443029	875010	831	795.0	15.0	17.0							CL	18.0	3.0
BN 1982	KE61	3		443029	875010	831	795.0	20.0	22.0							CL	22.0	3.0
BN 1982	KE61	3		443029	875010	831	795.0	25.0	27.0							CL	27.0	1.8
BN 1982	KE61	3		443029	875010	831	795.0	30.0	32.0							CL	26.0	1.5
BN 1982	UN	3		443029	875010	831	795.0	35.0	36.0							ML	14.0	4.5
BN 1982	UN	3		443029	875010	831	795.0	40.0	42.0							ML	20.0	3.8

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR BROWN COUNTY, DECATUR (BROWN COUNTY WEST) SITE

+ IDENTITY + County + (code) Year (code) No.	+ Libro- unit Mat. Site	+ Lat.	+ Long. No. (ft)	+ Brng. Elev. top (ft)	+ HYDRAULIC + CONDUCTIVITY		+ GRAINSIZE PERCENTAGES		+ ENGINEERING PROPERTIES		+ SPT Moist. Liquid Plastic. UC (IN) cont. (U) limit index (tsf) +
					Surf. Sample	Bottom	Matrix %	Matrix %	Unified Soil	Bulk Dry	
					(ft)	(ft)	Matrix %	Matrix %	Class. P200	Percent Unit Wt.	
					(ft)	(ft)	(0.0025mm)	(0.0025mm)	Class. P200	Percent Unit Wt.	
BN 1973	UN	8	2	443046	880921	DE1	680.5	0.0	0.5	3	3
BN 1973	UN	99	2	443046	880921	DE1	680.5	0.5	1.5	5	5
BN 1973	KE	5	2	443046	880921	DE1	680.5	2.0	4.0		
BN 1973	KE	5	2	443046	880921	DE1	680.5	4.0	5.5		20.0
BN 1973	KE	5	2	443046	880921	DE1	680.5	6.0	7.5		3.5
BN 1973	KE	5	2	443046	880921	DE1	680.5	10.0	12.0		
BN 1973	KE	5	2	443046	880921	DE1	680.5	15.0	17.0		22.0
BN 1973	KE	5	2	443046	880921	DE1	680.5	20.0	22.0		3.5
BN 1973	KE	5	2	443046	880921	DE1	680.5	25.0	27.0		27.0
BN 1973	KE	5	2	443046	880921	DE1	680.5	30.0	32.0		36.0
BN 1973	KE	5	2	443046	880921	DE1	680.5	35.0	36.5		34.0
BN 1973	KE	5	2	443046	880921	DE1	680.5	40.0	41.5		23.0
BN 1973	KE	5	2	443046	880921	DE1	680.5	45.0	46.5		44
BN 1973	KE	5	2	443046	880921	DE1	680.5	50.0	51.5		103
BN 1973	KE	5	2	443046	880921	DE1	680.5	55.0	56.5		200
BN 1973	UN	99	2	443046	880921	DE1	680.5	60.0	61.5		57
BN 1973	UN	99	2	443046	880921	DE1	680.5	65.0	66.5		12
BN 1973	UN	99	2	443046	880921	DE1	680.5	70.0	71.5		12
BN 1973	KE	5	2	443046	880921	DE2	670.6	2.0	3.5		
BN 1973	KE	5	2	443046	880921	DE2	670.6	4.0	6.0		
BN 1973	KE	5	2	443046	880921	DE2	670.6	6.0	8.0		
BN 1973	KE	5	2	443046	880921	DE2	670.6	10.0	12.0		25.0
BN 1973	KE	5	2	443046	880921	DE2	670.6	15.0	17.0		28.0
BN 1973	KE	5	2	443046	880921	DE2	670.6	20.0	22.0		15.0
BN 1973	KE	5	2	443046	880921	DE2	670.6	25.0	26.5		
BN 1973	KE	5	2	443046	880921	DE2	670.6	30.0	31.5		
BN 1973	KE	5	2	443046	880921	DE2	670.6	35.0	36.5		
BN 1973	KE	5	2	443046	880921	DE2	670.6	40.0	42.0		
BN 1973	KE	5	2	443046	880921	DE2	670.6	45.0	47.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	50.0	51.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	55.0	56.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	60.0	61.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	65.0	66.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	70.0	71.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	75.0	76.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	80.0	81.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	85.0	86.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	90.0	91.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	95.0	96.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	100.0	101.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	105.0	106.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	110.0	111.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	115.0	116.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	120.0	121.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	125.0	126.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	130.0	131.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	135.0	136.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	140.0	141.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	145.0	146.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	150.0	151.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	155.0	156.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	160.0	161.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	165.0	166.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	170.0	171.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	175.0	176.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	180.0	181.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	185.0	186.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	190.0	191.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	195.0	196.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	200.0	201.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	205.0	206.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	210.0	211.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	215.0	216.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	220.0	221.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	225.0	226.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	230.0	231.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	235.0	236.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	240.0	241.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	245.0	246.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	250.0	251.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	255.0	256.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	260.0	261.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	265.0	266.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	270.0	271.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	275.0	276.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	280.0	281.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	285.0	286.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	290.0	291.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	295.0	296.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	300.0	301.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	305.0	306.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	310.0	311.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	315.0	316.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	320.0	321.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	325.0	326.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	330.0	331.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	335.0	336.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	340.0	341.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	345.0	346.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	350.0	351.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	355.0	356.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	360.0	361.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	365.0	366.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	370.0	371.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	375.0	376.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	380.0	381.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	385.0	386.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	390.0	391.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	395.0	396.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	400.0	401.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	405.0	406.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	410.0	411.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	415.0	416.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	420.0	421.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	425.0	426.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	430.0	431.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	435.0	436.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	440.0	441.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	445.0	446.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	450.0	451.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	455.0	456.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	460.0	461.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	465.0	466.5		
BN 1973	UN	12	2	443051	880922	DE2	670.6	470.0	471.5		
BN 1973	UN	12	2								





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+ IDENTITY	+ Litho- strat.	+ County unit	+ Mat. Site (code)	+ Year (code)	+ Lat.	+ Long. no.	+ Surf. Elev. (ft)	+ Saste top (ft)	+ Bottom (ft)	+ HYDRAULIC + CONDUCTIVITY (cfs)	+ Matrix I (0.0025 to 0.0025)	+ Matrix II (0.0025 to 0.0025)	+ ENGINEERING PROPERTIES					+ SPT Moist. Liquid index (tsf)	
BN 1979	KE	5	2	443044	880929	B7	665.9	12.0	13.0	3.30E-08	5	5		CL	69	30	23	9	
BN 1979	KE	99	2	443044	880929	B7	665.9	2.0	3.0	2.60E-08	5	2		CL	62	53	24	12	
BN 1979	KE	5	2	443044	880928	B8	665.4	12.0	13.0		0	0		CL	99	32	35	15	
BN 1979	KE	5	2	443044	880928	B8	665.4	2.0	3.0		3	3		CL	81	54	35	20	
BN 1979	KE	5	2	443044	880927	B9	663.1	12.0	13.0		0	0		CL-HL	99	27	28	7	
BN 1979	KE	5	2	443044	880927	B9	663.1	2.0	3.0		0	0		CL-HL	67	47	24	5	
BN 1979	KE	99	2	443099	880999	B37	669.0		2.5								35	19	
BN 1979	KE	99	2	443099	880999	B39	670.0		6.0								28	15	
BN 1979	KE	99	2	443099	880999	B47	691.0		9.0								28	16	
BN 1979	KE	99	2	443099	880999	B40	669.0	2.0	3.0	1.01E-05	5	5				10			
BN 1979	KE	99	2	443099	880999	B40	669.0	4.0	5.0	5.00E-08	5	5				14			

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR BROWN COUNTY - WELLSITE SITE

+ IDENTITY	+ County	+ (code)	+ Year	+ Litho-strat. unit	+ Nat. Site (code)	+ No.	+ Lat.	+ Long.	+ Eng. no.	+ Surf. Elev. (ft)	+ Sample top (ft)	+ Sample bottom (ft)	+ Lab K Meth (cm/s)	+ Lab K code	+ Hyd K Meth (cm/s)	+ Hyd K code	+ Matrix I sand (0.0625 to 0.002mm)	+ Matrix I silt (0.002mm to 0.00075mm)	+ Matrix I clay (<0.00075mm)	+ Unified Soil Class.	+ Bulk P200 (pcf)	+ SPI Moist. Index (tcf)	+ Liquid Plastic. Index (tcf)	+ (M) cont. (t) limit
BN 1974	KE	4	3	412432	880028	DIA	811.5	18.5	20.0	6.80E-04														
BN 1974	KE	4	3	412432	880028	DIA	811.5	0.0	1.5															
BN 1974	KE	4	3	412432	880028	DIA	811.5	2.0	3.5															
BN 1974	KE	4	3	412432	880028	DIA	811.5	4.0	55.0															
BN 1974	KE	4	3	412432	880028	DIA	811.5	6.0	7.5															
BN 1974	KE	4	3	412432	880028	DIA	811.5	10.0	11.5															
BN 1974	KE	4	3	412432	880028	DIA	811.5	15.0	16.5															
BN 1974	KE	4	3	412432	880028	DIA	811.5	20.0	21.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	25.0	26.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	30.0	31.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	35.0	36.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	40.0	41.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	45.0	46.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	50.0	52.0															
BN 1974	KE	5	3	412432	880028	DIA	811.5	55.0	56.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	60.0	61.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	65.0	66.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	70.0	71.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	75.0	76.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	80.0	81.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	85.0	86.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	90.0	91.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	95.0	96.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	100.0	101.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	105.0	106.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	110.0	111.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	115.0	116.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	120.0	121.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	125.0	126.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	130.0	131.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	135.0	136.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	140.0	141.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	145.0	146.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	150.0	151.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	155.0	156.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	160.0	161.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	165.0	166.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	170.0	171.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	175.0	176.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	180.0	181.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	185.0	186.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	190.0	191.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	195.0	196.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	200.0	201.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	205.0	206.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	210.0	211.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	215.0	216.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	220.0	221.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	225.0	226.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	230.0	231.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	235.0	236.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	240.0	241.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	245.0	246.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	250.0	251.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	255.0	256.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	260.0	261.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	265.0	266.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	270.0	271.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	275.0	276.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	280.0	281.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	285.0	286.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	290.0	291.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	295.0	296.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	300.0	301.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	305.0	306.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	310.0	311.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	315.0	316.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	320.0	321.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	325.0	326.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	330.0	331.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	335.0	336.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	340.0	341.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	345.0	346.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	350.0	351.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	355.0	356.5															
BN 1974	KE	5	3	412432	880028	DIA	811.5	360.0																

## Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR BROWN COUNTY - DECLEENE SITE

+ IDENTITY		+ HYDRAULIC				+ GEOSYNTHETIC PERCENTAGES			+ ENGINEERING PROPERTIES			
:	Litho- strat.	Surf. Elev.	Seapie Strat.	CONDUCTIVITY	Matrix %	Matrix %	Matrix %	Unified	Bulk	Dry		
+ Count	unit	no.	top	bottom	sand	silt	clay	Soil	Percent	Unit Wt.	SP	Moist. Liquid Plastic UC
+ (code)	Year (code)(code)	Lat.	Long.	(ft)	(ft)	(ft)	(ft)	(ft)	Class.	P200 (pcf)	(Wt cont.%)	Shrink index (tsf)
BN 1983	KEFI	3	3	442199	880099	M27a	842.1	0.0	1.5		CL	20
BN 1983	KEFI	3	3	442199	880099	M27a	842.1	5.0	6.5		CL	16
BN 1983	KE	4	3	442199	880099	M27a	842.1	10.0	11.5		SP	8
BN 1983	KE	4	3	442199	880099	M27a	842.1	15.0	16.5		SP	46

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Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR CALUMET COUNTY

+ IDENTITY		+ Litho- strat.		+ County unit		+ Mat. Site (code)		+ Year (code)		+ Lat.		+ Long.		+ Elevation no. (ft)		+ Sample top (ft)		+ Sample bottom (ft)		+ HYDRAULIC + CONDUCTIVITY		+ Matrix Z Matrix X + sand silt clay		+ Matrix X Matrix Z + silt clay		+ ENGINEERING PROPERTIES		+ Bulk Unit Wt. P200 (pcf)		+ Soil Percent Class.		+ Moist. Limit (%)		+ Plasticity Index (%)			
CA	1981	KEDh	3	5	440609	881136	RM2	916.6	10.0	12.0	8.30E-08	1	14	22	78	CL	71	38	20																		
CA	1981	KEDh	3	5	440616	881128	RM5	918.0	10.0	12.0	1.90E-08	1	0	24	76	CL	90	49	30																		
CA	1982	KEDh	3	5	440616	881128	RM5A	907.5	33.3	40.3	4.70E-07	7	6	23	71	CL	77	23.0	4.3																		
CA	1982	KEDh	3	5	440609	881128	RM5B	922.4	8.0	10.0	2.60E-06	7	6	23	71	CL	77	34	18																		
CA	1982	KEDh	3	5	440616	881137	RM7B	922.4	34.5	39.5	7.50E-07	7	1	13	47	CL	92	46	24																		
CA	1982	KEDh	3	5	440619	881133	RM10	925.4	15.0	17.0	3.40E-08	1	1	18	51	CL	86	39	22																		
CA	1982	KEDh	3	5	440619	881133	RM10	925.4	4.4	14.4	2.00E-09	1	0	12	40	CL	94	42	23																		
CA	1982	KEDh	3	5	440616	881133	RM11	923.0	28.5	30.5	3.20E-08	1	4	15	51	CL	84	31	14																		
CA	1982	KEDh	3	5	440613	881133	RM12	921.7	10.0	12.0	3.50E-08	1	4	31	43	CL	73	54	27																		
CA	1982	KEDh	3	5	440613	881133	RM12	921.7	53.5	55.5	4.50E-09	1	4	31	43	CL	73	54	27																		
CA	1982	KEDh	3	5	440613	881133	RM12	921.7	5.7	15.7	9.40E-07	7	4	31	43	CL	73	54	27																		

+ IDENTITY			+ LITHO- strat.			+ SURT.			+ HYDRAULIC + CONDUCTIVITY			+ SOILSIZE PERCENTAGES			+ ENGINEERING PROPERTIES		
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
Year	Code	Unit	Mat.	Site	No.	Lat.	Long.	no.	ft.	ft.	ft.	ft.	ft.	ft.	ft.	ft.	ft.
DN 1964	H0	99	6	430438	891154	M3	15.4	23.0	1.07E-02	9							
DN 1984	H0	99	6	430438	891154	M3	15.4	23.0	2.80E-03	9							
DN 1984	H0	4	6	430438	891154	P6	38.0	48.0	3.47E-03	9							
DN 1984	H0	4	6	430438	891154	P6	38.0	48.0	9.84E-04	9							
DN 1984	H0	4	6	430438	891154	P6	38.0	48.0	1.74E-03	9							
DN 1984	H0	99	6	430438	891154	P22	48.0	65.0	5.88E-03	9							
DN 1984	H0	99	6	430438	891154	P22	48.0	65.0	1.50E-03	9							
DN 1984	H0	99	6	430438	891154	P22	48.0	65.0	1.32E-03	9							
DN 1980	UN	99	6	430440	891152	B2	1.0	2.5									
DN 1982	UN	99	6	430438	891156	B1	1.0	2.5									
DN 1982	UN	99	6	430438	891154	B3	1.0	2.5									
DN 1982	UN	99	6	430438	891154	B3	3.5	5.0									
DN 1982	UN	99	6	430440	891150	B4	1.0	2.5									
DN 1982	UN	99	6	430440	891150	B4	3.5	5.0									
DN 1982	UN	99	6	430438	891150	P6	33.5	35.0									
DN 1983	H0	4	6	430438	891154	P6	38.0	48.0									
DN 1983	H0	3	6	430437	891155	M7	9.0	15.0	7.01E-04	7							
DN 1983	UN	7	6	430440	891142	M8	9.2	14.5	2.20E-04	7							
DN 1983	H0	3	6	430438	891150	M9	14.7	21.0	6.90E-04	7							
DN 1983	H0	3	6	430438	891150	P10	35.0	45.0	9.08E-04	7							
DN 1983	H0	99	6	430438	891150	P10	13.5	15.0									
DN 1983	H0	4	6	430438	891154	M11	7.6	12.5	1.40E-04	7							
DN 1983	H0	3	6	430434	891154	M12	53.0										
DN 1983	H0	3	6	430437	891142	M12	53.0										
DN 1983	UN	7	6	430442	891156	M13	3.3	6.0	3.65E-04	7							
DN 1983	UN	7	6	430442	891156	M13	5.0										
DN 1983	H0	3	6	430445	891147	M14	13.1	29.0	3.38E-06	7							

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR DANE COUNTY LIBBY ROAD SITE

+ IDENTITY			+ LITHO-STRAT.			+ GEOLOGY			+ HYDRAULIC + CONDUCTIVITY			+ BRAINSLIE PERCENTAGES			+ ENGINEERING PROPERTIES			+ OTHER				
Country	Year	Unit	Lat.	Long.	Brng. Elev.	Surf. Elev.	Sample Top	Sample Bottom	Lab K	Math	Fld K	Meth	Matrix X	Matrix Y	Matrix Z	Unified Soil	Bulk Percent	Dr. Wt.	SPT	Moist.	Liquid Plastic	UC
(code)	(code)	(code)	(code)	(code)	(code)	(code)	(code)	(code)	(code)	(code)	(code)	(code)	(code)	(code)	(code)	(code)	(code)	(code)	(code)	(code)	(code)	(code)
DN 1981	HO	6	7 430125	892041	L1A	1.5	2.5															
DN 1981	HO	3	7 430125	892043	L1A	7.0	7.5															
DN 1981	HO	3	7 430125	892041	L1A	13.5	15.0															
DN 1981	HO	99	7 430115	892035	L1B	3.5	5.0															
DN 1982	HO	99	7 430115	892022	L3A	29.5	38.0															
DN 1982	HO	3	7 430131	892049	L4A	28.5	30.0															
DN 1982	HO	99	7 430131	892028	L5A	13.5	15.0															
DN 1982	HO	4	7 430124	892028	L8A	43.5	45.0															
DN 1982	HO	3	7 430124	892028	L8B	58.5	60.0															
DN 1982	HO	3	7 430125	892019	L9B	8.5	10.0															
DN 1982	HO	4	7 430125	892019	L9B	43.5	45.0															
DN 1982	HO	3	7 430120	892028	L11A	15.0	29.0															
DN 1982	HO	3	7 430120	892028	L11B	13.5	15.0															
DN 1982	HO	3	7 430115	892043	L12C	12.1	24.0															
DN 1982	HO	3	7 430117	892026	L13	33.5	35.0															
DN 1982	HO	3	7 430116	892007	L14C	13.5	15.0															
DN 1982	HO	4	7 430116	892007	L14C	28.5	30.0															
DN 1982	HO	4	7 430116	892007	L14C	58.5	60.0															
DN 1982	HO	5	7 430108	892043	L15A	8.5	10.0															
DN 1982	HO	4	7 430108	892043	L15A	28.5	30.0															
DN 1982	HO	4	7 430108	892028	L16B	18.5	20.0															
DN 1982	HO	5	7 430105	892028	L16B	33.5	35.0															
DN 1982	HO	4	7 430107	89																		

[illegible]

[illegible]

[illegible]

[illegible]

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR DOOR COUNTY BALEFILL

+ IDENTITY		+ HYDRAULIC				+ GRAINSIZE PERCENTAGES				+ ENGINEERING PROPERTIES					
+ Litho-	+ Strat.	+ CONDUCTIVITY		+ Sample		+ Matrix %		+ Matrix %		+ Unified		+ Soil		+ Moist. Liquid Plastic. UC	
+ County	+ Unit	+ Lab X		+ bottom		+ Bulk %		+ Bulk %		+ Percent		+ P200		+ (N) cont. (N) limit	
+ (code)	+ Year (code)	+ (code)	+ No.	+ (ft)	+ (ft)	+ (cm/s)	+ code	+ (cm/s)	+ code	+ (0.0025 to 0.0075mm)	+ (0.0025mm)	+ (0.0025mm)	+ (0.0025mm)	+ (N) cont. (N) limit	+ index (Isf)
DR 1973	KE61	3	10	445139	872653	M7	656.8	8.0	10.0			CL		18.0	4.3
DR 1973	KE61	3	10	445139	872655	M7	656.8	10.0	12.0			CL		15.0	4.2
DR 1973	KE61	3	10	445140	872644	M9	670.8	0.0	2.0					19.0	2.9
DR 1973	KE61	3	10	445140	872644	M9	670.8	2.0	3.0					22.0	
DR 1973	KE61	3	10	445140	872644	M9	670.8	3.0	4.0			ML		13.0	
DR 1973	KE61	3	10	445140	872644	M9	670.8	4.0	6.0			CL		20.0	4.5



[illegible]

[illegible]

County (code)	Year	Mat. Site (code)	Litho- strat.	Lat.	Long.	Brng. No.	Surf. Elev. (ft)	Sample top (ft)	Sample bottom (ft)	+ HYDRAULIC + CONDUCTIVITY		+ GRAIN SIZE PERCENTAGES				+ ENGINEERING PROPERTIES				SPT Moist. Unit Wt. (lb)	Liquid Plastic. Index (%)	Unit Wt. (pcf)
										Lab K (cm/s)	Field K (cm/s)	Matrix 1 sand	Matrix 2 silt	Matrix 3 clay	Unified Soil	Bulk Percent	Dr Unit Wt.					
6L 1980	H0	3	13	435799	885499	173	15.5	16.0				19	70		SN	26						
6L 1980	H0	3	13	435799	885499	174	4.0	4.5				9	74		SN	26						
6L 1980	H0	99	13	435799	885499	175	2.0	2.5							CL-MH							21
6L 1980	H0	3	13	435799	885499	177	6.0	6.5				8	76		SN	27						
6L 1980	H0	3	13	435799	885499	179	2.0	2.5				2	64	15	SN	38						
6L 1980	H0	3	13	435799	885499	1713	5.5	6.0				14	66		SN	31						
6L 1980	H0	3	13	435799	885499	1714	3.0	3.5				10	76	3	SN	25						
6L 1981	H0	3	13	435744	885445	81	785.4	25.0	26.0	1.80E-04					SC							194
6L 1981	H0	3	13	435744	885445	81	785.4	5.0	6.5			10	56		SC	49						23
6L 1981	H0	12	13	435740	885442	82	807.6	15.0	16.5						SP-SH	6						87
6L 1981	H0	3	13	435740	885437	83	816.3	5.0	6.5			45	84		SP-SH	10						53
6L 1981	H0	3	13	435740	885437	83	816.3	15.0	16.0			13	32		SH	56						128
6L 1981	H0	3	13	435735	885436	84	831.1	10.0	11.5			15	67		SH	30						44
6L 1981	H0	3	13	435735	885443	85	844.5	15.0	16.5			5	81		SH	21						102
6L 1981	H0	3	13	435732	885445	86	855.1	0.5	1.5			7	81		SH	24						
6L 1981	H0	3	13	435737	885445	89	15.0	16.0				8	66		SC	34						
6L 1981	H0	3	13	435737	885448	90	10.0	11.5				16	76		SC	22						
6L 1981	H0	12	13	435737	885448	90	35.0	35.4				8	86		ROCK	14						
6L 1981	H0	3	13	435735	885445	811	25.0	25.4		1.80E-04		10	66		SC	34						
6L 1981	H0	3	13	435735	885445	811	30.0	30.5				6	74		SC	25						
6L 1981	H0	3	13	435734	885443	812	30.0	30.7		7.40E-05		5	73		SC	28						
6L 1981	H0	3	13	435730	885443	812	35.0	35.6		2.50E-06		14	62		SC	35						
6L 1981	H0	3	13	435733	885448	813	30.0	30.5		2.00E-05		19	83		SC	16						
6L 1981	H0	12	13	435733	885448	813	50.0	50.4							ROCK	6						
6L 1985	UN	12	13	435729	885448	M16A	844.3	51.8	58.3		1.17E-04	7			SH-SC	26						300
6L 1985	H0	3	13	435728	885440	M18A	866.8	34.0	35.0			6	76		SH	13						133
6L 1985	H0	4	13	435728	885440	M18A	866.8	39.0	40.0		1.99E-04	7			SH	13						108
6L 1985	H0	12	13	435728	885440	M18A	866.8	54.6	62.6						SH-SC	26						999
6L 1985	H0	3	13	435730	885431	M19B	844.3	24.0	25.0			15	74		SH	26						133
6L 1985	UN	12	13	435730	885431	M19B	844.3	37.0	40.0			0	95		SP	7						73
6L 1985	H0	3	13	435734	885436	820	865.7	24.0	25.0			18	72		SH-SC	29						100
6L 1985	UN	12	13	435734	885436	820	845.7	49.0	50.0			0	95		SP	6						150
6L 1985	UN	12	13	435731	885430	M21A	831.7	32.0	40.0		5.49E-05	7			SP							999
6L 1985	H0	4	13	435735	885428	M22A	817.2	36.6	39.3		3.43E-03	7			SP, SH, SN	27						27
6L 1985	H0	4	13	435735	885428	M22B	817.8	39.0	40.0			22	85		SN	16						40
6L 1985	UN	12	13	435735	885428	M22B	817.8	39.0	40.0		3.20E-05	7			SP, SP-SH	171						171
6L 1985	H0	3	13	435736	885430	M23A	813.4	17.0	28.5		1.93E-05	7			SN	26						26
6L 1985	UN	12	13	435736	885430	M23A	813.4	17.0	28.5			0	96		SP	7						200
6L 1985	UN	12	13	435736	885431	M23B	799.1	8.9	16.0						ROCK							
6L 1985	UN	12	13	435733	885452	M27B	857.8	49.3	76.3		1.56E-04	7			ROCK	18						80
6L 1985	H0	4	13	435740	885431	M28B	799.1	9.0	10.0		2.53E-03	7			SN	19						25
6L 1985	H0	3	13	435733	885452	M27B	857.8	19.0	20.0		1.41E-03	7			SN	24						24
6L 1985	H0	4	13	435740	885431	M28B	799.0	9.0	10.0			6	84		SN	19						216
6L 1985	H0	3	13	435740	885431	M28B	799.0	35.9	42.9		7.31E-06	7			SN	37						37
6L 1985	H0	3	13	435743	885431	M29A	801.5	15.5	21.1		2.95E-04	7			SN	37						37
6L 1985	H0	3	13	435743	885431	M29A	801.5	15.5	21.1		3.02E-04	7			SN	37						37

[illegible]

+ IDENTITY			+ LITHO- strat.			+ COUNTY			+ HYDRAULIC + CONDUCTIVITY			+ GRAINSIZE PERCENTAGES			+ ENGINEERING PROPERTIES			+ ENGINEERING PROPERTIES									
Year	Code	Unit	Mat.	Site	Lat.	Long.	Borg. no.	Elev. top	Surf. Elev.	Bottom	Lab K	Meth	Fld K Meth	Bulk Z	Matrix Z	Matrix Z	Matrix Z	Unified	Bulk	Drv	SPT	Moist.	Liquid Plastic.	UC	Index	(tst)	
								(ft)	(ft)	(ft)	(cc/s)	(cc/s)	(cc/s)	(cc/s)	(cc/s)	(cc/s)	(cc/s)	(cc/s)	(cc/s)	(cc/s)	(cc/s)	(cc/s)	(cc/s)	(cc/s)	(cc/s)	(cc/s)	(cc/s)
KE 1984	OC	5	14	423533	880227	8440	731.2	88.5	90.0									CL	91		86			34	19	2.5	
KE 1984	OC	3	14	423533	880227	8440	731.2	73.5	75.0									CL	91		36					1.5	
KE 1984	OC	3	14	423533	880227	8440	731.2	113.5	115.0									CL	47								
KE 1983	OC	3	14	423529	880221	1845	735.0	18.0	28.0				2.90E-07	7				CL			10						
KE 1983	OC	3	14	423550	880236	1846	715.5	15.5	25.5				2.55E-07	7				CL			20						
KE 1984	OC	3	14	423550	880230	8440	715.5	135.5	135.0									CL	71		100			20	7	4.5	
KE 1984	OC	3	14	423550	880236	8440	715.5	123.5	125.0									CL	25		100						
KE 1983	OC	5	14	423546	880245	8440	745.7	98.5	100.0									CL	94		180			23	8	4.5	
KE 1983	OC	3	14	423546	880245	8440	745.7	98.5	100.0									CL	16		41						
KE 1984	OC	3	14	423542	880247	8440	745.4	53.5	55.0									CL			37			27	13	1.8	
KE 1984	OC	3	14	423542	880247	8440	745.4	68.5	70.0									CL			35			34	19	2.5	
KE 1984	OC	3	14	423542	880247	8440	745.4	68.5	70.0									CL			35			34	19	2.5	
KE 1984	OC	3	14	423542	880247	8440	745.4	68.5	70.0									CL			35			34	19	2.5	
KE 1984	OC	3	14	423542	880247	8440	745.4	68.5	70.0									CL			35			34	19	2.5	
KE 1984	OC	3	14	423542	880247	8440	745.4	68.5	70.0									CL			35			34	19	2.5	
KE 1984	OC	3	14	423542	880247	8440	745.4	68.5	70.0									CL			35			34	19	2.5	
KE 1984	OC	3	14	423542	880247	8440	745.4	68.5	70.0									CL			35			34	19	2.5	
KE 1984	OC	3	14	423542	88																						

[illegible]

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR KENAUKE COUNTY LANDFILL

+ IDENTITY	+ County	+ (code) Year	+ (code) Mat. Site	+ Lat.	+ Long.	+ Eng. No.	+ Surf. Elev. (ft)	+ Sample Elev. (ft)	+ Bot. Elev. (ft)	+ Hyd. Conductivity (cgs)	+ Lab. K (cgs)	+ Meth. code	+ Fld. K Meth. code	+ GRAIN SIZE PERCENTAGES			+ ENGINEERING PROPERTIES			
														Matrix %	Matrix %	Matrix %	Unified Soil Class.	Moist. Content (%)	Liquid Limit (%)	Plastic Index (%)
KW 1980 KEH	3	15	442835	873456	NW7C	744.9	49.0	51.0									CL	15.0	2.0	
KW 1980 KETr	3	15	442827	873456	NW8C	759.3	1.0	2.0									CL	18.0	2.0	
KW 1980 KETr	3	15	442827	873456	NW8C	759.3	2.0	4.0									CL	14.0	3.5	
KW 1980 KETr	3	15	442827	873456	NW8C	759.3	4.0	6.0									CL	13.0	4.5	
KW 1980 KETr	3	15	442827	873456	NW8C	759.3	6.0	8.0									CL	11.0	13	4.5
KW 1980 KETr	3	15	442827	873456	NW8C	759.3	8.0	10.0									CL	13.0	4.5	
KW 1980 KEH	5	15	442827	873456	NW8C	759.3	10.0	12.0									CL	13.0	4.5	
KW 1980 KEH	3	15	442827	873456	NW8C	759.3	15.0	17.0									CL	14.0	2.0	
KW 1980 KEH	3	15	442827	873456	NW8C	759.3	20.0	22.0									ML-CL	17.0	2.3	
KW 1980 KEH	3	15	442827	873456	NW8C	759.3	25.0	27.0									CL	15.0	2.0	
KW 1980 KEH	3	15	442827	873456	NW8C	759.3	30.0	32.0									CL	15.0	2.0	
KW 1980 KEH	3	15	442827	873456	NW8C	759.3	35.0	37.0									CL	13.0	2.5	
KW 1980 KEH	3	15	442827	873456	NW8C	759.3	40.0	42.0									CL	13.0	2.0	
KW 1980 KEH	3	15	442827	873456	NW8C	759.3	45.0	47.0									CL	13.0	2.0	
KW 1980 KEH	3	15	442827	873456	NW8C	759.3	50.0	52.0									CL	13.0	2.0	
KW 1980 UN	4	15	442827	873456	NW8C	759.3	55.0	56.5									SH-SP	13.0	1.8	
KW 1980 UN	4	15	442827	873456	NW8C	759.3	60.0	61.5									SH-SP	13.0	1.8	
KW 1980 KEU	99	15	442827	873456	NW8C	759.3	65.0	66.5									CL	15.0	2.0	
KW 1980 KEU	99	15	442827	873456	NW8C	759.3	70.0	72.0									CL	15.0	1.8	
KW 1980 KEU	99	15	442827	873456	NW8C	759.3	75.0	77.0									CL	14.0	1.7	
KW 1980 KEU	99	15	442827	873456	NW8C	759.3	80.0	82.0									CL	18.0	3.0	
KW 1980 UN	5	15	442827	873456	NW8C	759.3	85.0	87.0									ML-CL	17.0		
KW 1980 UN	5	15	442827	873456	NW8C	759.3	90.0	91.5									ML-CL	21		
KW 1980 UN	5	15	442827	873456	NW8C	759.3	95.0	96.6									ML-CL	21		
KW 1980 UN	5	15	442827	873456	NW8C	759.3	100.0	102.0									CL	24.0	2.0	
KW 1980 UN	99	15	442827	873456	NW8C	759.3	105.0	107.0									CL	22.0	2.0	
KW 1980 NB	99	15	442827	873456	NW8C	759.3	115.0	116.5									SP, SH-SP			
KW 1980 NB	99	15	442827	873456	NW8C	759.3	120.0	121.5									SP, SH-SP	88		
KW 1980 NB	99	15	442827	873456	NW8C	759.3	125.0	126.5									SP, SH-SP	87		
KW 1980 NB	99	15	442827	873456	NW8C	759.3	130.0	131.5									SP, SH-SP	122		
KW 1980 NB	99	15	442827	873456	NW8C	759.3	135.0	136.5									SP, SH-SP	112		
KW 1980 NB	99	15	442827	873456	NW8C	759.3	140.0	141.5									SP, SH-SP	52		
KW 1980 UN	3	15	442827	873456	NW8C	759.3	145.0	146.5									SH-SP, ML	160		
KW 1980 NB	99	15	442835	873456	NW1	756.3	30.0	31.5									CL	141		
KW 1980 KEH	99	15	442822	873456	NW2	761.7	30.0	32.0									CL	53		
KW 1980 KEH	99	15	442822	873456	NW2	761.7	35.0	37.0									CL	13.0	1.5	
KW 1980 KEH	99	15	442822	873456	NW2	761.7	40.0	42.0									CL	13.0	1.5	
KW 1980 KEH	99	15	442822	873456	NW2	761.7	45.0	47.0									CL	14.0	1.0	
KW 1980 KETr	3	15	442827	873440	NW3	744.8	2.0	4.0									CL	14.0	2.0	
KW 1980 KETr	3	15	442827	873440	NW3	744.8	4.0	6.0									CL	18.0	1.6	
KW 1980 KETr	3	15	442827	873440	NW3	744.8	6.0	8.0									CL	14.0	4.5	
KW 1980 KETr	3	15	442827	873440	NW3	744.8	8.0	10.0									CL	12.0	3.5	
KW 1980 KETr	3	15	442827	873440	NW3	744.8	10.0	12.0									CL	12.0	4.5	
KW 1980 KETr	3	15	442827	873440	NW3	744.8	15.0	17.0									CL	15.0	2.5	
KW 1980 KETr	3	15	442827	873440	NW3	744.8	20.0	22.0									CL	15.0	1.5	
KW 1980 KETr	3	15	442827	873440	NW3	744.8	25.0	26.0									CL			

+ IDENTITY			+ Litho-		+ County			+ Strat.			+ Unit			+ Site			+ Lat.			+ Long.			+ Brnd. no.			+ Surf. Elev.			+ Top			+ Bottom			+ Lab X			+ Meth			+ Fld K			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix Z			+ Matrix X			+ Matrix Y			+ Matrix 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Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR KENAWANEE COUNTY LANDFILL

+ IDENTITY	+ County	+ (code)	+ Year	+ Litho- strat.	+ Mat. Site	+ Lat.	+ Long.	+ Elev. top (ft)	+ Surf. Elev. top (ft)	+ Sample (ft)	+ HYDRAULIC		+ SOILSIZE PERCENTAGES				+ ENGINEERING PROPERTIES				+ SPf Moist. Liquid Plastic. UC	+ (10) cont. (2) limit index (1st) +			
											Lab K	Conductivity	Matrix 1	Matrix 2	Matrix 3	Matrix 4	Unified	Soil	Class.	P200					
											Lab K	Conductivity	Fld K Meth	Bulk 1	Bulk 2	Matrix 1	Matrix 2	Matrix 3	Matrix 4	Unified	Soil	Class.	P200	Percent	
											(cm/s)	(cm/s)	(cm/s)	(cm/s)	(cm/s)	(cm/s)	(cm/s)	(cm/s)	(cm/s)	(cm/s)	(cm/s)	(cm/s)	(cm/s)	(cm/s)	(cm/s)
KW 1982 KE1r	3	15	442824	873505	B29	761.0	4.0	5.0	2.40E-08	1	1.40E-08	1	8	35	47	18	CL	CL	CL	64	124.3	12.0	4.0	2.0	
KW 1982 KE1r	3	15	442826	873505	B30	761.9	4.0	7.5	1.40E-08	1	1.40E-08	1	8	32	52	16	CL	CL	CL	65	123.0	14.0	2.5	2.5	
KW 1982 KE1r	3	15	442827	873505	B31	763.8	10.0	11.5	3.14E-08	1	3.14E-08	1	6	35	51	14	CL	CL	CL	65	115.5	16.0	2.5	2.5	
KW 1982 KE1r	3	15	442828	873505	B32	764.9	2.0	4.0	3.30E-07	1	3.30E-07	1	6	41	50	9	CL	CL	CL	62	129.7	13.0	2.0	2.0	
KW 1982 KE1r	3	15	442829	873505	B33	765.4	10.0	11.5	3.60E-08	1	3.60E-08	1	16				CL	CL	CL	65			2.5	2.5	
KW 1982 KE1r	3	15	442825	873511	B34	765.1	2.0	4.0	1.90E-08	1	1.90E-08	1	16				CL	CL	CL	65			4.5	4.5	
KW 1982 KE1r	3	15	442825	873509	B35	761.5	4.0	6.0	1.30E-08	1	1.30E-08	1	16				CL	CL	CL	65			1.0	1.0	
KW 1982 KE1r	3	15	442825	873508	B36	760.4	4.0	8.0	5.60E-07	1	5.60E-07	1	8				CL	CL	CL	67			1.8	1.8	
KW 1982 KE1r	3	15	442825	873507	B37	759.5	8.0	10.0	2.30E-08	1	2.30E-08	1	8				CL	CL	CL	68			4.5	4.5	
KW 1982 KE1r	3	15	442824	873506	B38	759.2	2.0	2.5	7.50E-09	1	7.50E-09	1	10				CL	CL	CL	65			1.5	1.5	
KW 1982 KE1r	3	15	442826	873506	B39	759.2	8.0	10.0	4.90E-09	1	4.90E-09	1	10				CL	CL	CL	65			1.0	1.0	
KW 1982 KE1r	3	15	442827	873506	B40	756.8	4.0	8.0	2.00E-08	1	2.00E-08	1	10				CL	CL	CL	72			1.2	1.2	
KW 1982 KE1r	3	15	442827	873506	B41	755.0	4.0	8.0	1.60E-08	1	1.60E-08	1	10				CL	CL	CL	59			1.5	1.5	
KW 1982 KE1r	3	15	442828	873506	B42	753.6	4.0	8.0	3.70E-08	1	3.70E-08	1	10				CL	CL	CL	59			2.0	2.0	
KW 1982 KE1r	3	15	442829	873506	B43	753.9	2.0	4.0	5.90E-07	1	5.90E-07	1	5.8				CL	CL	CL	67			2.0	2.0	
KW 1982 KE1r	3	15	442829	873506	B44	753.8	12.0	14.0	1.20E-08	1	1.20E-08	1	6.9				CL	CL	CL	67	122.0				
KW 1982 KE1r	3	15	442824	873507	IP45	760.0	0.0	1.0	6.70E-08	3	6.70E-08	3	8.4				CL	CL	CL	64	115.4			4.5	
KW 1982 KE1r	3	15	442824	873508	IP46	761.0	0.0	6.5	7.80E-09	1	7.80E-09	1	6.4				CL	CL	CL	67	126.7			11.0	
KW 1982 KE1r	3	15	442824	873508	IP46	761.0	0.0	1.5					6.4				CL	CL	CL	67	119.3			127.9	
KW 1982 KE1r	3	15	442824	873510	IP47	762.0	0.0	3.5									CL	CL	CL	67	126.3				
KW 1982 KE1r	3	15	442824	873512	IP48	763.0	0.0	3.5									CL	CL	CL	67	126.3				

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR MANITOWOC COUNTY INCLUDING LENSEBER, PROPOSED MANITOWOC COUNTY, AND RIDGEVIEW SITES

+ IDENTITY	+ Litto- strat. unit	+ Conty (code)	+ Year (code)	+ Lat.	+ Long.	+ Brng.	+ Elev. (ft)	+ Sample top (ft)	+ Sample bottom (ft)	+ Lab K (cm/s)	+ Meth code	+ Hydralic conductivity (cm/s)	+ GRAINSIZE PERCENTAGES				+ ENGINEERING PROPERTIES				+ SPT Moist. Unit Mt. (pcf)	+ Liquid Plastic. Index (%)	+ UC (test)
													Matrix I	Matrix II	Matrix III	Matrix IV	Matrix V	Matrix VI	Matrix VII	Matrix VIII	Matrix IX	Matrix X	Matrix XI
NR 1978 UN 99 16 441099 874999 CS1	UN	99	16	441099	874999	CS1	20.0	30.0	42	90			42	90									
NR 1978 UN 99 16 441099 874999 CS2	UN	99	16	441099	874999	CS2	30.0	45.0	46	89			46	89									
NR 1978 UN 99 16 441099 874999 CS3	UN	99	16	441099	874999	CS3	30.0	45.0	52	100			52	100									
NR 1978 KEVA 3 16 441099 874999 B24	KEVA	3	16	441099	874999	B24	15.0	16.5	4	26	45		45	26	45								
NR 1978 KEVA 3 16 441099 874999 B24	KEVA	3	16	441099	874999	B24	33.0	38.5	3	30	44		44	26	44								
NR 1978 KEVA 3 16 441099 874999 B24	KEVA	3	16	441099	874999	B24	8.0	10.0	19	38	44		44	17	38								
NR 1978 UN 4 16 441040 875012 B27	UN	4	16	441040	875012	B27	45.0	46.5	4	30	44		44	26	44								
NR 1978 UN 4 16 441040 875012 B27	UN	4	16	441040	875012	B27	25.0	26.5	6	39	49		49	12	39								
NR 1978 UN 4 16 441040 875012 B27	UN	4	16	441040	875012	B27	30.0	30.5	10	40	49		49	11	40								
NR 1978 KEVA 3 16 441099 874999 TS1	KEVA	3	16	441099	874999	TS1	0.0	2.0															
NR 1978 KEVA 3 16 441099 874999 TS2	KEVA	3	16	441099	874999	TS2	0.0	2.0															
NR 1979 UN 12 16 441030 875010 B29	UN	12	16	441030	875010	B29	875.3	4.0	16.0	3	15	48	48	36	15								
NR 1979 KEVA 3 16 441030 875010 B29	KEVA	3	16	441030	875010	B29	875.3	60.0	73.0	3	15	48	48	36	15								
NR 1979 KEVA 3 16 441030 875010 B30	KEVA	3	16	441030	875010	B30	875.3	13.0	15.0	7	41	43	43	16	41								
NR 1979 KEVA 3 16 441030 875005 B31	KEVA	3	16	441030	875005	B31	880.5	6.0	16.0	19	86	45	40	15	18								
NR 1980 UN 4 16 441030 874950 B33	UN	4	16	441030	874950	B33	20.0	21.5	2	90													
NR 1980 UN 4 16 441030 874950 B33	UN	4	16	441030	874950	B33	25.0	26.5	7	41	43												
NR 1980 UN 99 16 441030 874944 B34	UN	99	16	441030	874944	B34	30.0	31.5	19	86	45												
NR 1980 UN 3 16 441030 874944 B34	UN	3	16	441030	874944	B34	15.0	15.7	18	45	40												
NR 1982 UN 3 16 441032 875008 B59	UN	3	16	441032	875008	B59	881.1	31.0	33.0	2	63												
NR 1982 KE 4 16 441032 875008 B59	KE	4	16	441032	875008	B59	881.1	9.5	11.0	47	53												
NR 1982 UN 3 16 441032 875008 B59	UN	3	16	441032	875008	B59	881.1	44.5	46.0	1	12	60	60	28	12								
NR 1982 KEVA 3 16 441032 875008 B59	KEVA	3	16	441032	875008	B59	881.1	4.5	6.0	7	27	49	49	24	24								
NR 1982 KEVA 5 16 441034 875007 B60	KEVA	5	16	441034	875007	B60	889.0	11.0	12.5	0	99												
NR 1982 KEVA 3 16 441034 875007 B60	KEVA	3	16	441034	875007	B60	889.0	9.5	11.0	9	32	48	48	20	20								
NR 1982 UN 3 16 441034 875007 B60	UN	3	16	441034	875007	B60	889.0	24.5	26.0	18	39	44	44	17	17								
NR 1982 KE 3 16 441099 875099 B61	KE	3	16	441099	875099	B61	906.3	14.5	16.0	0	0												
NR 1982 KEVA 3 16 441099 875099 B61	KEVA	3	16	441099	875099	B61	906.3	4.5	6.5	7	27	49	49	24	24								
NR 1982 UN 3 16 441034 875001 B62	UN	3	16	441034	875001	B62	918.2	4.5	6.0	22	36	45	45	19	19								
NR 1982 UN 3 16 441034 875001 B62	UN	3	16	441034	875001	B62	918.2	44.5	46.0	56	64												
NR 1982 UN 3 16 441034 875001 B62	UN	3	16	441034	875001	B62	918.2	29.5	31.0	64	78												
NR 1982 UN 3 16 441035 875003 B63	UN	3	16	441035	875003	B63	903.3	44.5	46.0	57	72												
NR 1982 KEVA 3 16 441035 875003 B63	KEVA	3	16	441035	875003	B63	903.3	9.5	12.0	15	28	48	48	24	24								
NR 1982 UN 3 16 441035 875003 B63	UN	3	16	441035	875003	B63	903.3	24.5	26.0	53	60												
NR 1982 KEVA 3 16 441040 875003 B64	KEVA	3	16	441040	875003	B64	904.9	34.5	36.0	20	95												
NR 1982 UN 4 16 441040 875003 B64	UN	4	16	441040	875003	B64	904.9	34.5	36.0	20	95												
NR 1982 UN 3 16 441040 875003 B64	UN	3	16	441040	875003	B64	904.9	29.5	31.0	21	13	66	66	29	29								
NR 1982 KEVA 3 16 441033 874953 B65	KEVA	3	16	441033	874953	B65	883.7	34.5	36.0	27	49												
NR 1982 UN 3 16 441033 874953 B65	UN	3	16	441033	874953	B65	883.7	19.5	21.0	16	18	26	26	32	32								
NR 1982 KEVA 3 16 441033 874953 B65	KEVA	3	16	441033	874953	B65	883.7	9.5	11.0	23	29	47	47	25	25								

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR MANITOWOC COUNTY INCLUDING LENEXER, PROPOSED MANITOWOC COUNTY, AND RIDGEVIEW SITES

+ IDENTITY		+ County		+ (code)		+ Year		+ Litho- strat.		+ Unit		+ Nat. Site		+ Lat.		+ Long.		+ Brg. no.		+ Elev. (ft)		+ Sample top (ft)		+ Sample bottom (ft)		+ Lab K (cm/s)		+ Lab K (cm/s) code		+ Filz K (cm/s) code		+ Matrix 1 sand (2.0 to 10.025 to 0.002mm)		+ Matrix 2 silt (10.025 to 0.002mm)		+ Matrix 3 clay (0.002mm)		+ ENGINEERING PROPERTIES										+ Moist. Plastic. Index		+ Liquid Limit		+ Plasticity Index																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																			
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IDENTITY	Litho- strat.	County unit	Nat. Site No.	Year	(code)	Lat.	Long.	Brgc. no.	Elev. top	Surf. bottom	Sample size	HYDRAULIC + CONDUCTIVITY		GRAIN SIZE PERCENTAGES		ENGINEERING PROPERTIES					
												Lab K (cm/s)	Hyd K (ft)	Fld K (cm/s)	Bolt Z (0.002mm)	Matrix X sand silt (0.075 to 0.002mm)	Matrix Y clay (0.002mm)	Unified Soil Class.	Dry Bulk Percent P200	Unit Wt. (pcf)	SPT Moist. (blows) Liquid Plasticity Index
MN 1983 KEVA	3	16	441013	874951	TP20	919.8	10.0	11.0				13	24	47	29	CL	77	28	18		
MN 1983 KEVA	3	16	441014	874945	TP21	896.7	7.0	8.0				9	30	47	23	CL	66				
MN 1983 KEVA	3	16	441014	874946	TP22	888.8	8.0	9.0				11	39	44	17	CL	55	20	9		
MN 1983 KEVA	3	16	441008	874952	TP25	915.9	9.0	10.0				10	29	47	24	CL	65	23	13		
MN 1983 KEVA	3	16	441008	874946	TP26	896.6	5.0	6.0				9	20	46	34	CL	74	31	19		
MN 1983 KEVA	3	16	441004	874950	TP27	901	4.0	5.0				7	30	45	25	CL	67	23	13		
MN 1983 KEVA	3	16	441035	874945	TP28	874.7	9.0	10.0				10	38	43	19	CL	59	20	9		
MN 1983 UN	3	16	441037	875010	TP3	897.2	16.5	17.5				13	25	48	26	CL	66	23	14		
MN 1983 KEVA	3	16	441024	874942	TP50	885	7.0	8.0				11	26	47	27	CL	67	28	17		
MN 1983 KEVA	3	16	441032	874944	TP31	882	3.0	4.0				6				CL-ML	64				
MN 1983 KEVA	3	16	441032	874944	TP31	882	11.0	12.0				12	26	47	27	CL	63	28	17		
MN 1983 KE	4	16	441039	875007	TP4	899	17.0	18.0				12	39			SP-SH	40				
MN 1983 KEVA	3	16	441040	875004	TP8	908.3	6.0	7.0				21	38	43	19	SH	50	21	12		
MN 1983 UN	3	16	441040	875004	TP6	908.3	17.0	18.0				49	39			SH-SF	23				
MN 1983 UN	3	16	441044	875007	TP7	906.5	11.0	12.0				13	38	45	17	CL	55	19	9		
MN 1983 UN	3	16	441044	875007	TP7	906.5	19.0	20.0				9	23	49	27	CL	71	23	13		
MN 1983 KE	4	16	441044	875007	TP7	906.5	4.0	5.0				6	69			SH	35				
MN 1983 KEVA	3	16	441044	875003	TP8	913.2	10.0	11.0				14	41	44	15	CL	53	19	10		
MN 1983 UN	3	16	441044	875003	TP8	913.2	19.0	20.0				37	51	41	8	SH-SF	32				
MN 1983 UN	3	16	441045	875008	TP9	898.7	10.0	11.0				13	31	47	22	CL	61	22	11		
MN 1983 UN	5	16	441045	875008	TP9	898.7	23.0	24.0				0	10	49	41	CL	93	35	24		

[illegible]

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR MARQUETTE COUNTY

+ IDENTITY		Litho- strat. unit	Mat. Site (code) Year (code)	No.	Lat.	Long.	Brng. Elev. no. (ft)	Surf. Elev. top (ft)	+ HYDRAULIC + CONDUCTIVITY		+ GRAIN SIZE PERCENTAGES				+ ENGINEERING PROPERTIES					
+ County	+ State								bot. (ft)	top (ft)	Lab K (cm/s)	Fld K Meth (cm/s) code	Bulk 2 (2.0 to 0.0625 to 0.002mm)	Matrix 1 sand	Matrix 2 silt clay	Unified Soil Class.	P200 (pcf)	Percent Unit Wt.	SPT	Moist. Liquid Plastic. UC
MD 1979	UN	5	19	434710	892842	87	816.7	10.0			2	46	EL	57			20	9		
MD 1979	UN	5	19	434710	892842	87	816.7	25.0			2	19	CL	79			32	16		
MD 1979	UN	5	19	434709	892846	88	836.4	5.0			0	21	CH	80			51	30		
MD 1979	UN	5	19	434709	892846	88	836.4	10.0			2	62	SH	43						
MD 1979	UN	5	19	434709	892846	88	836.4	15.0			0	19	CL	82			31	13		
MD 1978	UN	5	19	434708	892851	89	844.0	5.0			1	64	SC	39			23	11		
MD 1978	UN	5	19	434708	892851	89	844.0	20.0			0	67	SH	48						
MD 1978	UN	5	19	434703	892854	810	860.5	10.0			0	52	CL	49			22	8		
MD 1978	UN	5	19	434703	892854	810	860.5	15.0			6	32	CL	65			21	10		
MD 1978	UN	5	19	434703	892854	810	860.5	25.0			5	82	SH	19						
MD 1978	UN	5	19	434712	892855	812	868.7	20.0			6	32	EL	66			25	8		
MD 1978	UN	5	19	434709	892858	814	870.2	10.0			2	30	CL	70			24	8		
MD 1978	UN	5	19	434709	892858	814	870.2	25.0			3	84	SH	21						
MD 1978	UN	5	19	434709	892858	815	861.9	10.0			2	46	CL-ML	55			19	5		
MD 1978	UN	5	19	434716	892846	816	811.9	15.0			0	10	CL-ML	91			22	4		
MD 1978	UN	5	19	434713	892846	817	833.7	15.0			1	39	CL-ML	62			18	6		
MD 1978	UN	5	19	434716	892841	818	832.7	10.0			3	41	CL-ML	59			20	7		
MD 1978	UN	5	19	434716	892841	818	832.7	20.0			0	27	CL-ML	76			21	8		

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR RACINE COUNTY - (WEPCD) CALEDONIA SITE

+ IDENTITY		+ HYDRAULIC										+ GRAINSIZE PERCENTAGES										+ ENGINEERING PROPERTIES									
+ County		Litho- strat. unit	Mat.	Site	+ CONDUCTIVITY		+ Matrix		+ Matrix		+ Matrix		+ Unified		+ Bulk		+ Dry		+ SPT		+ Moist.		+ Liquid		+ Plastic		+ UC		+ Index		
(code)	Year	(code)	(code)	No.	Lat.	Long.	Brng.	Elev.	top	bottom	Lab K	Meth	Fld K	Meth	Bulk	Y (2.0 to	0.0625mm	0.002mm	<(0.002mm)	+ Class.	Soil	Percent	Unit Wt.	SPT	Moist.	Liquid	Plastic	UC	Index	(tsf)	
(code)	Year	(code)	(code)	No.	Lat.	Long.	no.	(ft)	(ft)	(ft)	(cm/s)	code	(cm/s)	code	>2.0mm	0.0625mm	0.002mm	<(0.002mm)		Class.	P200	(pcf)	(N)	cont. (%)	limit	index	(tsf)				
Ra	1977	OC	3	20	425031	875028	C1	705.6	1.5						0	32	50	10			74		4						1.0		
Ra	1977	OC	3	20	425031	875028	C1	705.6	5.0						0	11	64	25			91		23						4.5		
Ra	1977	OC	3	20	425031	875028	C1	705.6	10.0						0	11	64	25			91		14						4.5		
Ra	1977	OC	3	20	425031	875028	C1	705.6	15.0						0	11	69	30			92		15						4.0		
Ra	1977	OC	3	20	425031	875028	C1	705.6	20.0						0	10	62	28			93		14						3.5		
Ra	1977	OC	3	20	425031	875028	C1	705.6	25.0						0	8	65	27			94		16								
Ra	1977	OC	5	20	425031	875028	C1	705.6	30.0						13	84					15		11								
Ra	1977	OC	5	20	425031	875028	C1	705.6	35.0						3	11	68	21			88		19						4.5		
Ra	1977	OC	5	20	425031	875028	C1	705.6	40.0						0	15	71	14			90		46								
Ra	1977	OC	99	20	425025	875033	C2	711.8	1.5						0	14	62	24			89		3						1.8		
Ra	1977	OC	3	20	425025	875033	C2	711.8	5.0						0	13	64	23			91		22						4.5		
Ra	1977	OC	3	20	425025	875033	C2	711.8	10.0						0	10	65	25			92		25						4.5		
Ra	1977	OC	3	20	425025	875033	C2	711.8	15.0						0	8	62	30			94		18						4.5		
Ra	1977	OC	3	20	425025	875033	C2	711.8	20.0						0	4	61	35			97		11						2.5		
Ra	1977	OC	5	20	425025	875033	C2	711.8	25.0						0		92	7			100		20						2.8		
Ra	1977	OC	3	20	425025	875033	C2	711.8	30.0						14	26	57	17			64		11						2.5		
Ra	1977	OC	3	20	425025	875033	C2	711.8	35.0						0	9	71	20			92		15						1.8		
Ra	1977	OC	3	20	425025	875033	C2	711.8	40.0						0	10	73	17			92		14						1.5		
Ra	1977	OC	99	20	425024	875023	C3	696.9	1.5						2	19	51	30			82		3						1.5		
Ra	1977	OC	3	20	425024	875023	C3	696.9	5.0							13	64	23			89		12						3.0		
Ra	1977	OC	3	20	425024	875023	C3	696.9	10.0							9	68	23			92		21						4.5		
Ra	1977	OC	3	20	425024	875023	C3	696.9	15.0						3	8	69	23			91		18						4.5		
Ra	1977	OC	5	20	425024	875023	C3	696.9	20.0						0	3	89	8			98		15						2.5		
Ra	1977	OC	99	20	425024	875023	C3	696.9	25.0							3	62	35			97		14						3.5		
Ra	1977	OC	99	20	425024	875023	C3	696.9	30.0						0	10	55	35			91		13						3.0		
Ra	1977	OC	99	20	425024	875023	C3	696.9	35.0						3	11	60	29			98		15						4.0		
Ra	1977	OC	99	20	425024	875023	C3	696.9	40.0						3	15	64	21			84		10						2.0		
Ra	1977	OC	5	20	425020	875047	C4	698.4	1.5						0	20	65	15			82		3								
Ra	1977	OC	5	20	425020	875047	C4	698.4	5.0						12	32	57	11			63		14						2.0		
Ra	1977	OC	5	20	425020	875047	C4	698.4	10.0						16	26	60	14			54		15						2.0		
Ra	1977	OC	5	20	425020	875047	C4	698.4	15.0						0	4	49	47			96		11						3.0		
Ra	1977	OC	3	20	425020	875047	C4	698.4	20.0						0		49	50			99		14						3.5		
Ra	1977	OC	5	20	425020	875047	C4	698.4	25.0						0	3	47	50			99		12						3.0		
Ra	1977	OC	5	20	425020	875047	C4	698.4	30.0						0	2	53	45			99		9						2.0		
Ra	1977	OC	5	20	425020	875047	C4	698.4	35.0						0	3	45	52			98		11						1.8		
Ra	1977	OC	5	20	425020	875047	C4	698.4	40.0						0	2	48	50			99		9						2.8		
Ra	1977	OC	3	20	425019	875032	C5	703.5	1.5							17	55	28			85		4						2.0		
Ra	1977	OC	3	20	425019	875032	C5	703.5	5.0						2	10	64	26			90		18						4.5		
Ra	1977	OC	5	20	425019	875032	C5	703.5	10.0						16	58	36	6			37		18								
Ra	1977	OC	5	20	425019	875032	C5	703.5	15.0						25	83	16			15		19									
Ra	1977	OC	5	20	425019	875032	C5	703.5	20.0						10	78	20	2			22		11								
Ra	1977	OC	5	20	425019	875032	C5	703.5	25.0						13	72	23	5			26		13								
Ra	1977	OC	5	20	425019	875032	C5	703.5	30.0						0	10	79	11			95		20						4.5		
Ra	1977	OC	3	20	425019	875032	C5	703.5	35.0						0	7	49	44			96		11						3.0		
Ra	1977	OC	3	20	425019	875032	C5	703.5	40.0						2	6	63	31			94		15						3.3		
Ra	1977	OC	99	20	425016	875041	C6	696.0	1.5						0	15	65	20			89		2								



[illegible]

+ IDENTITY	+ Litho- unit	+ County + (code)	+ Year (code)	+ Mat. Site (code)	+ Lat.	+ Long.	+ Brng. no.	+ Surf. Elev. (ft)	+ Sample top (ft)	+ HYDRAULIC + CONDUCTIVITY		+ GRAIN SIZE PERCENTAGES			+ ENGINEERING PROPERTIES					+ SPT index (tsf)
										Lab K (cm/s)	Lab K (cm/s)	Matrix Z sand	Matrix Z silt	Matrix Z clay	Unif. Bulk Dry Percent Unit Wt. Sml (pcf)	Class.	Moist. Liquid Plastic. Shrinkage			
Ra 1977 OC	5	20	425099	875099	B2	713.3	25.0					0	23	68	9	84			9	2.0
Ra 1977 OC	97	20	425099	875099	B3	688.3	1.5					0	18	66	16	86			3	
Ra 1977 OC	3	20	425099	875099	B3	688.3	5.0					0	12	53	35	90			10	2.8
Ra 1977 OC	3	20	425099	875099	B3	688.3	10.0					0	2	53	45	99			9	2.3
Ra 1977 OC	3	20	425099	875099	B3	688.3	15.0					0	11	61	28	91			13	4.3
Ra 1977 OC	97	20	425099	875099	B3	688.3	20.0					0	74	24	2	43			11	
Ra 1977 OC	3	20	425099	875099	B3	688.3	25.0					0	9	41	30	93			15	4.5
Ra 1977 OC	97	20	425099	875099	B4	699.6	1.5					1	25	57	18	76			3	
Ra 1977 OC	3	20	425099	875099	B4	699.6	5.0					2	7	67	26	93			25	4.5
Ra 1977 OC	3	20	425099	875099	B4	699.6	10.0					3	7	62	31	92			28	4.5
Ra 1977 OC	5	20	425099	875099	B4	699.6	15.0					3	5	69	26	84			12	3.5
Ra 1977 OC	3	20	425099	875099	B4	699.6	20.0					0	83	15	2	23			16	
Ra 1977 OC	3	20	425099	875099	B4	699.6	25.0					1	8	62	30	93			10	2.0
Ra 1980 OC	5	20	425018	875052	B41		5.0	6.5				0							28	4.5
Ra 1980 OC	3	20	425018	875052	B41		10.0	11.5				0							21	2.5
Ra 1980 OC	3	20	425018	875052	B41		15.0	16.5				0							25	2.6
Ra 1980 OC	3	20	425018	875052	B41		20.0	21.5				0							18	2.0
Ra 1980 OC	35	20	425018	875052	B41		25.0	27.0				0							23	4.5
Ra 1980 OC	3	20	425018	875052	B41		30.0	31.5				0							45	2.5
Ra 1980 OC	3	20	425018	875052	B41		35.0	36.5				0							22	2.6
Ra 1980 OC	3	20	425018	875052	B41		40.0	41.5				0							15	1.0
Ra 1980 OC	3	20	425018	875052	B41		45.0	47.0				0							8	1.0
Ra 1980 OC	3	20	425018	875052	B41		50.0	51.5				0							10	1.3
Ra 1980 OC	3	20	425018	875052	B41		55.0	56.5				0							38	2.5
Ra 1980 OC	3	20	425018	875052	B41		60.0	61.5				0							37	4.5
Ra 1980 OC	3	20	425018	875052	B41		65.0	66.5				0							64	2.5
Ra 1980 OC	3	20	425018	875052	B41															



Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR RACINE COUNTY - (MEPCO) CALEDONIA SITE

+ IDENTITY		+ HYDRAULIC + CONDUCTIVITY										+ GRAINSIZE PERCENTAGES				+ ENGINEERING PROPERTIES									
+ County	Litho-strat.	Mat.	Site	Brng.	Elev.	Surf.	Sample	Sample	Lab K	Meth	Fld K	Meth	Bulk X	Matrix X	Matrix X	Matrix X	Unified	Bulk	Dry	SP	Moist.	Liquid	Plastic.	UC	
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	
(code)	Year	(code)	(code)	No.	Lat.	Long.	no.	(ft)	(ft)	(ft)	(cm/s)	code	(cm/s)	code	(2.0 to 0.0625mm)	(0.0625 to 0.002mm)	(0.002mm)	Class.	P200	Unit Wt. (pcf)	(%)	cont. (%)	limit	index	
Ra	1980	OC	3	20	425016	875038	BAS	14.0	16.0									CL	93					4.5	
Ra	1980	OC	3	20	425016	875038	BAS	19.0	21.0									CL	92					2.0	
Ra	1980	OC	3	20	425016	875038	BAS	24.0	26.0	2.34E-08								CL	93					2.5	
Ra	1980	OC	3	20	425016	875038	BAS	29.0	31.0									CL	90					2.2	
Ra	1980	OC	3	20	425016	875038	BAS	4.0	6.0									CL	88					4.5	
Ra	1980	OC	3	20	425016	875038	BAS	9.0	11.0	1.67E-08								CL	95					2.0	
Ra	1980	OC	3	20	425016	875038	BAS	14.0	16.0									CL	93					2.2	
Ra	1980	OC	3	20	425016	875038	BAS	19.0	21.0									CL	90					2.0	
Ra	1980	OC	3	20	425016	875038	BAS	24.0	26.0									CL	91					2.0	
Ra	1980	OC	5	20	425016	875038	BAS	499.9	5.0	6.0								CL	99		13			3.5	
Ra	1980	OC	5	20	425016	875038	BAS	499.9	6.0	6.5								SH	28		25				
Ra	1980	OC	5	20	425016	875038	BAS	499.9	10.0	11.5								SH	13		29			1.5	
Ra	1980	OC	3	20	425016	875038	BAS	499.9	15.0	16.5								CL	100		19			2.0	
Ra	1980	OC	3	20	425016	875038	BAS	499.9	20.0	21.5								CL	92		15			2.0	
Ra	1980	OC	3	20	425016	875038	BAS	499.9	25.0	26.5								CL	96		15				
Ra	1980	OC	3	20	425016	875038	BAS	499.9	30.0	31.5								CL	97		15			1.0	
Ra	1980	OC	3	20	425016	875038	BAS	499.9	35.0	36.5								CL	91		14			1.0	
Ra	1980	OC	3	20	425016	875038	BAS	499.9	40.0	41.5								CL	93		21			1.3	
Ra	1980	OC	5	20	425016	875038	BAS	499.9	45.0	47.0	1.76E-08							CL	89					2.2	
Ra	1980	OC	3	20	425016	875038	BAS	499.9	50.0	51.5								CL	92		25			1.5	
Ra	1980	OC	5	20	425020	875041	B86	4.0	6.0									CL	88					4.5	
Ra	1980	OC	5	20	425020	875041	B86	9.0	11.0									CL	90					4.5	
Ra	1980	OC	5	20	425020	875041	B86	14.0	16.0	3.98E-08								CL	94					2.2	
Ra	1980	OC	5	20	425020	875041	B86	19.0	21.0									CL-HL	90					2.0	
Ra	1980	OC	3	20	425012	875035	B87	4.0	5.5									CL	92					2.0	
Ra	1980	OC	3	20	425012	875035	B87	9.0	10.5									CL	91		33			4.5	
Ra	1980	OC	3	20	425012	875035	B87	14.0	16.0	7.95E-09								CL	89		33			4.5	
Ra	1980	OC	5	20	425012	875035	B87	19.0	21.0									CL	92					3.2	
Ra	1980	OC	3	20	425012	875035	B87	24.0	26.0									CL	90					4.0	
Ra	1980	OC	5	20	425009	875023	B88	4.0	5.5									CL	94					3.5	
Ra	1980	OC	3	20	425009	875023	B88	9.0	10.5									CL	58		16				
Ra	1980	OC	3	20	425009	875023	B88	14.0	16.0									CL	100		34			4.5	
Ra	1980	OC	5	20	425009	875023	B88	19.0	21.0									CL	99					3.0	
Ra	1980	OC	3	20	425009	875023	B88	24.0	26.0									CL	99					3.5	
Ra	1980	OC	5	20	425020	875021	B89	4.0	5.5									CL	97					4.5	
Ra	1980	OC	5	20	425020	875021	B89	9.0	10.5									CL	86		32			4.5	
Ra	1980	OC	3	20	425020	875021	B89	14.0	16.0	1.77E-08								CL	89		54			4.5	
Ra	1980	OC	3	20	425020	875021	B89	19.0	21.0									CL	90					2.5	
Ra	1980	OC	3	20	425020	875021	B89	24.0	26.0									CL	92					4.3	
Ra	1980	OC	3	20	425024	875022	B810	4.0	5.5									CL	87		31			3.5	
Ra	1980	OC	5	20	425024	875022	B810	9.0	10.5									CL	80		39			4.5	
Ra	1980	OC	5	20	425024	875022	B810	14.0	16.0	6.58E-05								HL	76					3.3	
Ra	1980	OC	3	20	425024	875022	B810	19.0	21.0	5.42E-08								CL	84					4.5	
Ra	1980	OC	3	20	425024	875022	B810	24.0	25.5									CL	89		33			2.5	
Ra	1980	OC	3	20	425020	875028	B811	4.0	5.5									CL	88		41			4.5	

[illegible]

[illegible]

+ IDENTITY			+ LITHO- + strat-			+ HYDRAULIC + CONDUCTIVITY			+ BRAINSTE PERCENTAGES			+ ENGINEERING PROPERTIES			+ UNITED STATES		
+ County	+ (code)	+ Year	+ unit	+ Mat.	+ Site	+ Surt.	+ Elev.	+ Top	+ Bottom	+ Spacie	+ (ft)	+ (ft)	+ (ft)	+ (ft)	+ (ft)	+ (ft)	+ (ft)
+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)
MI	1978	06	3	21	425053	880348	P28	872.9	85.0	87.0							
MI	1978	06	99	21	425053	880340	P29	792.7	15.0	17.0							
MI	1978	06	99	21	425056	880340	P29	792.7	20.0	22.0							
MI	1978	06	99	21	425056	880404	P30	791.7	10.0	12.0							
MI	1981	06	3	21	425056	880410	P8-AR	792.0	8.5	10.0							
MI	1981	06	3	21	425056	880410	P8-AR	792.0	8.5	10.0							
MI	1978	06	99	21	425056	880404	P30	792.0	15.0	16.0							
MI	1979	06	99	21	425058	880348	P26C	881.8	88.5	90.0							
MI	1979	06	99	21	425058	880348	P26C	881.8	88.5	90.0							
MI	1979	06	99	21	425058	880348	P26C	881.8	88.5	90.0							
MI	1981	06	99	21	425058	880340	P29A	792.7	3.5	5.0							
MI	1981	06	99	21	425056	880340	P29B	792.7	8.5	10.0							
MI	1981	06	99	21	425056	880340	P29B	792.7	13.5	15.0							
MI	1981	06	3	21	425056	880405	P30R	791.1	3.5	5.0							
MI	1981	06	3	21	425056	880405	P30R	791.1	8.5	10.0							
MI	1981	06	3	21	425056	880405	P30R	791.1	13.5	15.0							
MI	1981	06	99	21	425056	880405	P30R	791.1	18.5	20.0							
MI	1981	06	99	21	425056	880405	P30R	791.1	23.5	25.0							
MI	1981	06	99	21	425056	880405	P30R	791.1	28.5	30.0							
MI	1981	06	99	21	425056	880405	P30R	791.1	33.5	35.0							
MI	1981	06	3	21	425037	880355	T445	810.7	38.5	40.0							
MI	1981	06	3	21	425037	880355	T445	810.7	43.5	45.0							
MI	1981	06	3	21	425037	880355	T445	810.7	48.5	50.0							
MI	1981	06	3	21	425037	880355	T445	810.7	53.5	55.0							
MI	1981	06	3	21	425037	880355	T445	810.7	58.5	60.0							
MI	1981	06	3														





Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR MILWAUKEE COUNTY - METRO SITE

[illegible]

## Appendix 3 - Hydrogeologic and Engineering Data for Milwaukee County - Metro Site

+ IDENTITY			+ LITHO- strat.			+ COUNTRY			+ HYDRAULIC + CONDUCTIVITY			+ GRONISIZE PERCENTAGES			+ ENGINEERING PROPERTIES			+ ENGINEERING PROPERTIES		
Year	Unit	Mat. Site	Lat.	Long.	Brgg. no.	Surf. Elev.	Sample top	Sample bottom	Lab K	Meth	Fld K	Matrix	Matrix	Matrix	Matrix	Matrix	Matrix	Matrix	Matrix	Matrix
(code)	(code)	(code)	(code)	(code)	(code)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)
M1 1981	00	3	21	425038	880329	1453	811.8	83.5	45.0											
M1 1981	00	3	21	425038	880329	1453	811.8	88.5	70.0											
M1 1981	00	3	21	425038	880329	1453	811.8	73.5	75.0											
M1 1981	00	3	21	425038	880329	1453	811.8	78.5	80.0											
M1 1981	00	3	21	425038	880329	1453	811.8	83.5	85.0											
M1 1981	00	3	21	425038	880329	1453	811.8	88.5	90.0											
M1 1981	00	3	21	425038	880329	1453	811.8	93.5	95.0											
M1 1981	00	3	21	425038	880329	1453	811.8	98.5	100.0											
M1 1981	00	3	21	425038	880329	1453	811.8	108.5	110.0											
M1 1981	00	3	21	425038	880329	1453	811.8	118.5	120.0											
M1 1981	00	3	21	425038	880329	1453	811.8	123.5	125.0											
M1 1981	00	3	21	425038	880329	1453	811.8	134.0	140.0											
M1 1981	00	3	21	425038	880329	1453	811.8	53.0	55.0											
M1 1981	00	3	21	425038	880329	1453	811.8	58.0	60.0											
M1 1983	00	3	21	425042	880357	P80	809.4	3.5	5.0											
M1 1983	00	3	21	425042	880357	P80	809.4	8.5	10.0											
M1 1983	00	3	21	425042	880357	P80	809.4	13.5	15.0											
M1 1983	00	3	21	425042	880357	P80	809.4	18.5	20.0											
M1 1983	00	3	21	425042	880357	P80	809.4	23.5	25.0											
M1 1983	00	3	21	425042	880357	P80	809.4	28.5	30.0											
M1 1983	00	3	21	425042	880357	P80	809.4	33.5	35.0											
M1 1983	00	3	21	425042	880357	P80	809.4	38.5	40.0											
M1 1983	00	99	21	425042	880357	P80	809.4	43.5												

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR MILWAUKEE COUNTY - RETRO SITE

+ IDENTITY	+ Litho- strat.	+ County unit	+ Mat. Site (code) Year (code) (code) No.	Lat.	Long.	Brg. no.	Surf. Elev. top (ft)	Sample bottom (ft)	+ CONDUCTIVITY + Lab K (cgs/s)	+ HYDRAULIC + Meth (cgs/s)	+ Matrix X + Bulk X (cgs/s)	+ Matrix X + silt (0.0025 to 0.002mm)	+ Matrix X + clay (0.002mm to <0.002mm)	+ ENGINEERING PROPERTIES + Unified + Soil + Bulk + Percent Unit Wt. + P200 (pcf)	+ Moist. + Liquid Plastic. UC + (H) cont. (H) flat + index (Hsf) +
MI 1983 OC	3	21	425047 880357	P81	804.7	63.5	65.0								
MI 1983 OC	3	21	425047 880357	P81	804.7	68.5	70.0								
MI 1983 OC	3	21	425047 880357	P81	804.7	73.5	75.0								
MI 1983 OC	3	21	425047 880357	P81	804.7	78.5	80.0								
MI 1983 OC	3	21	425047 880357	P81	804.7	83.5	85.0								
MI 1983 OC	3	21	425047 880357	P81	804.7	88.5	90.0								
MI 1983 OC	3	21	425047 880357	P81	804.7	93.5	95.0								
MI 1983 OC	3	21	425047 880357	P81	804.7	98.5	100.0								
MI 1983 OC	3	21	425047 880357	P81	804.7	89.0	100.0								
MI 1983 OC	3	21	425047 880357	P81	804.7	85.0	100.0								
MI 1983 OC	99	21	425047 880359	P82	807.2	3.5	5.0								
MI 1983 OC	99	21	425047 880359	P82	807.2	8.5	10.0								
MI 1983 OC	99	21	425047 880359	P82	807.2	13.5	15.0								
MI 1983 OC	99	21	425047 880359	P82	807.2	18.5	20.0								
MI 1983 OC	99	21	425047 880359	P82	807.2	23.5	25.0								
MI 1983 OC	99	21	425047 880359	P82	807.2	28.5	30.0								
MI 1983 OC	3	21	425047 880359	P82	807.2	33.5	35.0								
MI 1983 OC	3	21	425047 880359	P82	807.2	38.5	40.0								
MI 1983 OC	3	21	425047 880359	P82	807.2	43.5	45.0								
MI 1983 OC	3	21	425047 880359	P82	807.2	48.5	50.0								
MI 1983 OC	3	21	425047 880359	P82	807.2	53.5	55.0								
MI 1983 OC	3	21	425047 880359	P82	807.2	58.5	60.0								
MI 1983 OC	3	21	425047 880359	P82	807.2	63.5	65.0								
MI 1983 OC	3	21	425047 880359	P82	807.2	68.5	70.0								
MI 1983 OC	3	21	425047 880359	P82	807.2	73.5	75.0								
MI 1983 OC	3	21	425047 880359	P82	807.2	78.5	80.0								
MI 1983 OC	3	21	425047 880359	P82	807.2	83.5	85.0								
MI 1983 OC	3	21	425047 880359	P82	807.2	88.5	90.0								
MI 1983 OC	3	21	425047 880359	P82	807.2	93.5	95.0								
MI 1983 OC	3	21	425047 880359	P82	807.2	98.5	100.0								
MI 1983 OC	3	21	425047 880359	P82	807.2	93.0	100.0								
MI 1983 OC	99	21	425050 880352	T83	802.6	13.5	15.0								
MI 1983 OC	99	21	425050 880352	T83	802.6	18.5	20.0								
MI 1983 OC	99	21	425050 880352	T83	802.6	23.5	25.0								
MI 1983 OC	99	21	425108 880410	P81B	805.2	250.0									
MI 1983 OC	3	21	425199 880499	B85	783.5	3.5	5.0								
MI 1983 OC	3	21	425199 880499	B85	783.5	8.5	10.0								
MI 1983 OC	3	21	425199 880499	B85	783.5	13.5	15.0								
MI 1983 OC	3	21	425199 880499	B85	783.5	18.5	20.0								
MI 1983 OC	3	21	425199 880499	B85	783.5	23.5	25.0								
MI 1983 OC	3	21	425199 880499	B85	783.5	28.5	30.0								
MI 1983 OC	3	21	425199 880499	B85	783.5	33.5	35.0								
MI 1983 OC	3	21	425199 880499	B85	783.5	38.5	40.0								
MI 1983 OC	3	21	425199 880499	B85	783.5	43.5	45.0								



## Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR MILWAUKEE COUNTY - METRO SITE

[illegible]

**Appendix 3 - Hydrogeologic and Engineering Data for Deonto County, City of Oconto Falls Landfill**

+ IDENTITY		+ LITHO-		+ COUNTY		+ YEAR		+ SITE		+ LAT.		+ LONG.		+ BRQ. NO.		+ SURF. ELEV.		+ TOP		+ BOTTOM		+ LAB K		+ MATH		+ FLD K		+ BULK Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z		+ Matrix Z	
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Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR OCOTON COUNTY LANDFILL

+ IDENTITY				+ HYDRAULIC + CONDUCTIVITY							+ GRAINSIZE PERCENTAGES				+ ENGINEERING PROPERTIES												
+ Countv	unit	Mat.	Site		Surs.	Sample	Sample																				
(code)	Year	(code)	(code)	No.	Lat.	Long.	no.	(ft)	top	bottom	(ft)	Lab K	Meth	Fld K	Meth	Bulk %	Matrix %	Matrix %	Matrix %	Unified	Bulk	Dry	SPT	Moist.	Liquid	Plastic	UC
												(cm/s)	code	(cm/s)	code	+ 2.0mm	0.0625mm	0.002mm	( $<0.002mm$ )	+ Class.	P200	(pcf)	(N)	cont. (%)	(X) limit	index	(tsf)
OC	1983	KE	3	23c	445016	880614	B1	722.6	10.0	11.0						28				SC	36		66				
OC	1983	KE	99	23c	445014	880602	B2	714.5	15.0	16.0						0				SM	39		16				
OC	1983	KE	4	23c	445024	880606	B5	704.1	10.0	11.5						0				SP	6		28				
OC	1983	KE	3	23c	445021	880604	B6	715.6	4.5	6.0						29				SC	30		32				
OC	1983	KEK1	3	23c	445012	880611	B8	718.0	4.5	6.0						1				CL	65		15				
OC	1983	KEK1	3	23c	445012	880611	B8	718.0	5.5	6.0		6.00E-08	53							CL							
OC	1983	KE	99	23c	445024	880612	MW11	709.8	5.0	40.0						0				SP-SH	6						
OC	1983	KEK1	3	23c	445016	880619	B14		9.5	11.0						18				CL	73		65				
OC	1983	KEN1	3	23c	445012	880618	MW15	720.6	3.0	4.0		6.00E-06	53							SC							
OC	1983	KE	99	23c	445012	880618	MW15	720.6	35.0	41.0				1.31E-04	8					SP							
OC	1983	KEN1	3	23c	445016	880625	B18	719.0	0.5	2.0		2.00E-05	53							SC							
OC	1983	KEK1	3	23c	445016	880625	B18	719.0	4.5	6.0						1				CL	55		4				
OC	1983	KEK1	3	23c	445016	880625	B18	719.0	7.0	7.5		1.00E-07	53														
OC	1983	KE	5	23c	445016	880625	B18	719.0	14.5	16.0						6				CL	66		62				
OC	1983	KE	99	23c	445026	880627	MW21	710.9	5.0	40.0						0				SP	6						
OC	1984	KEK1	3	23b	444113	881019	B1		2.0	7.0						8	34	51	15	CL	66				31	14	
OC	1984	KE	3	23b	444114	881020	B4		16.0	24.0						4	25	49	26	CL	78				39	23	
OC	1984	KE	3	23b	444111	881024	B6		9.0	15.0						7	18	44	38	CL	78				33	19	
OC	1984	KEK1	3	23b	444110	881027	B8		3.0	14.0						2	20	45	35	CL	81				42	21	
BN	1984	KEK1	3	23a	443921	880902	B1		8.0	12.0						73	22	44	33	CL	73				44	27	
BN	1984	KEK1	3	23a	443921	880907	B2		3.0	9.0						78	33	45	26	CL	78				33	19	

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR OUTAGAMIE COUNTY, OUTAGAMIE COUNTY LANDFILL

[illegible]



IDENTITY	Litho- strat.	County unit	Mat. Site (code)	No.	Lat.	Long.	Brg. no.	Elev. top (ft)	Surf. top (ft)	HYDRAULIC		BRAINSTIE PERCENTAGES		ENGINEERING PROPERTIES		SPT Moist. (pcf)	Liquid Plastic. (pcf)	Index (pcf)	
										Conductivity (ft/s)	Lab K (ft/s)	Matrix Z (0.0025in)	Matrix X (0.0025in)	Unified Soil Class.	Brv Percent Unit Wt.				
00 1982	KE	3	24	441727	882029	8224	45.0	47.0	1.07E-08		27	55	41	4	SN-SC	92.1	14	32.4	
00 1982	UN	3	24	441727	882029	8224	48.5	50.0							CL	94	112	15	11
00 1982	KENI	3	24	441727	882020	8225	18.5	20.0							CL	94	12	48	17
00 1982	KENI	3	24	441727	882003	8226	18.5	20.0							CL	86	14	37	15
00 1982	KENI	3	24	441733	882030	82158	5.0	7.0							CL				
00 1982	KENI	3	24	441733	882030	82158	10.0	12.0							CL	107.0	14.7		
00 1982	KENI	3	24	441733	882030	82158	15.0	17.0							CL	113.5	16.4		
00 1982	KENI	3	24	441733	882030	82158	20.0	22.0							CL	103.2	19.4		
00 1982	UN	3	24	441733	882030	82158	48.5	50.0			11	45	45	10	ML	55	240	15	12
00 1982	UN	3	24	441729	882035	8219	48.5	50.0			44	54	54	14	SN-SC	28	240	16	11
00 1982	UN	3	24	441729	882025	8220	48.5	50.0			15	51	35	14	SN	50	180	19	12
00 1982	UN	3	24	441729	882015	8221	48.5	50.0			17	67	27	6	SN	31	49	13	12
00 1982	UN	3	24	441729	882006	8222	48.5	50.0			10	60	31	9	SN-SC	44	300	12	
00 1982	UN	3	24	441727	882038	8223	48.5	50.0			29	49	39	11	SN-SC	41	300	16	11
00 1981	KENI	3	24	441799	882199	8100	14.5	17.0							CL		20.5	29	13
00 1981	KE	313	24	441799	882199	8101	24.5	26.0	1.70E-08	5					CL		47.9	67	40
00 1981	KE	3513	24	441799	882199	8101	21.6	27.1							CL				
00 1981	KENI	3	24	441799	882199	8102	14.5	17.0	1.10E-08	5	7				CL		22.9	36	19
00 1981	KE	5	24	441799	882199	8103	19.5	21.5	1.50E-08	5					CL		21.0	32	17
00 1981	KE	5	24	441799	882199	8103	16.2	21.7	2.38E-06	7					CL		19.4	37	13
00 1981	KENI	3	24	441799	882199	8104	17.0	19.0	1.70E-08	5					CL		20.6	34	18
00 1981	KENI	3	24	441799	882199	8105	19.5	21.5	1.30E-08	5					CL		20.6	34	21
00 1981	KENI	3	24	441726	882047	8105	15.4	20.9	7.40E-06	7					CL		24.9	39	18
00 1981	KE	5	24	441726	882047	8105	713.9	0.5	4.0		9	42	49	49	CL		24.9	39	21
00 1981	KE	5	24	441726	882047	8105	713.9	6.5	4.0	2.70E-07	24				CL		24.9	39	21
00 1981	KENI	3	24	441724	882047	8106	713.1	0.7	3.6						CL		42.1	49	22
00 1981	KE	5	24	441724	882047	8106	713.1	4.7	3.6	2.90E-08	1				CL		42.1	49	22
00 1981	KE	5	24	441723	882047	8107	711.5	0.2	3.2						CL		24.0	47	25
00 1981	KE	5	24	441723	882047	8107	711.5	4.4	3.2	1.70E-07	1				CL		24.0	47	25
00 1981	KE	5	24	441723	882047	8107	711.5	4.4	3.2						CL		27.9	40	23
00 1981	KE	99	24	441725	882051	8108	719.3	5.0	9.2	4.30E-08	1	10	40	50	CL		17.0	33	18
00 1981	KE	513	24	441725	882051	8108	719.3	10.5	9.2						CL		17.0	33	18
00 1981	KENI	3	24	441724	882051	8109	718.1	4.0	7.0	1.90E-08	1	13	41	46	CL		31.5	56	32
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981	KE	99	24	441723	882051	8109	718.1	8.0	7.0						CL		20.0	32	16
00 1981																			

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR OUTASHEE COUNTY, OUTASHEE COUNTY LANDFILL

[illegible]

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR OUTAGAMIE COUNTY, OUTAGAMIE COUNTY LANDFILL

+ IDENTITY		+ HYDRAULIC				+ GRAIN SIZE PERCENTAGES				+ ENGINEERING PROPERTIES				+															
+ County	+ Litho- strat.	+ Mat. Site	+ Lat.	+ Long.	+ No.	+ Surf. Elev.	+ Top	+ Bottom	+ Sample	+ Conductivity	+ Lab K	+ Meth	+ Fld K	+ Meth	+ Bulk	+ Matrix %	+ Matrix %	+ Matrix %	+ Matrix %	+ Unified	+ Bulk	+ Dry	+ Soil	+ Percent Unit Wt.	+ 997 Moist.	+ Liquid Plastic.	+ UC	+	
+ (code)	+ Year	+ (code)	+ (code)	+ (code)	+ No.	+ (ft)	+ (ft)	+ (ft)	+ (ft)	+ (cm/s)	+ (cm/s)	+ code	+ (cm/s)	+ code	+ (pcf)	+ P200	+ (pcf)	+ (pcf)	+ (pcf)	+ Class.	+ P200	+ (pcf)	+ (pcf)	+ (pcf)	+ (pcf)	+ (pcf)	+ (pcf)	+ (pcf)	+
OU 1974	KENI	3	24	441799	882199	B8	736.6	6.0	8.0						0	56	.28	16	CL-ML	45	109.0		23.0			3.5			
OU 1974	KENI	3	24	441733	882046	B11	737.3	25.0	27.0										CL				25.0			1.0			
OU 1974	KENI	3	24	441733	882046	B11	737.3	30.0	31.0										CL				25.0			1.0			
OU 1974	KENI	3	24	441733	882046	B11	737.3	30.0	32.0		7.48E-07								CL										
OU 1974	KE	5	24	441733	882046	B11	737.3	40.0	42.0						0	27	11	62	CL-CH	73									
OU 1974	KE	5	24	441733	882046	B11	737.3	40.0	42.0						0	64	32	4	CL	36									
OU 1975	KE	5	24	441728	882050	B3A	30.0	31.0											CL-CH		97.5		32.0			2.3			
OU 1975	KE	5	24	441728	882050	B3A	30.0	32.0			5.38E-08								CL-CH										
OU 1975	KE	5	24	441728	882042	B4A	33.0	34.0			4.53E-09								CL				110.0		4.0				
OU 1975	KENI	3	24	441738	882050	B9A	20.0	21.0											CL				111.0		1.0				
OU 1975	KENI	3	24	441738	882050	B9A	20.0	22.0			1.68E-08								CL										
OU 1979	KENI	3	24	441721	882107	B13A	737.9	25.0	27.0		1.53E-07	3			3	19	45	36	CL	79					2.3				
OU 1979	KE	5	24	441726	882107	B15A	736.6	40.0	42.0						0	11	45	44	CL-CH	89			40.0						
OU 1979	KE	5	24	441717	882047	B18B	733.8	35.0	37.0		3.87E-08	3							CL-CH										

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR OZARK COUNTY, INCLUDING ANDERSON, DIDIER, AND NEPCO PROPOSED SITES

+ IDENTITY	+ County	+ Litho- strat.	+ Unit	+ Lat.	+ Long.	+ Brng.	+ Elev.	+ Sample	+ Hydraulic + Conductivity	+ Grain Size Percentages	+ Engineering Properties	+ Bulk Percent Unit Wt. SPt Moist. Liquid Plastic, UC (M cont. (t) limit index (tsf) +	
01 1981	DC	3	25	432151	875427	M01	155.6	31.0	41.0	6.90E-05	7	ML-CL	89
01 1981	DC	3	25	432151	875427	M01	155.6	15.0	17.0	1.70E-05	7	ML-CL	89
01 1981	DC	3	25	432141	875429	M02	31.5	41.5	1.70E-05	7	10	ML-CL	58
01 1981	DC	3	25	432141	875429	M02	15.0	17.0	1.70E-05	7	33	CL	66
01 1982	KE02	3	26	432539	875121	M01	724.4	5.5	15.5	5.20E-06	7	CL	88
01 1982	KE02	3	26	432539	875121	M01	724.4	15.0	17.0	5.20E-06	7	CL	72
01 1982	KE02	3	26	432600	875104	M04	718.3	5.3	15.3	1.90E-07	7	CL	62
01 1982	KE02	3	26	432600	875104	M04	718.3	5.0	7.0	1.90E-07	7	CL	15.8
01 1983	KE02	3	27	432646	875143	M01	737.3	10.6	20.6	1.10E-07	7	CL	114.4
01 1983	KE02	3	27	432646	875143	M01	737.3	5.0	7.0	1.10E-07	7	CL	70
01 1983	KE02	3	27	432647	875155	M02	736.5	10.4	20.4	1.50E-07	7	CL	116.1
01 1983	KE02	3	27	432627	875155	M02	736.5	20.0	22.0	1.50E-07	7	CL	18.0
01 1983	KE02	3	27	432654	875152	M03	734.1	10.1	20.1	6.30E-07	7	CL	19.9
01 1983	KE02	3	27	432654	875152	M03	734.1	25.0	27.0	6.30E-07	7	CL	14.0
01 1983	KE02	3	27	432702	875147	B19	734.0	7.5	27.0	2.50E-08	7	CL	111.3
01 1983	KE02	3	27	432702	875147	B19	734.0	31.0	31.0	2.50E-08	7	CL	68
01 1983	KE02	3	27	432654	875147	B20	734.6	3.0	3.0	2.50E-08	7	CL	87
01 1983	KE02	3	27	432654	875147	B20	734.6	8.0	8.0	2.50E-08	7	CL	86
01 1983	KE02	3	27	432654	875147	B20	734.6	26.0	26.0	2.50E-08	7	CL	80
01 1983	KE02	3	27	432654	875147	B20	734.6	37.0	37.0	2.50E-08	7	CL	83
01 1983	KE02	3	27	432648	875153	B23	738.1	3.5	3.5	2.50E-08	7	CL	82
01 1983	KE02	3	27	432648	875153	B23	738.1	8.5	8.5	2.50E-08	7	CL	88
01 1983	KE02	3	27	432648	875153	B23	738.1	14.0	14.0	2.50E-08	7	CL	98
01 1983	KE02	3	27	432648	875153	B23	738.1	18.5	18.5	2.50E-08	7	CL	77
01 1983	KE02	3	27	432648	875153	B23	738.1	28.5	28.5	2.50E-08	7	CL	62
01 1983	KE02	3	27	432648	875153	B23	738.1	38.5	38.5	2.50E-08	7	CL	42
01 1983	KE02	3	27	432648	875153	B24	732.8	1.5	1.5	2.50E-08	7	CL	86
01 1983	KE02	3	27	432649	875138	B24	732.8	7.0	7.0	2.50E-08	7	CL	86
01 1983	KE02	3	27	432649	875138	B24	732.8	27.0	27.0	2.50E-08	7	CL	89
01 1983	KE02	3	27	432649	875138	B24	732.8	47.5	47.5	2.50E-08	7	CL	74
01 1983	KE02	3	27	432649	875138	B24	732.8	68.0	68.0	2.50E-08	7	CL	72
01 1983	KE02	3	27	432637	875156	B25	734.1	8.5	8.5	2.50E-08	7	CL	81
01 1983	KE02	3	27	432637	875156	B25	734.1	18.7	18.7	2.50E-08	7	CL	81

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR RACINE COUNTY - LAND RECLAMATION SITE

[illegible]

+ IDENTITY				Litho- strat. unit	Mat. No.	Site	Lat.	Long.	Brng. no.	Elev. (ft)	Surf. Elev. (ft)	Sample top (ft)	Sample bottom (ft)	+ HYDRAULIC		+ CONDUCTIVITY		+ GRAIN SIZE PERCENTAGES		+ ENGINEERING PROPERTIES		+ Unified Soil Class.	+ Bulk P200 (pcf)	+ Drv Unit W. Moist. (pcf)	+ Liquid Plastic. (pcf)	+ UC index (pcf)																																																																																																																																																																																																																																																																																																																																																																																																								
+ County (code)	+ Year (code)	+ (code)	+ Lab K (ft)											+ Meth (ft)	+ Fld K Meth (ft)	+ Bult I (ft)	+ Matrix I (ft)	+ sand (ft)	+ silt (ft)	+ clay (ft)	+ Matrix I (ft)						+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I 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Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I (ft)	+ Matrix I 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[illegible]

## Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR RACINE COUNTY - LAND RECLAMATION SITE

[illegible]



Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR BACINE COUNTY - LAND RECLAMATION SITE

+ IDENTITY			+ HYDRAULIC			+ GRAINSIZE PERCENTAGES			+ ENGINEERING PROPERTIES					
+ Litho- strat.	+ Conty unit	+ Mat. Site (code)(code) No.	Lat.	Long.	Borg. Elev. no. (ft)	Surt. Elev. top (ft)	Sample bottom (ft)	Lab K Meth (ft)	F10 K Meth (ft)	Matrix I sand silt clay	Matrix I sand silt clay	Unified Soil Class.	Dry Bulk Percent Unit Wt. p200 (pcf)	SPF Moist. Liquid Plastic. UC (%) cont. (t) limit index (tsf) +
RA 1985	OC	99	28	424240	875145	847	679.8	70.0				ML	67	
RA 1985	OC	3	28	424240	875138	853	695.5	2.5				CL	9	1.7
RA 1985	OC	3	28	424240	875138	853	695.5	5.0				CL	16	4.0
RA 1985	OC	3	28	424240	875138	853	695.5	10.0				CL	24	2.8
RA 1985	OC	99	28	424240	875138	853	695.5	15.0				CL	13	2.2
RA 1985	OC	3	28	424240	875138	853	695.5	20.0			23	CL	69	3.0
RA 1985	OC	3	28	424240	875138	853	695.5	25.0				CL	20	3.5
RA 1985	OC	3	28	424240	875138	853	695.5	30.0				CL	27	4.0
RA 1985	OC	3	28	424240	875138	853	695.5	35.0				CL	17	3.0
RA 1985	OC	99	28	424240	875138	853	695.5	40.0			56	CL	98	2.5
RA 1985	OC	99	28	424240	875138	853	695.5	45.0				CL	17	1.5
RA 1985	OC	3	28	424240	875138	853	695.5	50.0				CL	20	2.5
RA 1985	OC	3	28	424240	875138	853	695.5	55.0				CL	70	4.5
RA 1985	OC	3	28	424240	875138	853	695.5	60.0				CL	18	
RA 1985	OC	3	28	424240	875138	853	695.5	65.0			25	CL	23	3.5
RA 1985	OC	99	28	424240	875138	853	695.5	70.0				CL	28	
RA 1985	OC	99	28	424240	875138	853	695.5	75.0				ML, CL-ML	31	
RA 1985	OC	99	28	424240	875138	853	695.5	80.0				ML, CL-ML	133	4.5
RA 1985	OC	99	28	424237	875151	856	673.3	2.5				ML	73	4.5
RA 1985	OC	99	28	424237	875151	856	673.3	5.0				CL	31	
RA 1985	OC	99	28	424237	875151	856	673.3	10.0				SM-SM	4	
RA 1985	OC	99	28	424237	875151	856	673.3	15.0				SP-SM	17	
RA 1985	OC	99	28	424237	875151	856	673.3	20.0				CL	19	1.5
RA 1985	OC	3	28	424237	875151	856	673.3	25.0				CL	20	0.8
RA 1985	OC	3	28	424237	875151	856	673.3	30.0			52	CL	11	3.0
RA 1985	OC	99	28	424237	875151	856	673.3	35.0				CL	15	
RA 1985	OC	99	28	424237	875151	856	673.3	40.0				SM	21	
RA 1985	OC	3	28	424237	875151	856	673.3	45.0				CL	66	4.5
RA 1985	OC	3	28	424237	875151	856	673.3	50.0				CL	29	2.6
RA 1985	OC	3	28	424237	875151	856	673.3	55.0				CL	63	4.5
RA 1985	OC	99	28	424237	875151	856	673.3	60.0				SP-SM	109	
RA 1985	OC	99	28	424237	875151	856	673.3	65.0				SP-SM	100	
RA 1985	OC	99	28	424237	875151	856	673.3	70.0				SP-SM	150	
RA 1985	OC	3	28	424235	875148	859	675.0	2.5				CL	76	4.5
RA 1985	OC	3	28	424235	875148	859	675.0	5.0				CL-ML/CL	6	1.0
RA 1985	OC	3	28	424235	875148	859	675.0	10.0				CL-ML/CL	10	1.5
RA 1985	OC	99	28	424235	875148	859	675.0	15.0				CL	12	2.2
RA 1985	OC	99	28	424235	875148	859	675.0	20.0				ML	9	9
RA 1985	OC	3	28	424235	875148	859	675.0	25.0				ML	16	18
RA 1985	OC	3	28	424235	875148	859	675.0	30.0				CL	14	2.2
RA 1985	OC	99	28	424235	875148	859	675.0	35.0				CL	12	2.2
RA 1985	OC	99	28	424235	875148	859	675.0	40.0				ML	12	3.0
RA 1985	OC	99	28	424235	875148	859	675.0	45.0				ML	79	
RA 1985	OC	99	28	424235	875148	859	675.0	50.0				ML	71	
RA 1985	OC	3	28	424235	875148	859	675.0	50.0				CL	18	3.5



## Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR RACINE COUNTY - LAND RECLAMATION SITE

+ IDENTITY			+ HYDRAULIC + CONDUCTIVITY						+ GRAIN SIZE PERCENTAGES				+ ENGINEERING PROPERTIES						
+ Country + (code)	+ Year + (code)	Litho- strat. unit No.	Site (code)	Lat.	Long.	Borg. no.	Surf. Elev. (ft)	Samp. Sessie top (ft)	Meth (ft)	Fld K Meth (ca/s)	Matrix I sand (0.0625 to 0.002mm)	Matrix II silt (0.0625 to 0.002mm)	Matrix III clay (0.002mm)	Dry Bulk Percent Unit Wt. P200 (pcf)	Unifd Soil Class.	Moist. Liquid Plastic. Shrinkage Limit Index (tsf) +			
RA 1985	OC	99	28	424233	875137	867	698.3	25.0							CL	30	3.5		
RA 1985	OC	99	28	424233	875137	867	698.3	30.0							CL-ML	12			
RA 1985	OC	99	28	424233	875137	867	698.3	35.0							CL-ML	84			
RA 1985	OC	99	28	424233	875137	867	698.3	40.0							CL	38			
RA 1985	OC	99	28	424233	875137	867	698.3	45.0							CL	15	3.5		
RA 1985	OC	99	28	424233	875137	867	698.3	50.0							CL	14	2.8		
RA 1985	OC	99	28	424233	875137	867	698.3	55.0							SP-SG	35	3.2		
RA 1985	OC	99	28	424233	875137	867	698.3	60.0							CL	47	4.5		
RA 1985	OC	99	28	424233	875137	867	698.3	65.0							CL	37	3.0		
RA 1985	OC	99	28	424233	875137	867	698.3	70.0							CL	38	2.8		
RA 1985	OC	99	28	424233	875137	867	698.3	75.0							ML	20			
RA 1985	OC	99	28	424233	875137	867	698.3	80.0							ML	83			
RA 1985	OC	99	28	424233	875137	867	698.3	85.0							CL	18	4.0		
RA 1985	OC	99	28	424233	875137	867	698.3	90.0							CL	38			
RA 1985	OC	99	28	424233	875137	867	698.3	95.0							ML	110			
RA 1985	OC	99	28	424233	875137	868	706.7	2.5							CL	12	2.0		
RA 1985	OC	99	28	424233	875137	868	706.7	5.0							CL	39	4.5		
RA 1985	OC	99	28	424233	875137	868	706.7	10.0							CL	59	4.5		
RA 1985	OC	99	28	424233	875137	868	706.7	15.0							CL	29	2.5		
RA 1985	OC	99	28	424233	875137	868	706.7	20.0							CL	30	1.8		
RA 1985	OC	99	28	424233	875137	868	706.7	25.0							CL	19	1.8		
RA 1985	OC	99	28	424233	875137	868	706.7	30.0							CL	22			
RA 1985	OC	99	28	424233	875137	868	706.7	35.0							CL-ML	38			
RA 1985	OC	99	28	424233	875137	868	706.7	39.0							SH	30	1.5		
RA 1985	OC	99	28	424233	875137	868	706.7	45.0							CL	15	1.5		
RA 1985	OC	99	28	424233	875137	868	706.7	50.0							CL	24	1.5		
RA 1985	OC	99	28	424233	875137	868	706.7	55.0							CL	27	2.1		
RA 1985	OC	99	28	424233	875137	868	706.7	60.0							CL	26	0.6		
RA 1985	OC	99	28	424233	875137	868	706.7	65.0							CL	34	2.		

## Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR RACINE COUNTY - LAND RECLAMATION SITE

+ IDENTITY		+ HYDRAULIC		+ GRAIN SIZE PERCENTAGES			+ ENGINEERING PROPERTIES									
County	Litho- strat.	Surf. Sample	+ CONDUCTIVITY	Matrix I	Matrix I	Matrix I	Unified	Soil	Percent Unit Wt.	SPT	Moist. Liquid Plastic. UC					
+ (code)	unit	Brng. Elev. top	Lab K	Field K	Matrix I	Matrix I	clay	silt	clay	Moist. Liquid Plastic. UC	index (tsf) +					
Year	Mat. Site	no. (ft)	(ft)	(ft)	code	code	(0.0025 to	(0.0025 to	(0.0025 to	(N) cont. (X) limit	index (tsf) +					
RA 1985	OC	99	28	424233	875130	869	709.2	70.0	2	21	72	6	ML	E2	46	2.5
RA 1985	OC	99	28	424233	875130	869	709.2	75.0					CL		42	2.5
RA 1985	OC	3	28	424233	875130	869	709.2	80.0					CL-ML		19	2.5
RA 1985	OC	3	28	424233	875130	869	709.2	85.0					CL		22	2.5
RA 1985	OC	3	28	424233	875130	869	709.2	90.0					CL		48	2.5
RA 1985	OC	99	28	424233	875130	869	709.2	95.0					CL		27	2.5

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR SAUK COUNTY, BAAP SITE

[illegible]





## Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR SAKU COUNTY, BAAP SITE

+ IDENTITY				+ HYDRAULIC				+ GRAINSIZE PERCENTAGES				+ ENGINEERING PROPERTIES											
				+ CONDUCTIVITY																			
+ Country	Litho- strat.	unit	Mat. Site	Lat.	Long.	Surf. Elev. no. (ft)	Sample top (ft)	Sample bottom (ft)	Lab K (cm/s)	Meth code	Fld K Meth (cm/s)	Bulk K (2.0 to 0.002mm)	Matrix K sand (0.0625 to 0.002mm)	Matrix K silt (0.002mm to 0.00075mm)	Matrix K clay (0.00075mm to 0.0002mm)	Unified Soil Class.	Bulk Percent P200	Drv Unit Wt. (pcf)	SPT (IN)	Moist. cont. (%)	Liquid Plastic limit (%)	UC index	
+ (code)	Year	(code)	(code) No.																				
SK	1982	HO	4	29	432056	894454	PBB04	881.0	1.0	2.5		8	68			SC	34		19				
SK	1982	HO	4	29	432056	894454	PBB04	881.0	6.0	7.5		48	87			SP-SH	8		66				
SK	1982	HO	4	29	432056	894454	PBB04	881.0	13.5	15.0		57	88			SP-SH	6		86				
SK	1982	HO	4	29	432056	894454	PBB04	881.0	23.5	25.0	1.39E-04	3				SP		115.2	140				
SK	1982	HO	4	29	432056	894454	PBB04	881.0	28.5	30.0		28	94			SP	4		101				
SK	1982	HO	4	29	432056	894454	PBB04	881.0	48.5	50.0	8.28E-04	3	1	99		SP	4	107.3	111				
SK	1982	HO	4	29	432048	894457	PBB05	872.9	6.0	7.5	1.86E-06	3	8	92		SH	12	132.7	7				
SK	1982	HO	4	29	432048	894457	PBB05	872.9	8.5	10.0	8.64E-05	3				SP-SH		116.3	33				
SK	1982	HO	4	29	432048	894457	PBB05	872.9	13.5	15.0		55	87			SP-SH	7		105				
SK	1982	HO	4	29	432048	894457	PBB05	872.9	23.5	25.0	2.56E-04	3				SP		114.5	67				
SK	1982	HO	4	29	432048	894457	PBB05	872.9	28.5	30.0		9	98			SP	3		100				
SK	1982	HO	4	29	432048	894457	PBB05	872.9	48.5	50.0	1.86E-06	3	0	100		SP-SH	7	132.7	83				
SK	1982	HO	4	29	432104	894502	PBB06	866.8	8.5	10.0		51	84			SP-SH	10		58				
SK	1982	HO	4	29	432104	894502	PBB06	866.8	13.5	15.0	4.85E-04	3	32	93		SH-SH	7	119.6	49				
SK	1982	HO	4	29	432104	894502	PBB06	866.8	18.5	20.0	4.11E-05	3				SP		124.4	44				
SK	1982	HO	4	29	432104	894502	PBB06	866.8	23.5	25.0	5.06E-05	3	8	97		SP	3	111.7	92				
SK	1982	HO	4	29	432104	894502	PBB06	866.8	28.5	30.0		4	99			SP	3		37				
SK	1982	HO	4	29	432104	894502	PBB06	866.8	48.5	50.0	8.23E-05	3				SP		110.1	88				
SK	1982	HO	4	29	432199	894599	PBB07	865.4	6.0	7.5	8.83E-04	3				SP-SH		119.3	33				
SK	1982	HO	4	29	432199	894599	PBB07	865.4	13.5	15.0		3	97			SP	5		44				
SK	1982	HO	4	29	432199	894599	PBB07	865.4	18.5	20.0		40	87			SP-SH	10		56				
SK	1982	HO	4	29	432199	894599	PBB07	865.4	23.5	25.0	3.10E-06	3	18	94		SP-SH	6	114.1	96				
SK	1982	HO	4	29	432199	894599	PBB07	865.4	28.5	30.0	2.44E-06	3	10	94		SP-SH	6	110.1	83				
SK	1982	HO	4	29	432199	894599	PBB07	865.4	48.5	50.0	1.40E-03	3	1	98		SP	4	106.7	98				
SK	1982	HO	99	29	432041	894459	PBB08	871.9	1.0	2.5		25	67			SH	28		41				
SK	1982	HO	4	29	432041	894459	PBB08	871.9	6.0	7.5	1.74E-04	3				SP-SH		123.9	14				
SK	1982	HO	4	29	432041	894459	PBB08	871.9	13.5	15.0		8	99			SP-SH	6		20				
SK	1982	HO	4	29	432041	894459	PBB08	871.9	18.5	20.0	1.41E-04	3	27	96		SP	5	122.3	34				
SK	1982	HO	4	29	432041	894459	PBB08	871.9	23.5	25.0	9.08E-04	3	16	99		SP	4	106.5	63				
SK	1982	HO	4	29	432041	894459	PBB08	871.9	28.5	30.0	3.02E-05	3	45	96		SP	3	119.8	60				
SK	1982	HO	4	29	432041	894459	PBB08	871.9	48.5	50.0		26	80			SH	19		65				
SK	1982	HO	7	29	432113	894505	PBM01	855.7	3.5	5.0	1.97E-05	3	0	89		SH	18	121.4	7				
SK	1982	HO	4	29	432113	894505	PBM01	855.7	8.5	10.0		24	92			SP-SH	7		19				
SK	1982	HO	4	29	432113	894505	PBM01	855.7	13.5	15.0	1.62E-03	3				SH		106.3	15				
SK	1982	HO	4	29	432113	894505	PBM01	855.7	18.5	20.0		32	97			SP	3		20				
SK	1982	HO	4	29	432113	894505	PBM01	855.7	23.5	25.0	6.59E-04	3				SH		100.8	20				
SK	1982	HO	4	29	432113	894505	PBM01	855.7	28.5	30.0		24	99			SP	5		19				
SK	1982	HO	4	29	432113	894505	PBM01	855.7	53.5	55.0	4.46E-05	3				SP-SH		125.5	129				
SK	1982	HO	4	29	432113	894505	PBM01	855.7	78.5	80.0	6.05E-03	3	17	98		SP	2	112.4	122				
SK	1982	HO	4	29	432113	894505	PBM01	855.7	98.5	100.0	7.52E-03	3	0	100		SP	2	105.8	16				
SK	1982	HO	6	29	432053	894557	PBM02	870.9	3.0	5.0	4.30E-07	3				CH		93.4			52	27	
SK	1982	HO	99	29	432053	894557	PBM02	870.9	6.0	7.5	7.23E-07	3				SC		123.8	11				
SK	1982	HO	4	29	432053	894557	PBM02	870.9	8.5	10.0	1.70E-03	3				SH		116.7	49				
SK	1982	HO	4	29	432053	894557	PBM02	870.9	23.5	25.0	1.66E-05	3				SH		111.5	37				
SK	1982	HO	4	29	432053	894557	PBM02	870.9	28.5	30.0		18	95			SP-SH	6		44				
SK	1982	HO	4	29	432053	894557	PBM02	870.9	53.5	55.0	1.28E-03	3	2	98		SP	3	107.6	106				



+ IDENTITY	+ litho- strat.	+ County unit	+ (code) Year	+ Mat. Site (code)	+ No.	+ Lat.	+ Long.	+ Brn. no.	+ Elev. no. (ft)	+ Surt.	+ Bottom (ft)	+ Top (ft)	+ HYDRAULIC + CONDUCTIVITY		+ GRAINISTE PERCENTAGES		+ ENGINEERING PROPERTIES		+ Bulk Dry Percent P200	+ Soil Class.	+ Unif. (pcf)	+ SPT Blot. Unit Blot.	+ Liquid Plastic Index (Hst)	+ (Hst)
													Lab K (cal/s)	Math (cal/s)	Matrix I sand (2.0 to 0.0625 to 0.002mm)	Matrix I clay (0.0625 to 0.002mm)	Matrix I silt (0.0625 to 0.002mm)	Matrix I clay (0.0625 to 0.002mm)						
SK 1982	H0	4	29	432053	894557	PM002	870.9	78.5	80.0		4.42E-04	3	29	94		SP	5	128.9	120					
SK 1982	H0	4	29	432053	894557	PM002	870.9	113.5	115.0		1.24E-07	3	15	99		SP	3	109.1	173					
SK 1982	H0	4	29	432053	894557	PM002	870.9	18.5	10.0							SP	3							
SK 1982	H0	99	29	432107	894403	PM003	862.7	3.5	5.0							SC	24							
SK 1982	H0	4	29	432107	894403	PM003	862.7	6.0	7.5							SP-SH	10							
SK 1982	H0	4	29	432107	894403	PM003	862.7	18.5	20.0							SP	3							
SK 1982	H0	4	29	432107	894403	PM003	862.7	23.5	25.0							SP	5							
SK 1982	H0	4	29	432107	894403	PM003	862.7	29.5	30.0							SP	5							
SK 1982	H0	4	29	432107	894403	PM003	862.7	53.5	55.0							SP	5							
SK 1982	H0	4	29	432107	894403	PM003	862.7	78.5	80.0							SP	5							
SK 1982	H0	4	29	432107	894403	PM003	862.7	106.5	107.0							SP	5							
SK 1982	H0	99	29	432199	894499	PM004	859.0	6.0	7.5							SP	2							
SK 1982	H0	99	29	432199	894499	PM004	859.0	13.5	15.0							SP	2							
SK 1982	H0	4	29	432199	894499	PM004	859.0	18.5	20.0							SP	2							
SK 1982	H0	4	29	432199	894499	PM004	859.0	23.5	25.0							SP	2							
SK 1982	H0	4	29	432199	894499	PM004	859.0	53.5	55.0							SP	2							
SK 1982	H0	4	29	432199	894499	PM004	859.0	78.5	80.0							SP	2							
SK 1982	H0	99	29	432045	894458	PM005	873.7	3.5	5.0							SC	14							
SK 1982	H0	99	29	432045	894458	PM005	873.7	8.5	10.0							SC	14							
SK 1982	H0	99	29	432045	894458	PM005	873.7	13.5	15.0							SC	14							
SK 1982	H0	99	29	432045	894458	PM005	873.7	18.5	20.0							SC	14							
SK 1982	H0	4	29	432045	894458	PM005	873.7	23.5	25.0							SC	14							
SK 1982	H0	4	29	432045	894458	PM005	873.7	28.5	30.0							SC	14					</		

+ IDENTITY	+ Litho- strat.	+ Conty unit	+ Nat. Site (code/locode) No.	+ Lat.	+ Long. no. (ft)	+ Brn. Elev. top (ft)	+ Surf. Elev. bottom (ft)	+ Sample Sapre + Botto + Top (ft)	+ HYDRAULIC + CONDUCTIVITY	+ GRAIN SIZE PERCENTAGES			+ ENGINEERING PROPERTIES						
										Matrix %	Matrix %	Matrix %	Unified clay	Silt (2.0 to 0.0625 to 0.0025mm)	Bulk % (2.0 to 0.0625 to 0.0025mm)	Fld K Meth (cgs)	Lab K code	Perct Unit Wt. (pcf)	Moist. Liquid Plastic. Shrinkage (%) (cgs) (pcf) (mm) (cgs) (mm)
SK 1982	H0	99	29	432041	894459	P8004	875.0	18.5	20.0	3.14E-04	3					SH	115.4	44	
SK 1982	H0	99	29	432041	894459	P8004A	875.0	23.5	25.0			17	77			SH	23	60	
SK 1982	H0	3	29	432043	894458	P8005A	875.8	13.5	15.0	2.15E-06	3					SH	19	128.1	
SK 1982	H0	4	29	432043	894458	P8005B	875.8	23.5	25.0			16	89			SP-SH	9	33	
SK 1982	H0	4	29	432043	894458	P8005C	875.8	28.5	30.0	1.15E-03	3					SP-SH	114.2	37	

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## Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR SHAWANG COUNTY LANDFILL

+ IDENTITY		+ HYDRAULIC				+ STRAINRATE PERCENTAGES			+ ENGINEERING PROPERTIES										
:	Litho-	+ CONDUCTIVITY				:	Matrix %	Matrix %	Matrix %	:									
+	strat.	Surf.	Sasite	+		:	silt	clay	+	Unified	Bulk	Dry							
+	unit	Brg. Elev.	top	+		:	cl. to	+	+	+	Percent	Unit Mt.							
+	County	no.	bottom	+		:	(2.0 to	+	+	+	Class.	P200	(pcf)						
+	Site	Long.	(ft)	+		:	0.0625 to	+	+	+									
+	(code)	Lat.	(ft)	+		:	0.0025ast	+	+	+									
+	Year		(ft)	+		:	(0.0025ast	+	+	+									
+	(code)		(ft)	+		:	(0.0025ast	+	+	+									
+			(ft)	+		:	(0.0025ast	+	+	+									
SH 1985	KEVI	3	30	444899	883399	N13	834.9	2.5	4.5	5	34	53	14	CL	63	15.0	24.0	8.0	2.3
SH 1985	KEVI	3	30	444899	883699	N14	833.2	1.5	10.0		37	51	12	CL	64		25.0	13.0	
SH 1985	KEVI	3	30	444899	883699	N14	833.2	5.0	6.5	3	36	44	20	CL	63	16.0	23.0	8.0	3.5

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## Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR WALWORTH COUNTY, EAST TROY SITE

+ IDENTITY	Litho- strat.	+ Conty unit	+ Mat. Site (code)	+ Year (code)	+ Lat.	+ Long. no. (ft)	+ Brng. Elev. top (ft)	+ Surf. Elev. bottom (ft)	+ Sample Size top (ft)	+ Sample Size bottom (ft)	+ HYDRAULIC + CONDUCTIVITY	+ SOILS PERCENTAGES			+ ENGINEERING PROPERTIES						
												+	+	+	Matrix Z sand	Matrix Z silt	Matrix Z clay	Matrix Z clay	Unified Soil	Bulk Percent	Dry Unit Wt.
												Fld K (cm/s)	Meth code	Fld K (cm/s)	Meth code	Fld K (cm/s)	Meth code	Class. (0.002mm)	P200 (pcf)	(N) cont.(%)	Limit index (tsf)
UN	3	32	424549	882441	B6	943.0															8
UN	4	32	424558	882440	B7	927.6	28.5	30.0													
UN	99	32	424557	882455	B8	1065.0															
UN	4	32	424610	882449	B9	908.0															
UN	99	32	424699	882599	TP1																
UN	99	32	424699	882599	TP1																
UN	5	32	424699	882599	TP10																
UN	5	32	424699	882599	TP10																
UN	3	32	424699	882599	TP11																
UN	3	32	424699	882599	TP11																
UN	3	32	424699	882599	TP15																
UN	3	32	424699	882599	TP16																
UN	3	32	424699	882599	TP16																
UN	4	32	424699	882599	TP7																
UN	3	32	424699	882599	TP9																



[illegible]



[illegible]

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR WASHINGTON AND WAUKESHA COUNTIES. INCLUDES DATA FOR ONEIDA HILLS NORTH AND SOUTH AND PRECEDING LANDFILLS.

+ IDENTITY	+ Litho- strat.	+ County unit	+ Mat. Site (code) No.	+ Lat.	+ Long.	+ Brq. Elev. no. (ft)	+ Surf. Elev. top (ft)	+ Sample Depth bottom (ft)	+ Conductivity Lab K Meth (cc/s) code	+ Hydralic Fid K Meth (cc/s) code	+ Matrix 1 sand (0.0625 to 0.0025mm)	+ Matrix 2 silt (0.0025 to 0.00075mm)	+ Matrix 3 clay (0.00075 to 0.00025mm)	+ ENGINEERING PROPERTIES			
														+ Unified Soil Class.	+ Bulk P200 (pcf)	+ Percent Unit Wt. SPF Moist.	+ Liquid Plastic. UC (N) cont. (I) limit index (test) +
Wauk 1983	OC	3	35	431138	880446	B1	812.5	3.5	5.0					CL	20	16.0	4.5
Wauk 1983	OC	3	35	431138	880446	B1	812.5	8.5	10.0					CL	21	17.0	29
Wauk 1983	OC	99	35	431138	880446	B1	812.5	28.5	30.0					SN-ME-CL	20	21.0	32
Wauk 1983	OC	3	35	431138	880441	B7	819.5	3.5	5.0					CL	18	16.0	4.0
Wauk 1983	OC	3	35	431138	880441	B7	819.5	8.5	10.0					CL			
Wauk 1983	OC	3	35	431138	880441	B7	819.5	13.5	15.0					CL	33	14.0	23
Wauk 1983	OC	3	35	431138	880441	B7	819.5	38.5	40.0					CL	16	20.0	28
Wauk 1983	OC	3	35	431133	880441	L1		3.5	5.0					CL	12	16.0	24
Wauk 1983	OC	3	35	431133	880448	L2		8.5	10.0					CL	14	17.0	29
Wauk 1983	OC	3	35	431133	880448	L2		8.5	10.0					CL	14	20.0	33
Wauk 1983	OC	3	35	431134	880448	L3		3.5	5.0					CL	14	18.0	32
Wauk 1983	OC	3	35	431134	880448	L3		8.5	10.0					CL	13	21.0	34
Wauk 1983	UN	12	35	431144	880435	N22A	619.2	45.0	51.5	8.4E-04	7			DOLOMITE			4.0
Wauk 1983	UN	12	35	431144	880435	N22B	819.4	48.0	75.2	1.61E-04	7			DOLOMITE			4.5
Wauk 1983	UN	12	35	431152	880418	N50A	803.1	46.0	52.0	3.64E-05	7			DOLOMITE			3.0
Wauk 1983	UN	12	35	431144	880435	N22C	818.2	92.0	98.9	1.18E-05	7			DOLOMITE			4.5
Wauk 1983	UN	99	35	431140	880405	N35A				4.38E-05	7			DOLOMITE			3.5
Wauk 1983	UN	12	35	431149	880433	N51A	816.6	40.0	45.4	5.75E-05	7			DOLOMITE			4.0
Wauk 1983	UN	99	35	431151	880410	N54A				2.67E-04	7			DOLOMITE			4.5
Wauk 1983	UN	99	35	431151	880410	N54B				2.05E-03	7			DOLOMITE			4.5
Wauk 1983	UN	99	35	431151	880334	N61B				3.73E-05	7			DOLOMITE			4.5
Wauk 1983	UN	12	35	431153	880442	N68B	804.0	133.0		9.91E-06	7			DOLOMITE			4.5
Wauk 1983	UN	12	35	431143	880453	N67B	774.2	56.0	62.5	4.87E-05	7			DOLOMITE			4.5
Wauk 1983	OC	99	35	431147	880413	N4	776.0	20.0	24.0	6.81E-04	7			DOLOMITE			4.5
Wauk 1983	OC	3	35	431152	880418	N30	803.3	34.0	40.0	4.94E-05	7			DOLOMITE			4.5
Wauk 1983	OC	3	35	431149	880425	N61	804.6	14.5	24.5	7.07E-06	7			DOLOMITE			4.5
Wauk 1984	OC	3	35	431141	880437	N71	821.9	18.5	20.0					DOLOMITE			4.5
Wauk 1984	OC	3	35	431143	880437	N72	819.9	23.5	25.0					DOLOMITE			4.5
Wauk 1984	OC	3	35	431143	880437	N73	819.9	33.5	35.0					DOLOMITE			4.5
Wauk 1984	OC	5	35	431142	880439	N73	819.9	38.5	40.0					DOLOMITE			4.5
Wauk 1984	OC	3	35	431145	880437	N74	814.3	6.0	7.5					DOLOMITE			4.5
Wauk 1984	OC	3	35	431145	880436	N75	818.3	8.5	10.0					DOLOMITE			4.5
Wauk 1984	OC	5	35	431149	880437	N76	812.3	8.5	10.0					DOLOMITE			4.5
Wauk 1984	OC	5	35	431149	880437	N76	812.3	18.5	20.0					DOLOMITE			4.5
Wauk 1984	OC	3	35	431148	880430	N79	817.0	18.5	20.0					DOLOMITE			4.5
Wauk 1984	OC	3	35	431148	880430	N79	817.0	33.5	35.0					DOLOMITE			4.5
Wauk 1984	OC	3	35	431152	880426	N80	804.7	13.5	15.0					DOLOMITE			4.5
Wauk 1984	OC	3	35	431149	880425	N81	834.6	6.0	7.5					DOLOMITE			4.5
Wauk 1985	OC	3	35	431199	880499	B41	817.0							DOLOMITE			4.5
Wauk 1985	OC	3	35	431199	880499	B42	816.0							DOLOMITE			4.5
Wauk 1985	OC	3	35	431199	880499	B43	813.0							DOLOMITE			4.5
Wauk 1985	OC	3	35	431199	880499	B44	814.0							DOLOMITE			4.5
Wauk 1985	OC	3	35	431199	880499	B45	821.0							DOLOMITE			4.5
Wauk 1985	OC	3	35	431199	880499	B46	819.0							DOLOMITE			4.5
Wauk 1985	OC	3	35	431199	880499	B47	819.0							DOLOMITE			4.5



[illegible]



[illegible]





### Appendix 3 - Hydrogeologic and Engineering Data for Waukesha County - Brookfield Site

[illegible]

[illegible]

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR WAUPACA COUNTY, TOWN OF ROYALTON SITE

+ IDENTITY	+ Litho- unit	+ Bat. Site (code)	+ Year (code)	+ Lat.	+ Long.	+ No.	+ Brog. Elev. (ft)	+ Surf. Elev. (ft)	+ Sample bottom (ft)	+ Hydraulic conductivity (cm/s)	+ Matrix Z Bath + Bulk Z (cm/s)	+ Matrix Z sand + silt (0.0025 to 0.002mm)	+ Matrix Z clay (0.002mm)	+ Unified Soil Class.	+ Bulk Percent P200	+ Drv Wt. (pcf)	+ SPt Moist. (%)	+ Liquid Plastic. (%)	+ UC index (sf)	+ (N) cont.(N)	+ limit	+ (sf)	+ (sf)
NP 1982	KE1	3	39	442034	885655	B1	811.7	2.0	3.5		2	35	43	22	CL	66	20	26	11	1.5			
NP 1982	KE	5	39	442034	885655	B1	811.7	14.5	16.0		0	14	77	9	CL-ML	91	38						
NP 1982	KE	3	39	442034	885655	B1	811.7	39.6	51.0	3.79E-05	7				CL-ML	63	19	21	7	4.5			
NP 1982	KE1	3	39	442029	885655	B2	803.8	4.5	6.0		7	37	37	27	ML-CL	71	75						
NP 1982	KE	4	39	442029	885655	B2	803.8	34.5	36.0		3	94	2	4	SP	7	40	20	7				
NP 1982	KE1	3	39	442023	885655	B3	801.4	9.5	11.0		2	31	49	20	ML-CL	71	44	30	7				
NP 1982	KE	4	39	442023	885655	B3	801.4	19.5	21.0		0	3	76	21	ML-CL	97	44	30	7				
NP 1982	KE1	3	39	442017	885655	B4	791.8	4.5	6.0		3	31	51	19	ML-CL	70	12	20	7	4.0			
NP 1982	KE	4	39	442017	885655	B4	791.8	14.5	16.0		0	89	10	1	SP	15	35						
NP 1982	KE	5	39	442023	885706	B5	788.6	19.5	21.0		0	2	80	18	CL-ML	99	42	29	7				
NP 1982	KE	4	39	442023	885706	B5	788.6	29.5	31.0		22	92	3	5	SP	6	42						

[illegible]

[illegible]



[illegible]



Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR WINNEBAGO COUNTY LANDFILL

+ IDENTITY	+ Litho- strat.	+ County (code)	+ Year (code)	+ Mat. Site (code)	+ Lat.	+ Long. no. (ft)	+ Surf. Elev. (ft)	+ Sample top (ft)	+ Sample bottom (ft)	+ CONDUCTIVITY		+ HYDRAULIC		+ ENGINEERING PROPERTIES		+ Bulk Dry Unit Wt. Percent Moist. SPT Resist. Liquid Plastic. UC Index (tsf)	
										Lab X code (cm/s)	Lab Y code (cm/s)	Matrix Z code (+2.00e-0425m)	Matrix X code (+2.00e-0425m)	Matrix Y code (+2.00e-0425m)	Matrix Z code (+2.00e-0425m)		Matrix X code (+2.00e-0425m)
MI 1982	UN	3	41	470347	883401	B-C-6	769.7	25.0	26.0								
MI 1982	UN	3	41	470347	883401	B-C-6	769.7	35.0	36.5								
MI 1982	UN	3	41	470347	883407	B-C-7	770.3	8.0	9.5								
MI 1982	UN	3	41	470347	883407	B-C-7	770.3	20.0	21.5								
MI 1982	UN	3	41	470350	883550	B-C-8	773.2	20.0	21.0								
MI 1982	UN	5	41	470350	883550	B-C-8	773.2	30.0	31.5								
MI 1982	UN	3	41	470350	883555	B-C-9	773.0	20.0	20.8								
MI 1982	UN	3	41	470350	883555	B-C-9	773.0	30.0	30.8								
MI 1982	UN	3	41	470350	883555	F30	773.0	39.5	42.5								
MI 1982	UN	3	41	470350	883555	F30	773.0	17.8	20.3								
MI 1982	UN	3	41	470356	883407	BC-10	765.6	8.0	9.5								
MI 1982	UN	3	41	470356	883407	BC-10	765.6	15.0	16.5								
MI 1982	UN	5	41	470350	883407	F28	765.6	25.5	27.5								
MI 1982	UN	3	41	470350	883407	F28	765.6	11.0	13.5								
MI 1982	UN	3	41	470352	883550	BC-11	768.2	20.0	21.0								
MI 1982	UN	3	41	470352	883550	BC-12	770.9	8.0	9.0								
MI 1982	UN	3	41	470352	883550	BC-12	770.9	19.0	20.0								
MI 1982	UN	3	41	470352	883555	BC-13	772.2	10.0	11.5								
MI 1982	UN	3	41	470352	883555	BC-13	772.2	20.0	21.0								
MI 1982	UN	3	41	470352	883401	BC-14	765.1	10.0	11.0								
MI 1982	UN	5	41	470352	883401	BC-14	765.1	19.0	20.5								
MI 1982	UN	3	41	470352	883407	BC-15	763.7	8.0	9.5								
MI 1982	UN	3	41	470352	883555	BC-15	763.7	15.0	16.5								
MI 1982	UN	3	41	470354	883555	BC-16	763.4	14.0	14.5								
MI 1982	UN	3	41	470354	883555	BC-16	763.4	24.5	25.0								
MI 1982	UN	3	41	470354	883555	P26	763.4	30.2	32.7								
MI 1982	UN	3	41	470354	883401	BC-17	763.3	15.0	16.0								
MI 1982	UN	3	41	470354	883401	P27	763.3	31.0	34.0								
MI 1982	UN	3	41	470354	883401	P27A	763.3	9.9	12.4								
MI 1982	UN	3	41	470344	883344</												

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+ IDENTITY	+ Litho- unit	+ Strat. unit	+ Dunit (code)	+ Year (code)	+ Site (code)	+ Lat.	+ Long.	+ Elev. ft)	+ Sample top	+ Hydralic + Conductivity	+ Matrix sand	+ Matrix silt	+ Matrix clay	+ ENGINEERING PROPERTIES			
														Unifed Bulk Percent Unit wt.	Dry Soil Class.	Soil Class.	Soil Class.
MI 1977	UN	3	41	470399	883499	84.2	760.5	0.0	5.0		27	45		SH	44		
MI 1977	UN	3	41	470399	883499	84.5	761.9	6.0	9.0		20	55		SH	28		
MI 1977	UN	3	41	470399	883499	85.3	765.3	0.0	4.5		34	47		SH	40		
MI 1977	UN	5	41	470399	883499	85.7	771.0	7.0	11.0		0	25		CL	82		
MI 1977	UN	99	41	470399	883499	81.2	760.7	3.0	6.0		6	28		CL-ML	71		
MI 1977	UN	3	41	470399	883499	81.2	760.7	3.0	6.0		8	51		SH	52		
MI 1977	UN	3	41	470399	883499	81.6	767.2	14.0	15.5		6	41		SH	58		
MI 1977	UN	3	41	470399	883499	81.7	773.0	6.0	12.5		37	49		SH	35		
MI 1977	UN	3	41	470399	883499	82.1	760.4	0.0	3.0		12	43		SH	54		
MI 1977	UN	3	41	470399	883499	82.2	760.1	0.0	5.0		20	50		SH	51		
MI 1977	UN	3	41	470399	883499	82.4	760.5	0.0	5.0		13	43		SH	58		
MI 1977	UN	3	41	470399	883499	82.6	762.3	3.0	6.0		12	38		ML	32		
MI 1977	UN	3	41	470399	883499	82.7	772.5	5.0	15.4		34	38		SH	49		
MI 1977	UN	3	41	470399	883499	83.1	760.8	9.0	9.5		13	48		SH	49		
MI 1977	UN	3	41	470399	883499	83.2	759.9	0.0	5.0		85	47		SH	49		
MI 1977	UN	3	41	470399	883499	83.3	760.7	0.0	5.0		29	36		SH	43		
MI 1977	UN	3	41	470399	883499	83.4	761.0	3.0	3.8		41	49		SH	19		
MI 1977	UN	3	41	470399	883499	83.5	762.1	3.0	6.0		15	53		SH	45		
MI 1977	UN	3	41	470399	883499	83.6	760.3	0.0	5.0		22	53		SH	41		
MI 1977	UN	3	41	470399	883499	83.7	771.9	10.5			10	41		SP	46		
MI 1977	UN	3	41	470399	883499	84.3	760.8	0.0	5.0		14	48		SH	52		
MI 1977	UN	3	41	470399	883499	84.4	761.4	0.0	5.0		13	48		SH	50		
MI 1977	UN	3	41	470399	883499	84.7	771.5	9.0	14.0		14	48		SH-SC	49		
MI 1977	UN	3	41	470399	883499	85.1	778.3	21.5	26.5		0			CL-ML	88		
MI 1977	UN	3	41	470399	883499	85.1	778.3	24.0	25.5		19	54		SH	42		
MI 1977	UN	3	41	470399	883499	85.5	765.9	6.0	9.0		23	41		SH	34		
MI 1977	UN	3	41	470399	883499	85.6	767.6	8.0	9.0		40	53		SH	30		
MI 1977	UN	3	41	470399	883499	86.1-9	15.0	20.5			14	45		SH	52		
MI 1977	UN	3	41	470399	883499	87.1	762.9	2.0	3.5	1.80E-06	3			CL	12		
MI 1977	UN	3	41	470399	883499	87.2	766.2	2.0	3.5	1.							

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR WINNEAGO COUNTY, WINNEAGO COUNTY LANDFILL

IDENTITY	Litho- strat.	County	Year	Nat. Site (code)	No.	HYDRAULIC			+ BRINE/SLT PERCENTAGES			+ ENGINEERING PROPERTIES															
						Lat.	Long.	Brn. no.	Surf. Elev.	Sand. Elev.	Top	Sand. Elev.	Bottom	Lab K	Meth	Fld K	Meth	Matrix Z	Matrix Z	Matrix Z	Unified	Brn	Percent Unit Wt.	SPF	Moist.	Liquid Plastic.	UC
MI 1975	KE	99	41	470354	883355	P3	761.8	4.0	5.0																		
MI 1975	UN	3	41	470354	883346	P-4-20	769.7	16.0	17.0																		
MI 1975	UN	12	41	470354	883346	P-4-40	769.7	36.0	37.0																		
MI 1975	UN	12	41	470354	883346	P-4-60	769.7	31.0	32.0																		
MI 1975	KEK1	3	41	470338	883344	P-5C	782.8	4.0	5.0																		
MI 1975	UN	3	41	470338	883344	P-5C	782.8	9.0	10.0																		
MI 1975	UN	3	41	470338	883327	P-6C	775.0	29.0	30.0																		
MI 1975	KEK1	3	41	470338	883327	P-6	775.0	9.0	10.0																		
MI 1975	KEK1	3	41	470339	883327	P-7C	777.7	4.0	5.0																		
MI 1975	UN	3	41	470339	883344	P-8C	777.2	34.0	35.0																		
MI 1975	UN	3	41	470332	883354	P-9C	782.4	49.0	50.0																		
MI 1975	KEK1	3	41	470334	883404	P-10C	775.8	9.0	10.0																		
MI 1975	KEK1	3	41	470334	883464	P-10C	775.8	14.0	15.0																		
MI 1975	UN	3	41	470332	883344	P5-20	782.8	19.0	20.0																		
MI 1975	UN	3	41	470338	883344	P5-40	782.8	28.0	30.0																		
MI 1975	UN	12	41	470338	883344	P5-60	782.8	46.5	49.0																		
MI 1975	UN	3	41	470334	883407	P3-20	761.8	18.0	19.0																		
MI 1975	UN	12	41	470354	883407	P3-25	761.8	33.0	34.0																		
MI 1975	UN	3	41	470354	883407	P11	766.0	19.0																			

+ IDENTITY		+ LITHO- strat.		+ COUNTY		+ HYDRAULIC + CONDUCTIVITY		+ BORINGS PERCENTAGES		+ ENGINEERING PROPERTIES		+	
Year	Unit	Lat.	Long.	Top	Surf.	Bottom	Lab	Field	Matrix	Matrix	Unified	Bulk	Dev
(code)	(code)			ft	ft	ft	(code)	(code)	2.0 to 10.025	2.0 to 10.025	Soil	Percent	Unit
									0.0025	0.0025	Class.	P200	(ccf)
ML 1984	OC	3	50	425216	875106	BP-1	709.3	0.0	1.5		CL	47.4	9
ML 1984	OC	3	50	425216	875106	BP-1	709.3	5.0	6.5		ML/SP	15	3.0
ML 1984	OC	3	50	425216	875106	BP-1	709.3	10.0	11.5		CL	15	4.5
ML 1984	OC	3	50	425216	875106	BP-1	709.3	15.0	16.5		CL	21	15 4.5
ML 1984	OC	3	50	425216	875106	BP-1	709.3	20.0	21.5		CL	19	15 4.5
ML 1984	OC	3	50	425216	875106	BP-1	709.3	25.0	26.5		CL	15	12.0 21 9 3.5
ML 1984	OC	3	50	425216	875106	BP-1	709.3	30.0	31.5		CL	18	2.5
ML 1984	OC	3	50	425216	875106	BP-1	709.3	35.0	36.5		ML	21	21.2
ML 1984	OC	3	50	425216	875106	BP-1	709.3	40.0	41.5		CL	11	2.1
ML 1984	OC	3	50	425216	875106	BP-1	709.3	45.0	46.5		CL	11	18.0 34 20 2.5
ML 1984	OC	3	50	425216	875106	BP-1	709.3	50.0	51.5		CL	22	2.5
ML 1984	OC	3	50	425216	875106	BP-1	709.3	55.0	56.5		CL	16	18.1
ML 1984	OC	3	50	425216	875106	BP-1	709.3	60.0	61.5		SP	62	2.5
ML 1984	OC	3	50	425216	875106	BP-2	699.8	0.0	1.5		SP	40	20.5
ML 1984	OC	3	50	425216	875106	BP-2	699.8	5.0	6.5		CL	5	1.5
ML 1984	OC	3	50	425216	875106	BP-2	699.8	10.0	11.5		CL	12	3.0
ML 1984	OC	3	50	425216	875106	BP-2	699.8	15.0	16.5		CL	16	16.0
ML 1984	OC	3	50	425216	875106	BP-2	699.8	20.0	21.5		ML	15	18.4
ML 1984	OC	3	50	425216	875106	BP-2	699.8	25.0	26.5		CL	15	15.0 2.3
ML 1984	OC	3	50	425216	875106	BP-2	699.8	30.0	31.5		CL	15	16.4 26 12 2.2
ML 1984	OC	3	50	425216	875106	BP-2	699.8	35.0	36.5		CL	17	3.5
ML 1984	OC	3	50	425216	875106	BP-2	699.8	40.0	41.5		CL/ML	15	2.6
ML 1984	OC	3	50	425216	875106	BP-2	699.8	45.0	46.5		CL	20	14.8 27 14 3.5
ML 1984	OC	3	50	425216	875106	BP-2	699.8	50.0	51.5		CL	21	3.4
ML 1984	OC	3	50	425216	875106	BP-2	699.8	55.0	56.5		CL	19	2.5
ML 1984	OC	3	50	425216	875106	BP-2	699.8	60.0	61.5		CL	25	2.5
ML 1984	OC	3	50	425216	875106	BP-3	689.1	0.0	1.5				

[illegible]

## Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR MILWAUKEE COUNTY - BENDER PARK

+ IDENTITY	Litho- strat.	+ County (code) Year	unit (code)	Mat. Site (code)	No.	Lat.	Long.	Bnd. no.	Elev. top (ft)	Samp. Elev. bot (ft)	+ Hydraulic + Conductivity (cm/s)	+ GRAINSIZE PERCENTAGES + Matrix % Matrix % + sand silt clay	+ ENGINEERING PROPERTIES + Unified Soil + Class. P200 (pcf)	+ Bulk Unit Wt. + SPT Moist. Liquid Plastic. UC + (H) cont. (2) limit index (tsf) +
ML 1982	OC	3	50	425150	875047	B-2	487.0	25.0	26.5					CL
ML 1982	OC	3	50	425150	875047	B-2	487.0	30.0	31.5					CL
ML 1982	OC	3	50	425150	875047	B-2	487.0	35.0	36.0					CL
ML 1982	OC	3	50	425147	875046	B-4	492.0	0.0	1.0					CL
ML 1982	OC	3	50	425147	875046	B-4	492.0	1.5	3.0					ML-CL
ML 1982	OC	3	50	425147	875046	B-4	492.0	4.0	5.5					ML-CL
ML 1982	OC	3	50	425147	875046	B-4	492.0	6.0	7.0					CL
ML 1982	OC	3	50	425147	875046	B-4	492.0	10.0	10.5					CL
ML 1982	OC	3	50	425147	875046	B-4	492.0	15.0	15.5					CL
ML 1982	OC	3	50	425147	875046	B-4	492.0	20.0	20.5					CL
ML 1982	OC	3	50	425147	875046	B-4	492.0	25.0	27.0					CL
ML 1982	OC	3	50	425147	875046	B-4	492.0	30.0	32.0					CL
ML 1982	OC	3	50	425147	875046	B-4	492.0	35.0	37.0					CL
ML 1982	OC	3	50	425146	875054	B-5	701.0	0.0	1.5					CL
ML 1982	OC	3	50	425146	875054	B-5	701.0	2.0	3.5					CL
ML 1982	OC	3	50	425146	875054	B-5	701.0	4.0	5.5					CL
ML 1982	OC	3	50	425146	875054	B-5	701.0	6.0	7.5					CL
ML 1982	OC	3	50	425146	875054	B-5	701.0	10.0	11.5					CL
ML 1982	OC	3	50	425146	875054	B-5	701.0	15.0	16.5					CL
ML 1982	OC	3	50	425146	875054	B-5	701.0	20.0	21.0					CL
ML 1982	OC	3	50	425146	875054	B-5	701.0	25.0	27.0					CL
ML 1982	OC	3	50	425146	875054	B-5	701.0	30.0	31.5					CL
ML 1982	OC	3	50	425146	875054	B-5	701.0	35.0	36.5					CL
ML 1982	OC	3	50	425145	875048	B-6	695.0	0.0	1.5					CL
ML 1982	OC	3	50	425145	875048	B-6	695.0	2.0	3.0					CL
ML 1982	OC	3	50	425145	875048	B-6	695.0	4.0	5.5					CL
ML 1982	OC	3	50	425145	875048	B-6	695.0	6.0	7.5					CL
ML 1982	OC	3	50	425145	875048	B-6	695.0	10.0	11.0					CL-SH
ML 1982	OC	3	50	425145	875048	B-6	695.0	11.0	11.5					ML-CL
ML 1982	OC	3	50	425145	875048	B-6	695.0	11.5	12.0					CL
ML 1982	OC	3	50	425145	875048	B-6	695.0	15.0	16.5					CL
ML 1982	OC	3	50	425145	875048	B-6	695.0	20.0	22.0					ML
ML 1982	OC	3	50	425145	875048	B-6	695.0	25.0	27.0					SH
ML 1982	OC	3	50	425145	875048	B-6	695.0	30.0	31.5					ML-SH
ML 1982	OC	3	50	425145	875048	B-6	695.0	35.0	36.5					CL









Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR MILWAUKEE COUNTY - FALK LANDFILL

+ IDENTITY	+ litho- strat.	+ County unit	+ Nat. Site	+ (code) Year (code) (code) No.	+ Lat.	+ Long. no.	+ Brog. Elev. no. (ft)	+ Surf. Elev. top (ft)	+ Sample bottom (ft)	+ CONDUCTIVITY Lab K Meth (cc/s)	+ Hyd K (cc/s)	+ Matrix I sand (2.0 to 10.025 to 0.0025) + 0.0025	+ Matrix I silt (0.0025 to 0.0025) + 0.0025	+ Matrix I clay (0.0025 to 0.0025) + 0.0025	+ ENGINEERING PROPERTIES	+ Unified Soil Class.	+ Percent Unit Wt. P200 (pcf)	+ SPT Moist. Liquid Plastic. UC (NO cont. (2) limit index (pcf) +
ML 1980	OC	3	52	425524	875153	B-9	639.6	26.0	31.0									
ML 1980	OC	4	52	425519	875159	B-13	633.2	3.5	5.0									
ML 1980	OC	4	52	425519	875159	B-13	633.2	8.5	10.0									
ML 1980	OC	5	52	425519	875159	B-13	633.2	13.5	15.0									
ML 1980	OC	4	52	425519	875159	B-13	633.2	18.5	20.0									
ML 1980	OC	4	52	425519	875159	B-13	633.2	23.5	25.0									
ML 1980	OC	3	52	425519	875159	B-13	633.2	28.5	30.0									
ML 1980	OC	4	52	425519	875159	B-13	633.2	33.5	35.0									
ML 1980	OC	4	52	425519	875159	B-13	633.2	38.5	40.0									
ML 1980	OC	4	52	425515	875158	B-14	633.2	3.5	5.0									
ML 1980	OC	4	52	425515	875158	B-14	633.2	8.5	10.0									
ML 1980	OC	3	52	425515	875158	B-14	633.2	13.5	15.0									
ML 1980	OC	3	52	425515	875158	B-14	633.2	18.5	20.0									
ML 1980	OC	3	52	425515	875158	B-14	633.2	22.5	25.0									
ML 1980	OC	4	52	425515	875158	B-14	633.2	28.5	30.0									
ML 1980	OC	4	52	425515	875158	B-14	633.2	33.5	35.0									
ML 1980	OC	4	52	425513	875158	B-14	633.2	38.5	40.0									
ML 1980	OC	4	52	425516	875156	B-15	630.0	3.5	5.0									
ML 1980	OC	5	52	425516	875156	B-15	630.0	8.5	10.0									
ML 1980	OC	3	52	425516	875156	B-15	630.0	13.5	15.0									
ML 1980	OC	3	52	425516	875156	B-15	630.0	18.5	20.0									
ML 1980	OC	3	52	425516	875156	B-15	630.0	23.5	25.0									
ML 1980	OC	3	52	425516	875156	B-15	630.0	28.5	30.0									
ML 1980	OC	5	52	425516	875156	B-15	630.0	33.5	35.0									
ML 1980	OC	5	52	425516	875156	B-15	630.0	38.5	40.0									
ML 1980	OC	5	52	425516	875156	B-15	630.0	43.5	45.0									
ML 1980	OC	5	52	425516	875156	B-15	630.0	5.0	10.0									

6.30E-05

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR WADSWORTH COUNTY - FUTURE PARKLAND SITE

+ IDENTITY				+ HYDRAULIC				+ GRAIN-SIZE PERCENTAGES				+ ENGINEERING PROPERTIES									
+ County	+ Litho.	+ Strat.	+ Unit	+ Lat.	+ Long.	+ Brog. no.	+ Elev. (ft)	+ Surf. Elev. (ft)	+ Sample Size (ft)	+ Top (ft)	+ Bottom (ft)	+ Lab X Meth (cm/s)	+ Fld X Meth (cm/s)	+ Bulk X Meth (cm/s)	+ Soil (cm/s)	+ Unified	+ Bulk	+ Dry	+ SPT	+ Moist. Liquid Plastic. UC	+ (M) cont. (L) limit index (Isf) +
+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)	+ (code)
OK 1984	OC	3	53	425127	880446	M418	788.0	3.5	5.0												
OK 1984	OC	3	53	425127	880446	M418	788.0	8.5	10.0												
OK 1984	OC	3	53	425127	880446	M418	788.0	13.5	15.0												
OK 1984	OC	3	53	425127	880446	M418	788.0	18.5	20.0												
OK 1984	OC	3	53	425127	880446	M418	788.0	23.5	25.0												
OK 1984	OC	3	53	425127	880446	M418	788.0	28.5	30.0												
OK 1984	OC	3	53	425127	880446	M418	788.0	33.5	35.0												
OK 1984	OC	2	53	425127	880446	M418	788.0	38.5	40.0												
OK 1984	OC	3	53	425127	880446	M418	788.0	43.5	45.0												
OK 1984	OC	3	53	425127	880446	M418	788.0	48.5	50.0												
OK 1984	OC	3	53	425127	880446	M418	788.0	53.5	55.0												
OK 1984	OC	3	53	425127	880446	M418	788.0	58.5	60.0												
OK 1984	OC	3	53	425116	880441	M446/B	792.0	3.5	5.0												
OK 1984	OC	3	53	425116	880441	M446/B	792.0	8.5	10.0												
OK 1984	OC	3	53	425116	880441	M446/B	792.0	13.5	15.0												
OK 1984	OC	3	53	425116	880441	M446/B	792.0	18.5	20.0												
OK 1984	OC	3	53	425116	880441	M446/B	792.0	23.5	25.0												
OK 1984	OC	3	53	425116	880441	M446/B	792.0	28.5	30.0												
OK 1984	OC	3	53	425116	880441	M446/B	792.0	33.5	35.0												
OK 1984	OC	3	53	425116	880441	M446/B	792.0	38.5	40.0												
OK 1984	OC	3	53	425116	880441	M446/B	792.0	43.5	45.0												
OK 1984	OC	3	53	425116	880441	M446/B	792.0	48.5	50.0												
OK 1984	OC	3	53	425116	880441	M446/B	792.0	53.5	55.0												
OK 1984	OC	3	53	425116	880441	M446/B	792.0	58.5	60.0												
OK 1984	OC	3	53	425128	880436	M45A	781.0	3.5	5.0												
OK 1984	OC	3	53	425128	880436	M45A	781.0	8.5	10.0												
OK 1984	OC	3	53	425128	880436	M45A	781.0	13.5	15.0												
OK 1984	OC	3	53	425128	880436	M45A	781.0	18.5	20.0												
OK 1984	OC	3	53	425128	880436	M45A	781.0	23.5	25.0												
OK 1984	OC	3	53	425128	880436	M45A	781.0	28.5	30.0												
OK 1984	OC	3	53	425128	880436	M45A	781.0	33.5	35.0												
OK 1984	OC	3	53	425128	880436	M45A	781.0	38.5	40.0												
OK 1984	OC	3	53	425128	880436	M45A	781.0	43.5	45.0												
OK 1984	OC	3	53	425128	880436	M45A	781.0	48.5	50.0												
OK 1984	OC	3	53	425128	880436	M45A	781.0	53.5	55.0												
OK 1984	OC	3	53	425128	880436	M45A	781.0	58.5	60.0												
OK 1984	OC	3	53	425131	880452	M45A/B	777.6	3.5	5.0												
OK 1984	OC	3	53	425131	880452	M45A/B	777.6	8.5	10.0												
OK 1984	OC	3	53	425131	880452	M45A/B	777.6	13.5	15.0												
OK 1984	OC	3	53	425131	880452	M45A/B	777.6	18.5	20.0												
OK 1984	OC	3	53	425131	880452	M45A/B	777.6	23.5	25.0												
OK 1984	OC	3	53	425131	880452	M45A/B	777.6	28.5	30.0												
OK 1984	OC	3	53	425131	880452	M45A/B	777.6	33.5	35.0												
OK 1984	OC	3	53	425131	880452	M45A/B	777.6	38.5	40.0												
OK 1984	OC	3	53	425131	880452	M45A/B	777.6	43.5	45.0												

2.80E-08

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Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR WAUKESHA COUNTY - FUTURE PARKLAND SITE

[illegible]

### Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR WAUKESHA COUNTY - FUTURE PARKLAND SITE

+ IDENTITY										+ HYDRAULIC				+ GRAINSIZE PERCENTAGES				+ ENGINEERING PROPERTIES								
+ County		Litho-strat.	Mat.	Site	Surr.		Sample	+ CONDUCTIVITY		+ Matrix % sand		Matrix % silt	Matrix % clay	+ Unified		Bulk	Dry									
(code)	Year	(code)	(code)	No.	Lat.	Long.	No.	Elev. (ft)	top (ft)	bottom (ft)	Lab K (cm/s)	Meth code	Fld K (cm/s)	Meth code	+ Bulk %	(2.0 to 0.0625mm)	(0.0625 to 0.002mm)	((0.002mm))	+ Soil Class.	Percent P200	Unit Wt. (pcf)	SPT (N)	Moist. cont. (%)	Liquid limit	Plastic index	UC (tsf)
WK	1985	OC	3	53	425121	880452	NW10A	781.9	18.5	20.0									CL							
WK	1985	OC	3	53	425121	880452	NW10A	781.9	23.5	25.0									CL			13				
WK	1985	OC	3	53	425121	880452	NW10A	781.9	28.5	30.0									CL			9				
WK	1985	OC	3	53	425121	880452	NW10A	781.9	33.5	35.0									CL			10				
WK	1985	OC	3	53	425121	880452	NW10A	781.9	37.5	40.0									CL			12				
WK	1985	OC	3	53	425121	880452	NW10A	781.9	43.5	45.0									CL			13				
WK	1985	OC	3	53	425121	880452	NW10A	781.9	48.5	50.0									CL			13				
WK	1985	OC	3	53	425121	880452	NW10A	781.9	9.0	21.0		5.60E-07	7						CL							
WK	1985	OC	3	53	425123	880433	NW11A	787.2	3.5	5.0									CL			15				
WK	1985	OC	3	53	425123	880433	NW11A	787.2	8.5	10.0									CL			14				
WK	1985	OC	3	53	425123	880433	NW11A	787.2	13.5	15.0									CL			11				
WK	1985	OC	3	53	425123	880433	NW11A	787.2	18.5	20.0									CL			11				
WK	1985	OC	3	53	425123	880433	NW11A	787.2	23.5	25.0									CL			11				
WK	1985	OC	3	53	425123	880433	NW11A	787.2	28.5	30.0									CL			12				
WK	1985	OC	3	53	425123	880433	NW11A	787.2	33.5	35.0									CL			11				
WK	1985	OC	3	53	425123	880433	NW11A	787.2	37.5	40.0									CL			11				
WK	1985	OC	3	53	425123	880433	NW11A	787.2	43.5	45.0									CL			13				
WK	1985	OC	3	53	425123	880433	NW11A	787.2	48.5	50.0									CL			14				
WK	1985	OC	3	53	425123	880433	NW11A	787.2	53.5	55.0									CL			14				
WK	1985	OC	3	53	425123	880433	NW11A	787.2	14.0	26.0		4.60E-08	7						CL			14				
WK	1985	OC	3	53	425115	880445	NW12A	784.1	3.5	5.0									CL			7				
WK	1985	OC	3	53	425115	880445	NW12A	784.1	8.5	10.0									CL			5				
WK	1985	OC	3	53	425115	880445	NW12A	784.1	13.5	15.0									CL			21				
WK	1985	OC	3	53	425115	880445	NW12A	784.1	18.5	20.0									CL			10				
WK	1985	OC	3	53	425115	880445	NW12A	784.1	23.5	25.0									CL			7				
WK	1985	OC	3	53	425115	880445	NW12A	784.1	28.5	30.0									CL			8				
WK	1985	OC	3	53	425115	880445	NW12A	784.1	33.5	35.0									CL			9				
WK	1985	OC	3	53	425115	880445	NW12A	784.1	38.5	40.0									CL			11				
WK	1985	OC	3	53	425115	880445	NW12A	784.1	43.5	45.0									CL			14				
WK	1985	OC	3	53	425115	880445	NW12A	784.1	48.5	50.0									CL			16				
WK	1985	OC	3	53	425115	880445	NW12A	784.1	9.0	21.0		2.00E-06	7						CL							
WK	1985	OC	3	53	425117	880428	NW13AB	803.4	3.5	5.0									CL			15				
WK	1985	OC	3	53	425117	880428	NW13AB	803.4	8.5	10.0									CL			40				
WK	1985	OC	3	53	425117	880428	NW13AB	803.4	13.5	15.0									CL			22				
WK	1985	OC	3	53	425117	880428	NW13AB	803.4	18.5	20.0									CL			22				
WK	1985	OC	3	53	425117	880428	NW13AB	803.4	23.5	25.0									CL			16				
WK	1985	OC	3	53	425117	880428	NW13AB	803.4	28.5	30.0									CL			22				
WK	1985	OC	3	53	425117	880428	NW13AB	803.4	33.5	35.0									CL			17				
WK	1985	OC	3	53	425117	880428	NW13AB	803.4	38.5	40.0									CL			16				
WK	1985	OC	3	53	425117	880428	NW13AB	803.4	43.5	45.0									CL			15				
WK	1985	OC	3	53	425117	880428	NW13AB	803.4	48.5	50.0									CL			16				
WK	1985	OC	3	53	425117	880428	NW13AB	803.4	53.5	55.0									CL			16				
WK	1985	OC	3	53	425117	880428	NW13AB	803.4	58.5	60.0									CL			17				
WK	1985	OC	3	53	425117	880428	NW13AB	803.4	63.5	65.0									CL			17				
WK	1985	OC	3	53	425117	880428	NW13AB	803.4	67.5	70.0									CL			36				
WK	1985	OC	3	53	425117	880428	NW13AB	803.4	73.5	75.0						0	0	50	50	CL	100.0	107.0		21.5	43	22

+ IDENTITY		Litho- strat.	Unit	Mat. Site (code) Year	Lat.	Long.	Brook no. (ft)	Surf. Elev. (ft)	Sample Saddle Top Bottom (ft) (ft)	+ HYDRAULIC		+ GRAINISTE PERCENTAGES		+ ENGINEERING PROPERTIES					
+	+									+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
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+	+	+	+																







Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR MILWAUKEE COUNTY - (MPCO) CALVERTON EXPANSION

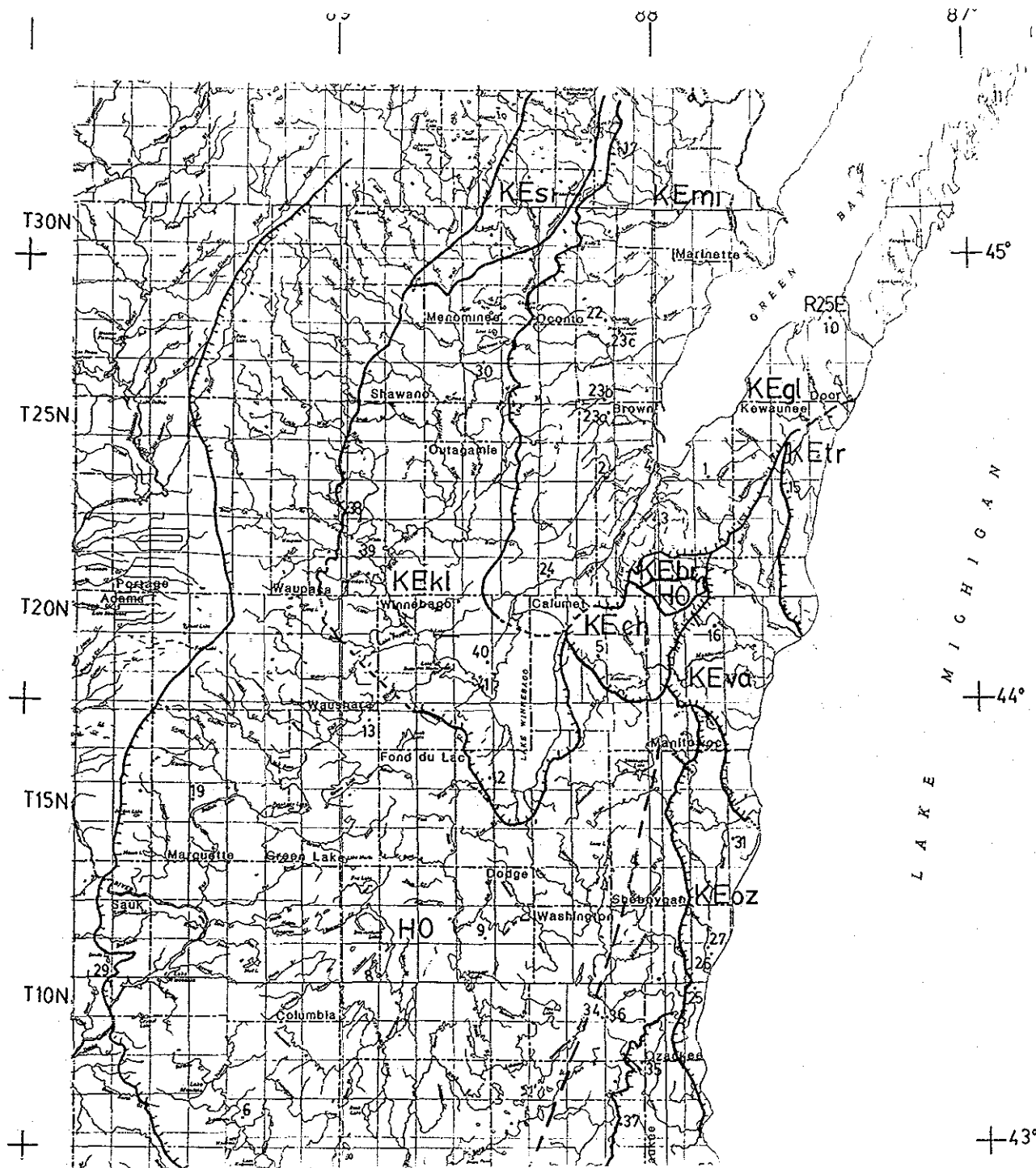
+ IDENTITY		Litho- strat.	+ County unit	Mat. Site (code)	Year	Lat.	Long.	Brg. no.	Elev. (ft)	Sample top (ft)	Sample bottom (ft)	+ HYDRAULIC + CONDUCTIVITY		+ GRAIN SIZE PERCENTAGES			+ ENGINEERING PROPERTIES																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																													

[illegible]

+ IDENTITY			+ LITHO-STRAT.			+ DENSITY			+ HYDRAULIC			+ SOILSIZING PERCENTAGES			+ ENGINEERING PROPERTIES										
Year	Code	Unit	Mat.	Site	Lat.	Long.	Bro. no.	Surf. Elev.	Top	Bottom	Lab K	Meth	Fld K	Meth	Matrix %	Matrix %	Matrix %	Unified	Bank	Dev	SPT	Moist.	Liquid Plastic	UC	
(code)	(code)	(code)	(code)	(code)				(ft)	(ft)	(ft)	(cm/s)	code	(cm/s)	code	(cm/s)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)
1982	DC	3	55	425338	881046	14-42	837.6	43.5	45.0																
1982	DC	3	55	425338	881046	14-42	837.6	48.5	50.0																
1982	DC	3	55	425338	881046	14-42	837.6	52.5	55.0																
1982	DC	4	55	425338	881046	14-42	837.6	58.5	60.0																
1982	DC	3	55	425338	881030	P-439	837.6	62.5	65.0																
1982	DC	3	55	425348	881030	P-439	838.4	3.5	5.0																
1982	DC	3	55	425348	881030	P-439	838.4	8.5	10.0																
1982	DC	3	55	425348	881030	P-439	838.4	13.5	15.0																
1982	DC	3	55	425348	881030	P-439	838.4	18.5	20.0																
1982	DC	5	55	425348	881030	P-439	838.4	23.5	25.0																
1982	DC	5	55	425348	881030	P-439	838.4	28.5	30.0																
1982	DC	5	55	425348	881030	P-439	838.4	33.5	35.0																
1982	DC	5	55	425348	881030	P-439	838.4	38.5	40.0																
1982	DC	5	55	425348	881030	P-439	838.4	43.5	45.0																
1982	DC	5	55	425348	881030	P-439	838.4	48.5	50.0																
1982	DC	5	55	425348	881030	P-439	838.4	53.5	55.0																
1982	DC	5	55	425348	881030	P-439	838.4	58.5	60.0																
1982	DC	3	55	425348	881030	P-439	838.4	63.5	65.0																
1982	DC	3	55	425348	881030	P-439	838.4	68.5	70.0																
1982	DC	3	55	425348	881030	P-439	838.4	73.5	75.0																



+ IDENTITY			+ LITHO-STRAT.			+ COUNTY			+ HYDRAULIC			+ STRAINING PERCENTAGES			+ ENGINEERING PROPERTIES								
Year	Code	Unit	Mat.	Site	No.	Lat.	Long.	Brook. Elev.	Surf. Elev.	Top	Bottom	Lab K	Field K	Matrix	Matrix	Matrix	Unified	Soil	Percent Unit Wt.	SF	Moist.	Liquid Plastic	UC
(code)	(code)	(code)	(code)	(code)	(code)	(code)	(code)	(ft)	(ft)	(ft)	(ft)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)
1984	MB	3	55	425340	881046	8-72	852.7	63.5	65.0														
1984	MB	3	55	425340	881046	8-72	852.7	68.5	70.0														
1984	MB	3	55	425340	881046	8-72	852.7	73.5	75.0														
1984	MB	3	55	425340	881046	8-72	852.7	78.5	80.0														
1984	MB	3	55	425340	881046	8-72	852.7	83.5	85.0														
1984	MB	3	55	425340	881046	8-72	852.7	88.5	90.0														
1984	MB	3	55	425340	881046	8-72	852.7	93.5	95.0														
1984	MB	3	55	425340	881046	8-72	852.7	98.5	100.0														
1982	OC	3	55	425337	881049	8-73	834.5	3.5	5.0														
1982	OC	3	55	425337	881049	8-73	834.5	8.5	10.0														
1982	OC	3	55	425337	881049	8-73	834.5	13.5	15.0														
1982	OC	3	55	425337	881049	8-73	834.5	18.5	20.0														
1982	OC	4	55	425337	881049	8-73	834.5	23.5	25.0														
1982	OC	3	55	425337	881049	8-73	834.5	28.5	30.0														
1982	OC	3	55	425337	881049	8-73	834.5	33.5	35.0														
1982	OC	3	55	425337	881049	8-73	834.5	38.5	40.0														
1982	OC	3	55	425337	881049	8-73	834.5	43.5	45.0														
1982	OC	3	55	425337	881049	8-73	834.5	48.5	50.0														
1982	OC	3	55	425337	881049	8-73	834.5	53.5	55.0														
1982	OC	3	55	425337	881049	8-73	834.5	58.5	60.0														
1982	OC	5	55	425337	881049	8-73	834.5	63.5	65.0														
1982	OC	5	55	425337	881049	8-73	834.5	68.5	70.0														
1982	OC	3	55	425336	881036	8-76	824.5	3.5	5.0														
1982	OC	3	55	425336	881036	8-76	824.5	8.5	10.0														
1982	OC	3	55	425336	881036	8-76	824.5	13.5	15.0														
1982	OC	3	55	425336	881036	8-76	824.5	18.5	20.0														
1982	OC	3	55	425336	881036	8-76	824.5	23.5	25.0														
1982	OC	3	55	425336	881036	8-76	824.5	28.5	30.0														
1982	OC	3	55	425336	881036	8-76	824.5	33.5	35.0														
1982	OC	3	55	425336	881036	8-76	824.5	38.5	40.0														
1982	OC	3	55	425336	881036	8-76	824.5	43.5	45.0														
1982	OC	3	55	425336	881036	8-76	824.5	48.5	50.0														
1982	OC	3	55	425336	881036	8-76	824.5	53.5	55.0														
1982	OC	4	55	425336	881036	8-76	824.5	58.5	60.0														
1982	OC	4	55	425336	881036	8-76	824.5	63.5	65.0														
1982	OC	3	55	425336	881036	8-76	824.5	68.5	70.0														



# EXTENT OF ICE ADVANCES RESPONSIBLE FOR LITHOSTRATIGRAPHIC UNITS

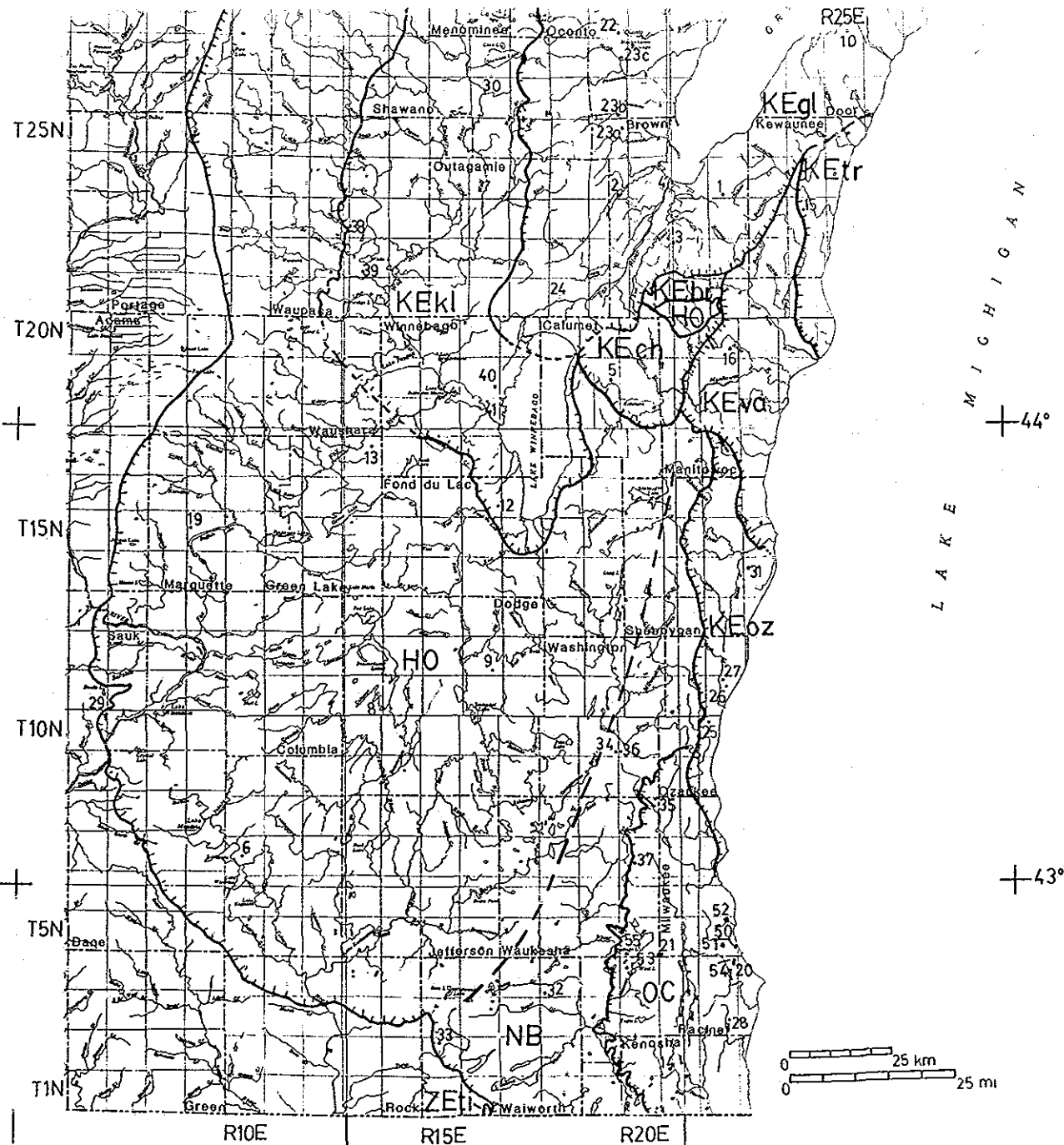
The extent of ice advances responsible for lithostratigraphic units is after Mickelson et al. (1984). Ice marginal positions are indicated by moraines; these were traced from Lineback et al. (1983) and Farrand et al. (1984). The tills in lithostratigraphic units were deposited by ice within the approximate margins drawn on this figure, but tills are not always present at the land surface within the margins. For example, till of the Glenmore Member does not cover all the land surface of the Door Peninsula (the peninsula separating Green Bay and Lake Michigan), but the ice advance that deposited the Glenmore Member covered the Door Peninsula entirely.

The southern extent of the glacial advance that deposited the Haven Member of the Kewaunee Formation is problematic. Mickelson et al. illustrate the Haven Member as extending farther south than the Valders Member. No southern ice margin associated with the Haven Member is shown here, and the mapped location in Mickelson et al. (1984) is "purely diagrammatic" (Mickelson, personal communication, 1987).

Site numbers are consistent throughout the text, illustrations, and appendices. Appendix 2 includes township and range coordinates for each site.

- 2 location of land disposal site studied
- inferred position of the ice margin
- ice marginal position indicated by a moraine

KE	Kewaunee Fm.
KEmi	Middle Inlet M.
KEkl	Kirby Lake M.
KEsi	Silver Cliff M.
KEgl	Glenmore M.
KEch	Chilton M.
KEbr	Branch River M.
KEtr	Two Rivers M.
KEva	Valders M.
KEha	Haven M.
KEoz	Ozaukee M.
OC	Oak Creek Fm.
NB	New Berlin Fm.



deposited by ice within the approximate margins drawn on this figure, but tills are not always present at the land surface within the margins. For example, till of the Glenmore Member does not cover all the land surface of the Door Peninsula (the peninsula separating Green Bay and Lake Michigan), but the ice advance that deposited the Glenmore Member covered the Door Peninsula entirely.

The southern extent of the glacial advance that deposited the Haven Member of the Kewaunee Formation is problematic. Mickelson et al. illustrate the Haven Member as extending farther south than the Valders Member. No southern ice margin associated with the Haven Member is shown here, and the mapped location in Mickelson et al. (1984) is "purely diagrammatic" (Mickelson, personal communication, 1987).

Site numbers are consistent throughout the text, illustrations, and appendices. Appendix 2 includes township and range coordinates for each site.

• 2 location of land disposal site studied

— inferred position of the ice margin

--- ice marginal position indicated by a moraine

KE	Kewaunee Fm.
KEml	Middle Inlet M.
KEkl	Kirby Lake M.
KEsl	Silver Cliff M.
KEgl	Glenmore M.
KEch	Chilton M.
KEbr	Branch River M.
KEtr	Two Rivers M.
KEva	Valders M.
KEha	Haven M.
KEoz	Ozaukee M.
OC	Oak Creek Fm.
NB	New Berlin Fm.
HO	Horicon Fm.
ZE	Zenda Fm.
ZEtl	Tiskilwa M.