University of Wisconsin-Extension

GEOLOGICAL AND NATURAL HISTORY SURVEY 3817 Mineral Point Road Madison, Wisconsin 53705

M.E. Ostrom, State Geologist and Director

MERGING PLEISTOCENE LITHOSTRATIGRAPHY WITH GEOTECHNICAL AND HYDROGEOLOGIC DATA - EXAMPLES FROM EASTERN WISCONSIN

bу

Sue Anita Rodenbeck

Open-File Report 88-9 303 p.

This report represents work performed by the Geological and Natural History Survey, and is released to the open files in the interest of making the information more readily available. This report has not been edited or reviewed for conformity with Geological and Natural History Survey standards and nomenclature.

PREFACE

This open-file report is a Master of Science thesis by Sue A Rodenbeck, University of Wisconsin-Madison Department of Geology and Geophysics. This work was completed while Ms Rodenbeck was employed as a Research Assistant by the Wisconsin Geological and Natural History Survey, and reflects the Survey's continuing interest in the hydrogeologic properties of Pleistocene materials in Wisconsin This study was funded through the Survey by a grant from the Wisconsin Department of Natural Resources.

This report contains the most complete synthesis to date of hydrogeologic and geotechnical data from solid waste disposal sites in eastern Wisconsin. These data, collected from 41 sites, are organized by lithostratigraphic unit, and are presented in spreadsheet format. The report discusses the values and ranges of variation of hydraulic conductivity, grain size, Atterberg Limits, and other parameters in relation to lithostratigraphic unit. The resulting analyses should be of interest to regulatory agencies and private firms involved in waste disposal and other shallow geotechnical projects in eastern Wisconsin.

Merging Pleistocene Lithostratigraphy with Geotechnical and
Hydrogeologic Data--Examples from Eastern Wisconsin

by

Sue Anita Rodenbeck

A thesis submitted in partial fulfillment of the requirements

for the degree of

Master of Science

(Geology)

at the University of Wisconsin - Madison

1988

ABSTRACT

The objectives of this project are: 1) to identify the hydrogeologic and geotechnical properties of Pleistocene materials in eastern Wisconsin, 2) to associate the properties with mappable, extensive hydrostratigraphic units that can be identified in the field, and 3) to assess the variability and expected range of values within the individual units. This study is a synthesis of hydrogeologic and engineering data submitted by geotechnical consulting firms to the Wisconsin Department of Natural Resources. Values of hydraulic conductivity (380), particle size analyses (475 completed to 002 mm), Atterberg limits (525), approximations of strength (964 pocket penetrometer measurements), and dry unit weights (155) were compiled, geologically interpreted, and assigned to the till units in five mapped formations of late Wisconsin age. Published definitions of lithostratigraphic units are used.

The data are organized by till unit, then statistically analyzed to examine variation of properties within each till unit and to compare till units of superposed lithostratigraphic units. In cases for which at least five field measurements of hydraulic conductivity (K) are available at more than one site within a single till unit, ANOVA tests suggest that the till units have significant internal variation in K. Thus, the till units are heterogeneous. Application of ANOVA tests to field measurements of separate till units also indicates heterogeneity. Median field measurements of K vary considerably among till units of late Wisconsin age, from 10⁻⁶ to

10⁻⁴ cm/s. With respect to laboratory measurements of K at more than one site within a single till unit, only one till is homogeneous in a statistical sense while the others are statistically significantly different, thus heterogeneous. In contrast to field measurements, ANOVA tests of laboratory measurements of K for superposed, separate till units suggest that not all the till units are significantly different. Moreover, median laboratory and field measurements of K frequently differ by more than an order of magnitude for a single till unit.

Underlying relationships among the data recorded are statistically analyzed using correlation and regression. Median values of each parameter for each till unit were used in the analysis because geotechnical properties and hydraulic conductivity are typically not determined for the same sample. A weak relation between plastic limit and log field hydraulic conductivity ($R^2 = 67\%$) and a relatively strong relationship between natural moisture content and dry unit weight ($R^2 = 80\%$) could be used by hydrogeologists and engineers to constrain modeled values of hydraulic conductivity

Wisconsin Administrative Code should be modified to require a standard method for calculation of hydraulic conductivity from field measurements and should cite a specific reference for use of the Unified Soil Classification System More than one classification and description system should be used, as no classification system seems best suited to hydrogeologic characterization. The lithostratigraphic framework has practical applications for landfill site assessment

since it is useful for predicting the occurrence and characteristics of subsurface materials

ACKNOWLEDGEMENTS

First of all, thanks are due to Dr. David Mickelson for accepting me as his student, for his criticism, and for his encouragement. Dr. Mary Anderson and Dr. Charlie Byers read the thesis, and I benefited from their comments. Dr. Ken Bradbury repeatedly read rough drafts that slowly drew less red ink; I am especially grateful for his provocative, helpful comments and good humor.

I would not have been able to complete my studies at the UW Madison if it were not for the financial assistance of the Jessie
Smith Noyes Foundation, the Wisconsin Geological and Natural History
Survey, and the Department of Geology and Geophysics The Department
of Natural Resources funded this project through the Wisconsin
Geological and Natural History Survey The staff at the Bureau of
Solid Waste Management, Wisconsin Department of Natural Resources
provided me with the background information necessary to collect data,
and the Bureau provided office space

My fellow graduate students provided a stimulating environment for the exchange of ideas and opinions. I would have given up without their support during especially difficult times. I owe special thanks to fellow users of the Quaternary lab.

My list of acknowledgments would be incomplete without mention of my parents. My father instilled me with a desire to understand nature and with the belief that people matter more than books. My mother encouraged me to choose my own path and cheerfully shared the cost

Table of Contents

		Page
I	Introduction	
	A. Reason for Study	1
	B Study definition	2
	C Location of study	4
	D Why combine geotechnical data with lithostratigraphy?	4
	E Problems of classification	7
	F. Combination of geological and geotechnical approaches	10
II.	Pleistocene History and Stratigraphy	
	A Stratigraphic Terminology	
	1 Definition of rock stratigraphic terms	13
	2 Definition of geochronologic terms	13
	3 Definition of diachronic terms	14
	B History of stratigraphic nomenclature in Wisconsin	16
	C. The late Wisconsin lithostratigraphic framework in	
	eastern Wisconsin	
	1. Introduction	16
	2 Zenda Formation	19
	3 New Berlin Formation	20
	4 Horicon Formation	21
	5. Oak Creek Formation	21
	6. Kewaunee Formation	22
	7. Importance of Pleistocene history and stratigraphy	25

		vii
	•	<u>Page</u>
III	Study Methods	
	A Application of lithostratigraphy	26
	B. USDA Soil Conservation Service reports	27
	C Geotechnical reports submitted in accord with	
	Wisconsin Administrative Code	
	1. The influence of Wisconsin Administrative Code	29
	2 Compilation of information required by NR 180	30
	D. Associating data with a lithostratigraphic unit	
	1. Stratigraphic nomenclature	31
	2. The different approaches taken by engineers and	
	geologists	32
	3. Distinction of till from other sedimentary facies	32
	4 Identification of lithostratigraphic units	33
	5 'Incompatible' maps and scales	34
	E The spreadsheet	35
	F. Spatial locations	35
	G. Choice of analytical tool	38
EV.	Presentation of Data	
	A Variation within tills of lithostratigraphic units	44
	1. Kewaunee Formation	45
	2 Oak Creek Formation	63
	3. Horicon Formation	68
	4 Unnamed unit	71

	viii
	Page
5 New Berlin Formation	74
6 Tiskilwa Member of the Zenda Formation	77
B Variation between tills of lithostratigraphic units	
1 Interunit comparison of hydraulic conductivity measure	∍d
in the field	77
2. Interunit comparison of hydraulic conductivity measure	∍d
in the laboratory	82
3 Vertical differences in texture	84
4 Interunit comparison of plasticity charts	85
5 Interunit comparison of dry unit weight	87
6. Pocket Penetrometer	90
V. Discussion of data	
A Approximations of strength	92
1. Standard penetration test	92
2 Pocket penetrometer	93
3 Applications of approximations of strength	93
B Particle size analysis	98
1. Till of the Middle Inlet Member of the Kewaunee	
Formation	101
2 Till of the Kirby Lake Member of the Kewaunee	
Formation	102
3 Till of the Glenmore Member of the Kewaunee Formation	104
4 Tills of the Chilton, Two Rivers Valders, Haven, and	

*	**
•	х.

		Page
	Ozaukee Members of the Kewaunee Formation	105
	5. Till of the Oak Creek Formation	105
	6 Till of the Horicon Formation	106
	7. Till of the unnamed unit	107
	8 Till of the New Berlin Formation	108
	9 Till of the Tiskilwa Member of the Zenda Formation	108
C	Atterberg Limits	
	1 Background	109
	2 Plasticity charts	111
	3 Clay mineralogy	114
	4 Activity	114
	5. Liquidity index	118
	6 Consistency index	119
Đ.	Classification in the Unified Soil Classification System	119
Ε.	Hydraulic conductivity	121
	1 Field measurements of hydraulic conductivity	124
	2 Laboratory measurements of hydraulic conductivity	126
F	Dry unit weight	128
G	Relationships between hydraulic conductivity and other	
	data	
	1 Hydraulic conductivity and plastic limit	130
	2. Hydraulic conductivity and dry unit weight	132
	3 Hydraulic conductivity and pocket penetrometer	
	measurements	134

	Page
H. Relationships between lithostratigraphic units and	
hydrostratigraphic units	134
I. Recommendations for sampling and testing procedures	136
VI. Summary and conclusions	
A. Summary	139
B. Conclusions	140
C Recommendations	142
	,
Works Cited	145
Appendix 1: Data required by Wisconsin Administrative Code	154
Appendix 2: Location summary	
Latitude and longitude	157
Topographic quadrangle, section, township, and range	159
Appendix 3: Data references and data	161

List of Figures

Fig	<u>ure</u>	Pag	<u>e</u>		
1.	Maximum extent of ice during late Wisconsin time.				
2	The U.S. Department of Agriculture textural triangle.	9			
3.	Definition of particle size classes	11			
4a.	Time-stratigraphic terminology	15			
4b.	Lithostratigraphic framework of the study area with				
	associated diachronic or event-stratigraphic phase names	in			
	parentheses	17			
5	Equivalent time-related stratigraphic names.	18			
6.	Surface distribution of named lithostratigraphic units of	f			
	late Wisconsin age.	28			
7 .	Features of the boxplot	42			
8a	Data for till in the Middle Inlet Member of the Kewaunee				
	Formation	46,	47		
8b	Data for till in the Kirby Lake Member of the Kewaunee				
	Formation	48,	49		
8c	Data for till in the Glenmore Member of the Kewaunee				
	Formation	50,	51		
8d.	Data for till in the Chilton Member of the Kewaunee				
	Formation	52,	53		
8e .	Data for till in the Two Rivers Member of the Kewaunee				
	Formation	54,	55		
8f.,	Data for till in the Valders Member of the Kewaunee				
	Formation	56.	57		

Fig	<u>ure</u>	<u>Pag</u>	<u>e</u>
8g	Data for till in the Haven Member of the Kewaunee		
	Formation	58,	59
8h	Data for till in the Ozaukee Member of the Kewaunee		
	Formation	60,	61
9	Data for till of the Oak Creek Formation	64,	65
10 .	Data for till of the Horicon Formation	69,	70
11	Data for an unnamed unit, possibly till of the Horicon		
	Formation	72,	73
12	Data for till of the New Berlin Formation	75,	76
13	Data for till of the Tiskilwa Member of the Zenda		
	Formation	78,	79
14	Boxplots for interunit comparison of hydraulic conductivity	У	
	measured in the field	80	
15.	Boxplots for interunit comparison of hydraulic conductivity	У	
	measured in the laboratory	83	
16	Plasticity chart with mean values of plasticity index and		
	liquid limit for tills of lithostratigraphic units	86	
17	Boxplots for interunit comparison of dry unit weight	88	
18	Boxplots for interunit comparison of pocket penetrometer		
	measurements	91	
19	Plot of SPT blow counts as a function of depth below land		
	surface for sediments in the Oak Creek Formation	95	
20 .	Plot of SPT blow counts as a function of pocket		
	penetrometer measurements	97	

Figu:	<u>r·e</u>	<u>Page</u>
21	Relationship between natural moisture content and log	
	pocket penetrometer measurements	99
22	Atterberg Limits related to volume and water content	110
23	Plasticity chart for a variety of soils.	113
24	Plots of plastic limit versus log plasticity index for	
	till units in superposed lithostratigraphic units.	115
25 .	Log hydraulic conductivity from field measurements versus	
	length of the saturated interval tested	127
26	Relationship between natural moisture content and dry	
	unit weight	129
27	Regression of median log hydraulic conductivity measured	
	in the field on mean plastic limit for fine-grained till	
	units	131
28.	Regression of median log hydraulic conductivity measured	
	in the field on median dry unit weight for till units	133
Plate	e 1 Extent of ice advances responsible for till units	
	(in pocket)	

List of Tables

<u>Tabl</u>	<u>e</u>	<u>Page</u>
1.	Description of 'soil' for classification.	8
2 ,	Categories of data recorded using the spreadsheet	36
3	Codes used to identify spreadsheet data	37
4	Statistical summary of dry unit weights.	89
5 .	Mean values of percentage greater than 2 mm, matrix	
	percent sand, matrix percent silt, and matrix percent	
	clay for selected till units by site	103
6	Summary of classification using activity, liquidity index,	
	and consistency index.	117

I. Introduction

A. Reason for study

Pleistocene materials cover roughly three-quarters of Wisconsin's surface, including its most densely populated areas, yet the hydrogeologic properties of these materials have not been fully assessed. Nationally, concern over human degradation of drinking water supplies has grown tremendously since the 1960s. Recent estimates indicate that ". . . 95 percent of rural America and in total about half the U.S. population rely on ground water" (U.S. EPA, 1987, p. 3). At the federal level, the actions of citizens concerned about degradation of water resources resulted in statutory laws like the National Environmental Pollution Act (1970), the Federal Water Pollution Control Act (1972), the Clean Water Act (1977), the Safe Drinking Water Act (1974), the Toxic Substances Control Act (1976), the Resource Conservation and Recovery Act (1976), and the Comprehensive Environmental Response, Compensation, and Liability Act (1980). These federal statutory laws required that the states create legislation to protect water resources. In Wisconsin, the Department of Natural Resources wrote Administrative Code Chapter NR 180, "Solid Waste Management," in response to Wisconsin Statutes Chapters 144 and 227 (Laws of 1977). Chapter NR 180 requires geotechnical investigations to document hydrogeologic conditions at proposed solid waste land disposal sites (hereafter referred to as 'landfills').

The data submitted in accord with NR 180 and similar regulations is important for protection of drinking water supplies near proposed

landfills, but much greater use could be made of the information if it could be easily retrieved and if it was organized so that a user could tell which information might be relevant to another location. Natural resource professionals working in the public and private sector are already accustomed to using written and computerized databases of well records and water quality analyses. A similar database of hydrogeologic and geotechnical data for Pleistocene materials in Wisconsin had not been attempted until this project. The Wisconsin Geological and Natural History Survey's Pleistocene mapping program and the development of a stratigraphic framework make this study possible.

B. Study definition

This study is part of a larger research project funded by the Wisconsin Department of Natural Resources and administered by the Wisconsin Geological and Natural History Survey. Long term objectives of the project are as follows:

- 1. To identify the hydrogeologic properties (permeability, porosity, etc.) and geotechnical properties (grain-size distribution, Atterberg limits, etc.) of Pleistocene materials in Wisconsin.
- 2. To associate these properties with mappable, areally extensive hydrostratigraphic units that can be identified in the field.
- 3. To assess the variability and expected range of values for these properties within any stratigraphic unit.
- 4. To develop field and laboratory methodologies for the evaluation of hydrogeologic and geotechnical properties in previously untested areas.

In keeping with these broad objectives, this study organizes and provides a geologic interpretation of the geotechnical and hydrogeologic information submitted in accord with NR 180 and other regulations for most of eastern Wisconsin. The lithostratigraphic framework defined in Pleistocene Stratigraphic Units in Wisconsin (Mickelson et al., 1984) is the organizational framework used to categorize the submitted data. I compiled the properties of samples and then assigned the data to a lithostratigraphic unit. I studied type and reference sections of these mapped units in the field to improve my interpretation of the data in reports. I combined the properties of each lithostratigraphic unit and then analyzed them. The statistical techniques used to assess the variability and the expected range of values are discussed later in this report. Although this study does not directly address the development of new methodologies, suggestions are made for improvements based on a review of existing geotechnical test methods and the statistical analysis of data.

In addition to the larger research project objectives, the data compilation, interpretation, and analysis completed here provide information for the discussion of three additional questions:

- 1. Are the formally defined lithostratigraphic units also hydrostratigraphic units?
- 2. Would other sampling and testing procedures better define the site hydrogeology?
- 3. Can geotechnical index tests function as lithic criteria to identify and differentiate units?

These issues are discussed in Part V.

C. Location of study

I collected data from reports of geotechnical investigations on file at the Bureau of Solid Waste Management, Wisconsin Department of Natural Resources. I limited the study's extent to late Wisconsin-aged glacial sediments in twenty-four counties of eastern Wisconsin glaciated by the Green Bay and Lake Michigan Lobes of the Laurentide Ice Sheet (Figure 1). Plate 1 (in pocket) illustrates the location of more than forty proposed or existing landfills. My emphasis on the collection of grain size analyses, atterberg limits, and hydraulic conductivities restricted data collection to sites with relatively recent investigations, usually located in areas of dense population or economic development requiring land disposal facilities.

D. Why combine geotechnical data with lithostratigraphy?

There are many good reasons for both engineers and geologists to organize geotechnical data into a lithostratigraphic framework.

Geologic studies provide relevant background information prior to detailed civil, structural, or foundation engineering investigations.

Geotechnical consultants unfamiliar with the state's Pleistocene materials may find the compiled index test data and summary of geologic history useful for bid preparation. Regulatory agencies can refer to the data analysis to evaluate the reasonableness of submitted reports containing geotechnical data for which no standardized quality assurance and quality control methods exist.

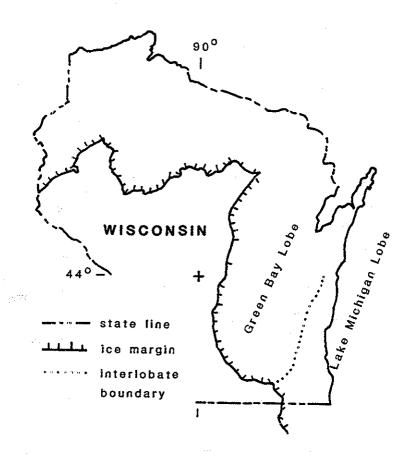


Figure 1. Maximum extent of ice during late Wisconsin time. Only the ice lobes pertinent to this study are labelled.

Hydrogeologists can use the hydraulic conductivity values reported here as input variables in groundwater flow models. Statistical summaries of hydraulic conductivity may be used to construct likely best and worst case scenarios for advective flow arrival times. Association of the hydraulic conductivity with mapped units makes it useful for site selection and screening on a statewide or regional scale.

Assessment of the local hydrogeologic setting prior to sitespecific investigation usually consists of reviewing regional or county water resources investigations and geologic studies, soil surveys, and remote sensing techniques such as aerial photography. Unfortunately, water resources investigations in Wisconsin have tended to focus on bedrock aquifers, and have restricted discussion of Pleistocene and Holocene sediments to sand and gravel aquifers. Soil surveys are generally limited to materials within 6 feet of the land surface. This report uses the lithostratigraphic framework (Mickelson et al., 1984) to present statistical summaries of geotechnical data for sediments from the land surface to bedrock, aquitards as well as aquifers. The same geologic conditions that make till units lithologically recognizable, areally continuous, and mappable may produce similar hydrogeologic and geotechnical properties within each unit. Once geotechnical data has been associated with lithostratigraphic units, the question, "Can geotechnical tests function as lithic criteria to differentiate units?" may be answered.

E. Problems of classification

The problem of how samples of earth materials should be described and classified has received considerable attention both in the past and in the present. The geologists who study the Quaternary materials in eastern Wisconsin define lithostratigraphic units using some or all of the criteria listed in Table 1 (Mickelson et al., 1984). The American Society for Testing Materials (ASTM) "Standard Practice for Classification of Soils for Engineering Purposes" (D2488-84, ASTM, 1986) relies upon the Unified Soil Classification System (USCS). The USCS criteria are also listed in Table 1. Soil scientists use yet another descriptive scheme (see Table 1) and have devoted considerable attention to the revisions to Chapter 4 in the Soil Survey Manual, "Examination and Description of Soils in the Field," (Soil Survey Staff, 1981). All of these classifications include grain size analysis and a description of the soil color; other criteria and descriptive terms are related but not synonymous.

Even the common factors of the classifications are expressed in different terms and thus are not directly transferable. For example, soil scientists and geologists who study the Quaternary describe the grain size distribution of a sample using a textural triangle (figure 2) on which sand, silt, and clay percentages of the less than 2 mm size fraction are plotted. Geotechnical reports for landfill investigations describe the grain size distribution of a sample using a USCS group name and group symbol. The same reports generally include graphs of cumulative percent finer versus particle size in

Table 1 Description of 'soil' for classification

a. -by geologists who study the Quaternary in eastern Wisconsin (Mickelson et al., 1984)

texture
munsell color
clay mineralogy
calcite to dolomite ratio
pebble lithology
stratigraphic position
magnetic susceptibility
depth of carbonate leaching

b. -by USCS (ASTM, 1986)

percent finer than the #200 sieve (0.075 mm) coefficient of uniformity coefficient of curvature liquid limit plastic index plotted location on the plasticity chart

c. -by soil scientists
 (Soil Survey Staff, 1981)
depth
munsell color
texture
structure
cutans
consistance
special features
reaction or effervescense
boundary

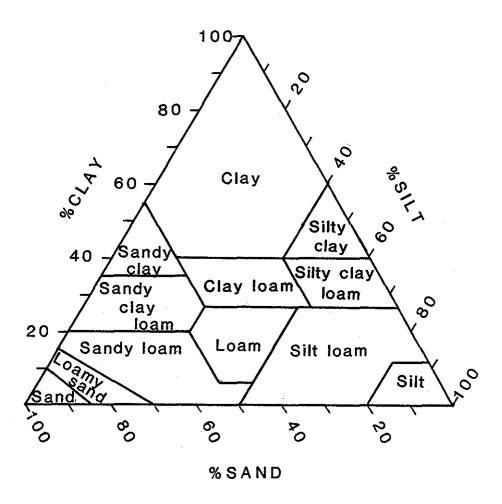


Figure 2. The U. S. Department of Agriculture (USDA) textural triangle. Both geologists and soil scientists use the textural triangle despite their differing definitions of silt and clay.

appendices. The exchange of information is hindered further by differing definitions of sand, silt, and clay. Figure 3 illustrates these definitions.

With respect to color, both Quaternary geologists and soil scientists use the Munsell color chart and notation (Munsell Color Co., Inc., Baltimore) in an attempt to standardize terminology. Geotechnical reports use descriptive phrases like "reddish-brown" that do not distinguish subtle variations in sediment color unless the phrases are standardized. Considering these inconsistent methods of sample description and classification, interdisciplinary transfer of information can be quite challenging.

F. Combination of geological and geotechnical approaches

The approach of assigning geotechnical data to stratigraphic units is not without precedent. Many authors have combined geotechnical data with glacial depositional or sedimentary models, but few, if any combine existing geotechnical data, including hydraulic conductivities, with a published formal lithostratigraphic framework. Kenney (1976) discusses glacial sedimentation in fresh and marine waters, the fabric of lacustrine sediments, and the relationship between the preceding factors and geotechnical behavior. May and Thompson (1978) discuss the Quaternary glacial deposits of the Edmonton area and describe circumstances in which lack of geologic interpretation can lead to engineering problems. Mickelson, Acomb, and Edil (1979) studied Wisconsin's Lake Michigan shoreline using

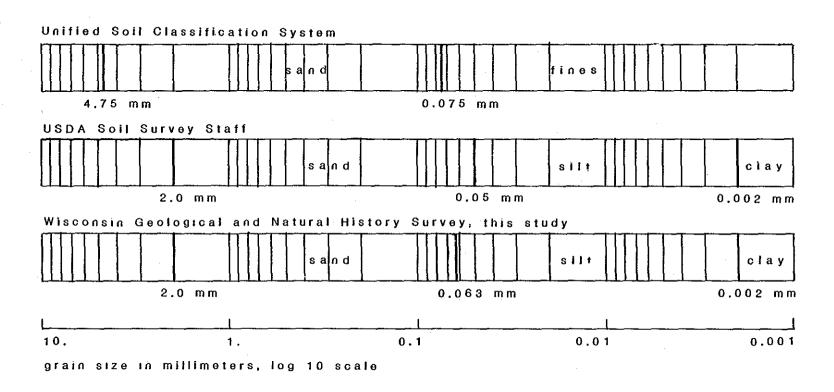


Figure 3. The USCS does not divide 'fines' into silt and clay fractions. The geologists studying the Quaternary materials in Wisconsin and soil scientists divide the silt and clay classes at different particle sizes.

engineering index properties and shear strength to interpret glacial processes. Singh, Tatioussian, and Flagg (1983) used a lithostratigraphic framework for their statistical summary of geotechnical data for the Milwaukee area and found the depositional environment valuable to their interpretation of the data. Baracos et al. (1983) prepared a series of engineering and geotechnical maps from geotechnical and geological data collected from several thousand boreholes in urban Winnipeg, Manitoba. Although Baracos et al. incorporated geological genetic terms, stratigraphy, sedimentary environment, and post-depositional changes in the environment, they did not use lithostratigraphic names for glacial sediments. Lo and McCabe (1984) used existing engineering and pedologic data, grouped by physiographic regions and soil classification, to create a geotechnical data base for Indiana. Similar studies too numerous to detail here include those by Chassefiere and Monaco (1983), Connell (1984), Eyles and Sladen (1981), Quigley (1980), and Richards (1976). This study is different from these for three reasons: 1) the geotechnical data base includes both hydraulic conductivity and engineering properties, 2) the properties have been organized with a published lithostratigraphic framework, and 3) data from diverse sources are organized within a single spatial coordinate system.

II. Pleistocene History and Stratigraphy

A. Stratigraphic terminology

1. Definition of rock stratigraphic terms

In addition to using the characteristics listed in Table 1, geologists subdivide, classify, and map sediments as stratigraphic units. The North American Stratigraphic Code (North American Commission on Stratigraphic Nomenclature (NACSN), 1983) requires that lithostratigraphic units be formally distinguished from each other and mapped on the basis of observable lithic characteristics and stratigraphic position. The formation is the fundamental unit in this system and must be mappable at land surface or traceable in the subsurface. Formations may be subdivided into members—these are the next lower hierarchy in the classification and need not be distinguishable in the field. Members are named when the formation is heterogeneous and when it is beneficial to do so. A member has lithic characteristics distinguishing it from adjacent parts of the formation.

2. Definition of geochronologic terms

Geologists' stratigraphic nomenclature also includes geochronologic units. These are divisions of time traditionally distinguished by bodies of rock with synchronous boundaries (NACSN, Articles 66 and 80). Geochronologic terms used include eon, era, period, epoch, and age. Geochronologic epochs may be modified with

the adjectives Early, Middle, and Late (NACSN, Article 82). Capital letters indicate formal definition of time, whereas lower case, as in 'late Wisconsin', indicate informal use and lack of a formal definition. Figure 4a illustrates the temporal position of the late Wisconsin.

3. Definition of diachronic terms

Another category of stratigraphic terms, diachronic terms, is used when discussing the time during which the glacier produced specific stratigraphic units or an assemblage of units. Attig, Clayton, and Mickelson (1985) use event-stratigraphic units to associate landforms with ice advances that deposited specific lithostratigraphic units. These event-stratigraphic units are not recognized by the NACSN, but closely resemble the NACSN's diachronic units. Simultaneous use of lithostratigraphic, event-stratigraphic or diachronic, and geochronologic names confuses users and complicates the nomenclature. However, it also reduces confusion caused by revisions of the nomenclature when the same name (e.g., 'Cary' or 'Valders') is used for a lithostratigraphic unit, an interval of time, and the ice advance that deposited it (Attig, personal communication, 1987).

The nomenclature of diachronic units includes the terms episode and phase, with phase being subordinate in the hierarchy to episode (NACSN, Articles 91-95). Geographic names previously used for "geochronologic" units may be used for diachronic units only if the geochronologic use has been formally abandoned (NACSN, 1983, p. 871).

GEOCHRONOLOGIC					DIACI	IRONIC
Era	Period	Epoch	Age	Subdivision of age (10 ³ years ago) F&P R&F	Episode	Phase <u>∻</u>
		HOLOGENE				
		₩.	WISCONSIN	10 late 10	WISCONSIN	See figure 4b
GENOZOIC	QUATERNARY	PLEISTOCENE	SANGAMONIAN	_130 132	SANGAMON	
0			ILLINOIAN			

Figure 4a. Time-stratigraphic terminology. The late Wisconsin spanned the time from 10,000 b. p. to 23,000 b. p. (Fulton and Prest, 1987) or to 35,000 b. p. (Richmond and Fullerton, 1986). Informal stratigraphic units frequently have differing interpretations. Modified from Fulton and Prest, 1987 and Richmond and Fullerton, 1986.

Thus, the time when the Lake Michigan Lobe advanced to deposit the Cary Moraine in Illinois is now properly called the Cary phase (as used by Hansel et al., 1985). Of all the tills described by Thwaites (1943) and Thwaites and Bertrand (1957) as being of Cary age, only the Oak Creek Formation is now (informally) associated with the Cary phase. Willman and Frye (1970) formally abandoned the geochronologic use of "Cary". Figure 4b provides the diachronic terms associated with late Wisconsin-aged glacial events in eastern Wisconsin.

- B. History of stratigraphic nomenclature in eastern Wisconsin Previous authors have classified the late Wisconsin-aged glacial sediments in eastern Wisconsin into five formations. Table 2 synthesizes some of the stratigraphic nomenclature found in the literature predating Pleistocene Lithostratigraphic Units in Wisconsin (Mickelson et al., 1984). Observations made during earlier investigations should not be discounted because the terminology used is not up-to-date. Figure 5 is intended to improve the transition from past terminology to the present names.
- C. The late Wisconsin lithostratigraphic framework in eastern Wisconsin

1. Introduction

The Zenda, Horicon, New Berlin, Oak Creek, and Kewaunee

Formations include sediments of late Wisconsin age in eastern

Wisconsin. They are heterogenous units containing a variety of ice-

GREEN BAY LOBE West Side	GREEN BAY LOBE East Side	LAKE MICHIGAN LOBE
Kewaunee Fm.	Kewaunee Fm.	Kewaunee Fm.
Middle Inlet M. (Late Athelstane phase)	Glenmore M. (Denmark phase)	Two Rivers M. (Two Rivers advance)
		- Two Creeks Forest Bed (Two Creeks retreat)
		Valders M. (Inner Port Huron advance)
Kirby Lake M. (Early Athelstane phase)	Chilton M.	Haven M. (Inner Port Huron advance)
Silver Cliff M. (Early Athelstane phase)	Branch River M.	Ozaukee M. (Outer Port Huron advance)
Horicon Fm.	Horicon Fm.	Oak Creek Fm. (Cary advance)
Mapleview M.	Liberty Grove M.	New Berlin Fm.
(Häncock phase)		Zenda Fm. Tiskilwa M.

Figure 4b. Lithostratigraphic framework of the study area with associated diachronic or event-stratigraphic phase names in parentheses. Phase names for the west side of the Green Bay Lobe are from Attig, Clayton, and Mickelson, 1985; these supercede phase names in McCartney, 1983. Phase names for the east side of the Green Bay Lobe have not been established except for McCartney's (1983) use of 'Denmark phase'. Phase names in the Lake Michigan Lobe are from Hansel et al., 1985 and are based on stratigraphic position and geomorphic evidence. At the time of writing, these have not been verified with field work in Wisconsin. McCartney and Mickelson (1982) correlated the Two Creeks Forest Bed across the Green Bay lobe.

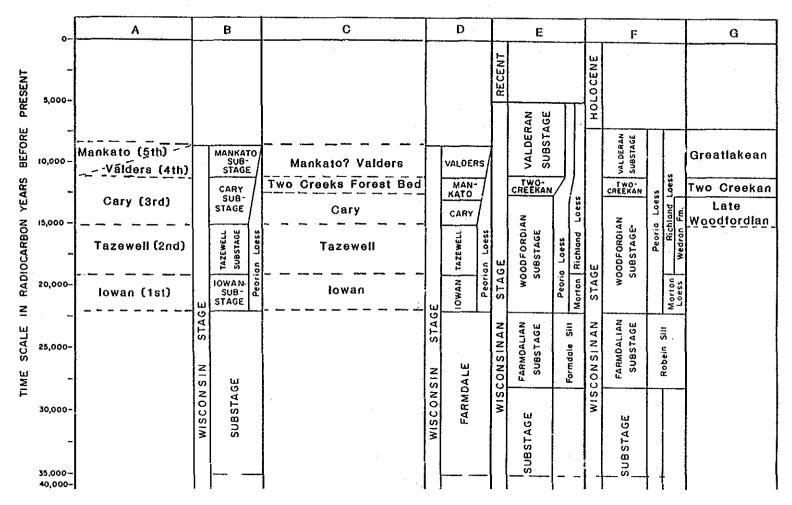


Figure 5. Equivalent time-related stratigraphic names. A: Thwaites, 1943. B: Leighton and Willman, 1950. C: Thwaites and Bertrand, 1957. D: Leighton, 1957. E: Frye and Willman, 1960. F: Willman and Frye, 1970. G: Acomb, Mickelson, and Evenson, 1982. After Frye and Willman, 1970, p. 123.

deposited (till), water-deposited (lacustrine or fluvial), or airdeposited (aeolian) sediments. The tills within the formations are
more easily distinguished—using lithic criteria as stipulated by the
NACSN's code—than the lacustrine and fluvial sediments that in many
places separate them. Very similar lacustrine and fluvial sediments
may occur repeatedly within a given stratigraphic sequence because the
glacial lobes advanced into proglacial lakes, deposited till, and
ablated into pro— and post glacial lakes. Eventually, as the study of
these sediments continues and more subsurface stratigraphy is mapped,
geologists may define lithostratigraphic members composed primarily of
lacustrine and fluvial sediments.

This report summarizes late Wisconsin geologic history for the Green Bay and Lake Michigan Lobes. As Boulton and Paul (1976) write, "It seems axiomatic that the geotechnical properties of sediments should be related to their source, their mode of transport, and their mode of deposition" (p. 159). Papers by Hansel et al. (1985), McCartney and Mickelson (1982), Acomb, Mickelson, and Evenson (1982), Schneider and Need (1985), and Attig, Clayton, and Mickelson (1985) give a more detailed review of the relevant geology and complete references. The following narration collects the main features of the literature into an overview so that the sediments at a particular site can be more easily anticipated.

2. Zenda Formation

Of the five late Wisconsin formations, the Zenda Formation is the oldest. The Harvard Sublobe of the Lake Michigan Lobe deposited the

Tiskilwa Member of the Zenda Formation between 18,000 to 20,000 years ago. This pinkish-tan sandy till is associated with the Wedron Formation and the Marengo moraine in Illinois (Mickelson et al., 1984, p. A6-6), but it is mapped at the surface only in the extreme south-central portion of Walworth County in Wisconsin. It is present at least as far north as Milwaukee in the subsurface. No glacial sediments in the Green Bay Lobe have been formally correlated with the Zenda Formation; burial of the Zenda Formation by younger sediments complicates such correlation.

3. New Berlin Formation

The second-oldest late Wisconsin formations are the Horicon Formation, deposited by the Green Bay Lobe approximately 14,000 to 18,000 years ago, and the New Berlin Formation, deposited by the Delavan Sublobe of the Lake Michigan Lobe approximately 14,000 to 18,000 years ago. The Kettle Moraine was formed when the two ice lobes abutted against each other and discharged fluvial sand and gravel (outwash) over blocks of ice that later melted.

Two till units, one superposed on the other, can be recognized in the New Berlin Formation that outcrops in Lake Michigan shoreline bluffs, but these have not been mapped or traced in the subsurface individually. The New Berlin Formation has not been studied extensively or subdivided into formal lithostratigraphic members.

Till in the formation has been described as gravelly sandy loam till of brown to yellowish brown color or gray color when unoxidized. Sand and gravel outwash underlies the till strata in the type and reference

sections. The formation has been mapped at the land surface behind the Darien Moraine and between the Kettle Moraine and the Valparaiso Moraine (Mickelson et al., 1984, p. A7-3).

4. Horicon Formation

The Horicon Formation includes three named lithostratigraphic members, the Mapleview, the Wayside, and the Liberty Grove Members.

Till in the Horicon Formation have been described as brown to reddish-brown cobbly, pebbly, silty sand (Mapleview Member) and as light brown to yellowish brown pebbly sandy loam (Liberty Grove Member) (Mickelson et al., 1984, p. A9-1). Each of these members was defined in the northernmost part of the Green Bay Lobe but the members have not been delimited. No lithostratigraphic members have been defined in the formation's southern extent. The moraines mapped by Alden (1918, Plates XXXVI and XXIII) indicate that separate till units may exist south of Lake Winnebago. The Hancock Moraine forms the Horicon Formation's western boundary (Attig, Clayton, and Mickelson, 1985).

Prior to 1970, the Horicon Formation was known as drift of Cary age, or 'Cary drift'.

5. Oak Creek Formation

Deposition of the Horicon Formation coincides with deposition of the Oak Creek Formation in the Lake Michigan Lobe 14,000 to 12,500 years ago (Mickelson et al., 1984, p. A8-3). Members of the Oak Creek Formation have been informally called the "Valparaiso," "Tinley," and "Lake Border" (Rodenbeck et al., 1987) and "2A, 2B, and 2C" (Mickelson et al., 1984). These preliminary designations are based on

lithic characteristics and are associated with minor readvances of the retreating ("Cary advance" in Hansel et al., 1985) ice that formed the Valparaiso, Tinley, and Lake Border Moraines. Tills in the Oak Creek Formation are silty because the ice overrode gray, silty lake sediments of Glacial Lake Milwaukee (Schneider and Need, 1985). In places, silty lake sediments separate the till units in the Oak Creek Formation.

Following deposition of the Oak Creek and Horicon Formations, both the Green Bay and Lake Michigan Lobes wasted back to the north beyond the Straits of Mackinac. Lake levels fell as the glacier retreated and Lake Superior, with its modern outlet blocked by ice, drained through a channel across the upper peninsula of Michigan and into the Lake Michigan Basin (Hansel et al., 1985). This glacial retreat was temporary, and both lobes of the glacier again advanced down the Lake Michigan Basin and the Green Bay Lowland.

6. Kewaunee Formation

This Early Port Huron advance incorporated the finer grained, red sediment that had been carried into these basins from iron-rich glacial sediments in the Lake Superior Basin (Murray, 1953). The Kewaunee Formation, described in a very general way as having red, clayey tills, includes ten lithostratigraphic members consisting primarily of till (figure 4b). McCartney and Mickelson (1982) use the Fox River as an arbitrary dividing line between the lithostratigraphic members on the east and west sides of the Green Bay Lobe; Kewaunee Formation tills on the east and west sides have distinct lithic

properties because the bedrock, which the glacier eroded as it advanced, outcrops in a pattern nearly parallel to the axis of the Green Bay Lobe. On the east side, ice of the Green Bay Lobe overrode the Maquoketa Formation of Ordovician age and dolomites of the Silurian System. On the west side, ice of the Green Bay Lobe eroded the Sinnippee, Ancell, and Prairie du Chien Groups of Ordovician age, Cambrian sandstones, and igneous rocks of the Middle Proterozoic Wolf River Batholith (Mudrey, Brown, and Greenberg, 1982).

The Ozaukee Member, stratigraphically the lowest Kewaunee

Formation till in the Lake Michigan Basin, has been estimated as

12,900 years old (Mickelson et al., 1984, p. A10-4). In the Green Bay

Lobe, the lowermost Kewaunee Formation tills are included in the

Silver Cliff Member on the west side and the Branch River Member on

the east side. No radiocarbon dates are available and no member-to
member contacts have been observed, so the estimated age of greater

than 12,200 years before present (b.p.) is by correlation of

stratigraphic position and geomorphology (McCartney and Mickelson,

1982). The Silver Cliff Member is bounded by the Early Athelstane

Moraine to the west (Attig, Clayton, and Mickelson, 1985). The Branch

River Member has been assumed to extend as far south as Alden's (1918)

"Outer Moraine of Red Drift."

After deposition of the first red tills, both lobes retreated at least as far north as Algoma (Acomb, Mickelson, and Evenson, 1982) before readvancing and depositing a second red till. In the Lake Michigan Lobe, the Haven Member overlies silty glacial Lake Chicago

sediments and/or the Ozaukee Member. In the Green Bay Lobe, ice deposited the tills of the Chilton and Kirby Lake Members of the east and west sides of the Fox River, respectively. Sediment from a proglacial lake, Early Lake Oshkosh (Thwaites and Bertrand, 1957), in places separates the first and second tills of the Kewaunee Formation in the Green Bay Lowland. A third till was deposited by the Lake Michigan Lobe, and is included in the Valders Member. The Valders and Chilton Members form an interlobate boundary west of the late Woodfordian interlobate moraine, the Kettle Moraine (McCartney and Mickelson, 1982).

Roughly 12,000 years ago, ice again withdrew north of the Lake Michigan Basin and lake levels fell below the modern level. Water again entered the Lake Michigan Basin from the Lake Superior Basin across the upper peninsula of Michigan, bringing more red, finegrained sediments. The boreal Two Creeks Forest grew during the time of this low lake level only to be drowned by the rise to Calumet level and buried in Lake Chicago sediments (Hansel et al., 1985). The next ice advance (11,800 to 11,200 years b. p.) flattened the forest and deposited the uppermost Kewaunee Formation members in the Green Bay Lowland and Lake Michigan Basin: the Middle Inlet, Glenmore, and Two Rivers Members. The southern extents of the Two Rivers Member, the Glenmore Member, and the Middle Inlet Member are marked by the Two Rivers, the Denmark, and the Late Athelstane moraines, respectively (Evenson and Mickelson, 1974; Attig, Clayton, and Mickelson, 1985).

Later Lake Oshkosh, at the margin of the Greatlakean-age ice in

the Green Bay Lowland, fell from an elevation of 829 feet. Apparently the ice margin was very jagged, and the lakes that formed at various elevations did not have sufficiently stable levels for mappable beaches to develop (Thwaites, 1943, p. 139). Lake levels fell from the time of Greatlakean ice retreat until the Nipissing I (4,500 b. p.) and later lake phases (Hansel et al., 1985).

7. Importance of the Pleistocene history and stratigraphy

An understanding of the geologic setting and the variability possible is necessary to understand the potential variability in geotechnical properties (May and Thomson, 1978, p. 362). The proglacial and postglacial ice marginal lakes described by Quigley (1980) in Ontario may be very similar to Thwaites' Early Lake Oshkosh and Lake Oconto. Quigley (1980) describes glaciolacustrine facies including ice-contact deltas, fluvial or turbidite sands and gravels or clays in ice-proximal areas to thick, massive clays in distal regions (p. 266). Since Thwaites' mapping, additional buried beaches have been discovered in the area glaciated by the Green Bay Lobe (Gordon and Huebner, 1984).

A. Application of lithostratigraphy

My interpretation and analysis of geotechnical data is based on the lithostratigraphic framework described in the preceding section. I associated the geotechnical and hydrogeologic properties compiled from geotechnical reports with the defined lithostratigraphic units. I interpreted the stratigraphy of the individual sites using stratigraphic investigations conducted at a reconnaissance level (McCartney, 1979; Need, 1985; Acomb, 1978) in conjunction with stratigraphic interpretation and geologic mapping of Wisconsin's Lake Michigan bluffs (Mickelson et al., 1977). Detailed geologic mapping has not been attempted over most of the area glaciated by the Green Bay and Lake Michigan Lobes in late Wisconsin time; recent reports on Brown County (Need, 1985), Florence County (Clayton, 1986), and Portage County (Clayton, 1986) are notable exceptions.

One convention established by Mickelson et al. (1984) is to associate facies other than till with a named lithostratigraphic member. For example, "the Valders Member contains basal glacial till deposited by ice of the Lake Michigan Lobe and associated fluvial and lacustrine deposits" (p. A10-8). To be included in one lithostratigraphic member, all of the facies must be clearly lithologically associated with each of the others (Mickelson et al., 1984, p. 3).

The boring logs that I used were not always written by geologists and frequently did not include the lithic criteria (e.g., mineralogy) necessary to distinguish one fluvial or lacustrine sediment from another. I made three assumptions: Mickelson et al.'s (1984) descriptions of tills in lithostratigraphic members are 1) accurate, 2) complete, and 3) the extent of the stratigraphic units is closely approximated by figure 6. Then I expected to find the mapped unit from the land surface to variable depths, underlain by a possibly discontinuous fluvial and/or a lacustrine layer of sediment, in turn underlain by the next lower lithostratigraphic member (including a till) in the stratigraphic section, and so forth. To some extent, my expectations were based on glacio-depositional models like those in Clayton and Moran (1974) and Boulton and Paul (1976), but consideration of local constraints (e.g., mapped distribution, topography) and my observations of modern glacial processes in Alaska influenced my interpretation more than the generic models. The buried glacial geomorphology produced by repeated ice advances (White, 1974) and other disruptions of bedding, such as involutions (Mickelson and Evenson, 1974) and glaciotectonic structures (Moran, 1971) frequently complicated stratigraphic interpretation.

B. USDA Soil Conservation Service county reports

I did not find published Soil Conservation Service reports consistently helpful for distinguishing lithostratigraphic members within a formation. The Soil Conservation Service map units are

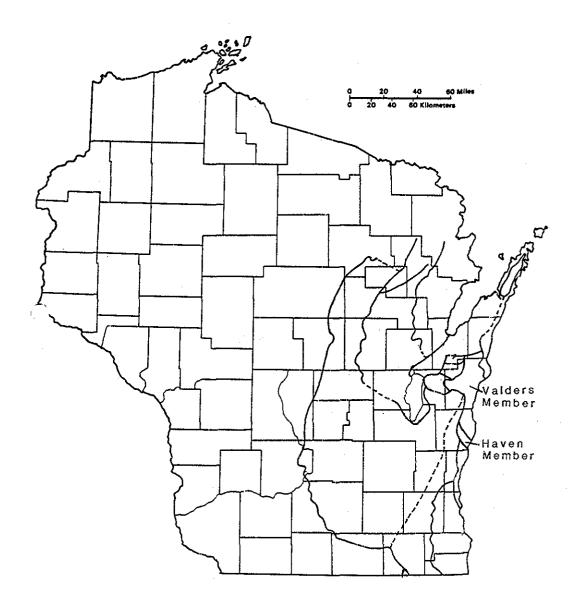


Figure 6. Surface distribution of named lithostratigraphic units of late Wisconsin age. (From Mickelson et al., 1984.) This map differs from Plate 1 by showing surface distribution of the Haven Member farther south than the Valders Member.

influenced by climate, living organisms, relief, parent material, and time. In other words, the factor pertinent to this study is combined with other factors in the determination of soils mapping units. As a result, the same soils mapping units may form on different lithostratigraphic members.

C. Geotechnical reports submitted in accord with Administrative Code

1. The influence of Wisconsin Administrative Code

The quality and quantity of data suitable for this study is strongly affected by the legal requirements for geotechnical information in the Wisconsin Administrative Code. Some reports of geotechnical investigations for proposed landfills prior to 1980 exceeded the minimum data requirements of Chapters NR 51 (1969) and NR 151 (1971). These early codes required investigations to a depth of only 10 feet below proposed base grade (revised to 15 feet) and did not stipulate a minimum number of borings or specific tests until a 1976 revision. NR 180 (1980) requires a minimum number of borings per area with descriptive boring logs, grain size analyses, permeability tests, and raw data in appendices. Data from geotechnical investigations prior to 1980 were included in the database of this report if the data resulted from standard engineering practices commensurable with those of post-1980 investigations. The availability and quantity of geotechnical information is expected to improve with the promulgation of NR 510 and NR 512; these will replace

NR 180.13 (5) and NR 180.13 (6), respectively. Excerpts from the Wisconsin Administrative Codes dealing with geotechnical investigations for landfills are included in an appendix to this report, "Data required by Wisconsin Administrative Code."

2. Compilation of information required by NR 180

i. Method of compiling data

Compilation of data submitted by consulting firms in individual reports and correspondence required considerable effort. A single site might have ten reports of geotechnical investigations by different consulting firms, each with a slightly different style of data presentation. The amount of suitable data varied with individual histories of site development and expansion. I compiled the data by hand and supervised its entry to a microcomputer spreadsheet.

ii. Quality and selection of data compiled

Early in the project, several individuals suggested that I eliminate reports by firms with reputations for poor quality work. I did not eliminate any firm's data because the apparent quality of all the reports varied with time, personnel, and circumstances. Moreover, I could not always distinguish between poor quality investigations and written reports of poor quality. Some "wild" data were "eliminated" by the resistant statistical techniques used; these techniques are described later in this report.

The emphasis in this report is on assessment of in-situ characteristics of stratigraphic units. For this reason, I did not

compile lab hydraulic conductivities for samples identified as recompacted. I carefully reviewed field hydraulic conductivities and well construction diagrams, then recorded field hydraulic conductivities. If the well screen intersected two materials, I assigned codes indicating that two materials (facies) were present within the saturated interval tested. Hydraulic conductivities for multiple facies are not included in comparisons of tills in lithostratigraphic members.

D. Associating data with a lithostratigraphic unit.

Several difficulties complicated the process of associating geotechnical data with Pleistocene lithostratigraphy. These difficulties include: 1) the confusing and complex stratigraphic nomenclature, 2) the difference in approaches taken by geologists and engineers, 3) distinction of till from other sediment facies, 4) identification of till units, 5) "incompatible" scales and maps. Despite these problems, Pleistocene lithostratigraphy provides a reasonable framework for data organization. Resolution of these problems is described below.

1. Stratigraphic nomenclature

As demonstrated in part II, the late Wisconsin stratigraphic names are numerous and confusing. Using the most detailed information available requires knowledge of the variety of names and what the materials have most recently been called. Associating the engineering information with glacial lithostratigraphic units requires familiarity

with the units both in the literature and in the field. I visited type or reference sections to obtain a better understanding of the literature.

2. The different approaches taken by engineers and geologists

It seemed as though the information in the boring logs was collected for a purpose other than definition of soil, bedrock, and groundwater conditions (hydrogeology) at the site. This is due to the difference in professional orientation between geotechnical engineers and geologists. Although Terzaghi, the father of soil mechanics, emphasized the effects of sedimentation, erosion, weathering, jointing, and groundwater flow (Dixon, 1974, p. 234), the boring logs produced by geotechnical consulting firms that are included in initial site reports and feasibility reports seem to emphasize the soil mechanics approximations of strength. To a large extent, this is a matter of presentation. Hydrogeologists prefer to see all test results and geologic interpretation on a boring log. A geotechnical consulting firm, on the other hand, may wish to present boring logs completed by a subcontractor separately (in an appendix) from the geologic interpretation (which is usually in the text).

3. Distinction of till from other sedimentary facies

Most geologists who study Quaternary materials rely on field and laboratory evidence to determine whether a sediment is till or sediment of a different facies. Dreimanis (1976) lists five criteria commonly emphasized in the identification of till:

". . . (1) glacial origin; (2) presence of a variety of rock and mineral fragments of various sizes, many of them having been

transported considerable distances; (3) poor sorting, in the geologic meaning of this term, that is: presence of a wide range of particle sizes, usually with bi-modal or multi-modal distribution; (4) lack of stratification, although some tills are foliated, or even truly bedded; (5) compactness or close packing, also with certain exceptions" (p. 14).

Even with good field exposures, the interpretation is open to professional dispute, largely because of the varying definitions of till (see Dreimanis, 1976). The techniques used by geologists to distinguish individual till units have varied to accommodate the lithostratigraphy being studied, and the criteria pertinent to this study have been summarized in table 1. (Other techniques may be found in Raukas, Mickelson, and Dreimanis, 1978.) Within each of the Kewaunee Formation members, I relied on grain size analysis and sorting to determine whether a material was till (poorly sorted), or lacustrine or fluvial (well sorted). Distinguishing till from outwash in the very sandy Horicon Formation was nearly impossible if a complete grain size analysis was not available (i.e., if the grain size analysis was completed only to P200, 0.075 mm). If the genesis of a sediment could not be determined from the information available, it was coded as unknown.

4. Identification of lithostratigraphic units

Distinction of tills in members of the Kewaunee Formation presents another difficulty because the tills have similar provenance. Distinctions between lithostratigraphic members of the Kewaunee Formation were made on the basis of description (including qualitative color changes noted on the log and grain size analysis), mapped location, and stratigraphic sequence. If sediments clearly belonged

within a formation, but could not be confidently identified at the member level, no member code was entered. If not even the formation could be identified, or if the sediment did not fit within a formation's defined range of lithic characteristics, a code of UN for unknown/unnamed was assigned. The sites with sediments that did not fit the expected lithostratigraphic framework are useful for identification of areas requiring further geologic study. Some excellent logs included observations on mineralogy, depth of leaching, or fabric and structure of the samples that were very helpful.

5. "Incompatible" maps and scales

The next difficulty in assigning data to a lithostratigraphic unit has to do with scale. Little detailed mapping of late Wisconsin glacial sediments has been completed in the Green Bay and Lake Michigan Lobes. Thesis (McCartney, 1979) and journal illustrations and two 1:1,000,000 maps of Quaternary sediments and glacial landforms (Lineback et al., 1983; Farrand et al., 1984) were used to determine a preliminary, theoretical stratigraphic section at a site.

Incompatible map bases (lack of common political and hydrographic features or coordinate systems) complicated map—to—map comparisons.

The geotechnical boring locations are plotted at a relatively large scale for submittal, on the order of 1 inch equals 200 feet. These boring locations were transferred to 7 1/2 minute topographic quadrangle maps so that the boring locations could be seen in a more regional geomorphic context.

E. The spreadsheet

Data from handwritten summary sheets were entered to a microcomputer spreadsheet for ease of manipulation. Table 2 gives the spreadsheet headings and subheadings used, and table 3 lists the codes. The spreadsheet allowed relatively easy sorting and combining of data into files of single parameters, such as lab or field hydraulic conductivity, or single lithostratigraphic units.

F. Spatial locations

The data collected for this study have been assigned spatial locations so that the data are suitable for entry to a geographic information system and may be combined with data from other sources. Reconciliation of the spatial location of all data points to a single system provided a difficult problem in the assembly of a large database from diverse sources. Engineering site plans usually record precise spatial locations, but these locations are frequently tied to arbitrary bench marks. In fact, the current administrative code, NR 180, requires site specific grid coordinates and the use of local benchmarks. Although this does not preclude use of a real space coordinate system such as universal transverse mercator, latitude and longitude, or public land survey system (township and range) coordinates for each borehole, none of the submitted reports included coordinates of these types for each boring.

Geological investigations typically use information plotted on 15- or 7 1/2-minute topographic quadrangles. For this study, latitude

Identity:

County

Year sampled

Lithostratigraphic unit

Geologic genesis

Location:

Latitude (degrees, minutes, seconds) Longitude (degrees, minutes, seconds)

Boring number

Land surface elevation (feet above MSL) Top of interval sampled (depth in feet) Bottom of interval sampled (depth in feet)

Hydraulic conductivity: Lab K (cm/s)

Lab K method of test

Field K (cm/s)

Field K method of test

Grainsize percentages:

Percent of bulk > 2 mm

Sand percentage of matrix (< 2 mm) Silt percentage of matrix (< 2 mm) Clay percentage of matrix (< 2 mm)

Engineering properties:

USCS group symbols

P200 (%)

Dry unit weight (pcf) SPT N (blows/foot)

Natural moisture (% of dry weight)

Liquid limit (%) Plastic index (%)

Pocket penetrometer measurement (tsf)

Table 2. Categories of data recorded using the spreadsheet. symbolizes hydraulic conductivity. 'P200' means the percent passing the #200 sieve. 'SPT N' abbreviates standard penetration test blow counts.

Counties			Lithostratigraphic	: Units
Brown	BN		Middle Inlet M.	mi
Calumet	CA		Ozaukee M.	oz
Dane	DN		Silver Cliff M.	si
Dodge	DG		Two Rivers M.	tr
Door	DR		Valders M.	va
Fond du Lac	FL			
Green Lake	GL		Oak Creek Fm.	oc
Kenosha	KE			
Kewaune e	KW		Horicon Fm.	HO
Manitowoc	MN		Mapleview M.	ma
Marinette	MT		Liberty Grove M.	lg
Marquette	MQ			
Milwaukee	ML		New Berlin Fm.	NB .
Oconto	OC			
Outagamie	OU		Zenda Fm.	ZE
Ozaukee	OZ	:	Tiskilwa M.	ti
Racine	RA			•
Sauk	SK		Unnamed units	UN
Shawano	SH			
Sheboygan	SB			
Walworth	WW			
Washington	WN		Materials and genes	cie
Waupaca	WP .		Till (all varieties	
Winnebago	WI		Outwash (sand & gra	
			Lacustrine (sand, s	
			and/or clay)	5
			Loess	6
Test methods			Modern alluvium	7
for hydraulic conductivity			Rock	12
lab constant head (vert) 1			Organic	13
lab constant head (hor) 2			Undifferentiated	99
lab falling head (vert) 3				
lab falling head (hor) 4				
lab backpressure or				
consolidometer (vert) 5				
lab backpressure or				
consolidometer (hor) 6				
field rising head 7				
field falling head		8		
pumping test		9		
other		10		

Table 3. Codes used to identify spreadsheet data. Although codes for lithostratigraphic members appear in only lower case here, they may appear in upper or lower case in the appendices.

and longitude coordinates were chosen because these coordinates lend themselves to easy conversion to map projections such as universal transverse mercator, and they follow simple rules like increasing to the north and west. The seconds of latitude and longitude usually provide an adequate resolution of borehole locations' relative positions at individual landfill sites. Use of latitude and longitude avoids problems associated with the use of township and range such as irregular section shapes that resulted from influences of the original system of surveying.

Elevations must be reported relative to USGS datum according to Wisconsin Administrative Code (NR 180.13(6)). The datum was often missing from the documents predating the existing code. Although reports have improved in this respect, lack of datum elevations continues to be a problem.

G. Choice of analytical tool

Associating groups of material properties with mapped lithostratigraphic units in Wisconsin is a principal goal of this study. All the material properties recorded vary in three dimensions. Measurement error is associated with each observation of each parameter. The lack of control over how samples were chosen for testing controls the choice of data analysis tools. Many of our sample sizes are small and lack Gaussian distributions; resistant and robust exploratory statistical methods are necessary for confidence in study results. In order to assess the validity of statistical

assumptions that the sample is random, that it has a normal (Gaussian) distribution, and that all of the populations have equal variances, I used Minitab (Release 5.1.1, Minitab, Inc., 1986) statistical software.

Within each unit I constructed histograms of both field and lab \log_{10} hydraulic conductivities, P200 values, plastic and liquid limits, plastic index, pocket penetrometer measurements, and dry unit weights for each site. According to Ryan, Joiner, and Ryan (1985), "Observations taken in close proximity, either in time or in space, often are correlated. Observations that are correlated do not form a simple random sample" (p. 175). In some cases there were clear patterns from site to site within a single till unit; thus, the sample is not random. However, in most cases, no clear pattern was apparent and a random sample was assumed.

I used several methods to determine whether the data are normally distributed. These methods include comparison of median and mean, normal probability plots (Ryan, Joiner, and Ryan, p. 177), and visual assessment of histograms. Liquid limit, plastic limit, and dry unit weights typically have Gaussian or approximately Gaussian distributions. Values of P200, \log_{10} hydraulic conductivities, and pocket penetrometer measurements are not always Gaussian.

The assumption of equal variances between populations is important when choosing an analysis of variance (ANOVA) technique. Some of the samples are small (15 > n > 5), leading to relatively large standard deviations about the mean; when sample sizes are small

and have unequal variances, use of an ANOVA technique incorporating pooled standard deviations leads to an undesirable Type I error.

Previous workers have described the statistical distribution of hydraulic conductivity data. Freeze and Cherry (1979, p. 31) and Neumann (1983, p. 83), among others, indicate that hydraulic conductivity follows a log-normal distribution. The hydraulic conductivities included here more closely resemble a Gaussian distribution after a base 10 power transformation. But the medians and the means of the hydraulic conductivity data still do not always equal each other; some histograms show a skewed distribution. addition to the non-Gaussian distribution, the small sample sizes (fewer than 15 values) restrict the use of standard parametric statistical tests. Nonparametric techniques have the advantage of being resistant to the influence of a few outlying data points. In most cases, I used the Kruskal-Wallis test, ". . . a generalization of the Wilcoxon two-sample test to the case of k > 2 samples . . . the test is an alternative nonparametric procedure to the F test for testing the equality of means . . . " (p. 495, Walpole and Myers). The Kruskall-Wallis test assumes that the data form continuous distributions all having the same shape. The hypotheses are:

 H_O : k independent samples are from identical populations;

 \mathbf{H}_1 : there is at least one difference among the k independent samples.

If the test statistic h falls in the critical region ${\tt H} > {\tt X}^2$, ${\tt H}_{\tt O}$ may be

rejected at a level of significance determined from a statistical table. Otherwise, H_1 is rejected (Walpole and Myers, p. 496).

A nonparametric statistical technique—the boxplot—is well—suited for graphical analysis of data. A box and whisker plot gives more information than a histogram, but requires a minimum of 5 values. Figure 7 shows a median, the fourthspread (box), outerfourth ranges (whiskers), outliers, and the approximate 95% confidence interval (parentheses). The parentheses indicate the confidence interval of the median and are much more sensitive to changes in the data than the box. Batches (the exploratory data analysis equivalent of samples) of data may be compared using the values of the median, the fourth spread, the location of the median with respect to the fourths, whisker length, and outlying data points. Up to 25% of the data in each batch can be "wild" without greatly affecting the features of the box (Emerson and Strenio, 1983).

The methods just described are used to assess the variability and expected range of values for properties of tills within lithostratigraphic units. Other methods are appropriate for investigation of the underlying relationships among data compiled. If the compiled data are from a carefully designed experiment, inferences can be made from straight-line fits. The conditions for statistical inference follow.

[&]quot;1. In the underlying population, the relationship between x and y should be a straight line...."

[&]quot;2. For each x, the amount of variation in the population of ys in the population should be approximately the same..."

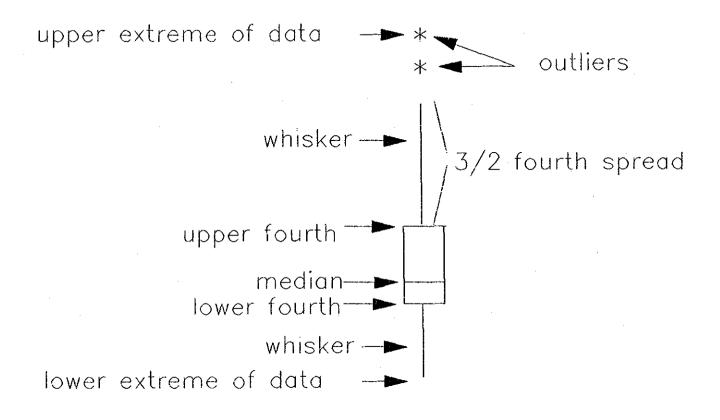


Figure 7. Features of the boxplot. This boxplot was drawn at an arbitrary scale. The fourth spread is the distance (or range of values) between the upper and lower fourths. Whiskers are drawn out to the data value most remote from the median within a distance evaluated as (3/2 * fourth spread). Confidence limits for the median may be added in the form of parentheses. See Hoaglin, Mosteller, and Tukey for a discussion of exploratory data analysis terminology (1983, pp. 1-6).

- "3. For each x, the distribution of ys in the population should be approximately normal...."
- "4. The ys that actually are obtained should be approximately independent..." (Ryan, Joiner, and Ryan, p. 230).

Frequently, only one type of data was available for a specific sample. The data compiled in this project were not always paired, and medians are used to represent individual till units. Thus, few inferences may be confidently made. Correlation and regression are used in this study to determine which tests are useful for hydrogeologic interpretation and to make recommendations for future investigations.

IV. Presentation of Data

A. Variation within tills of lithostratigraphic units

Data for materials other than till are not discussed here because the extent of these materials is not known. However, values of hydraulic conductivity for Pleistocene sand and gravel outwash in eastern Wisconsin are typically within an order of magnitude of 10⁻³ cm/s. Values of hydraulic conductivity measured in the field for silty lacustrine sediments are typically about 10⁻⁵ cm/s while rhythmites of silt and clay (commonly referred to as 'varved' lacustrine sediments) have lower values of hydraulic conductivity. Site-specific data for all materials at each site were included in appendices.

The following discussion of the variability of till units assumes that the stratigraphic and geologic interpretations are correct. Histograms of \log_{10} values of hydraulic conductivity measured in the field and in the laboratory were plotted for the till(s) of each lithostratigraphic unit. Matrix percentages of sand, silt, and clay are plotted in textural triangles. Plasticity charts illustrate the range in liquid limit and plastic index. Pocket penetrometer and dry unit weight data are not discussed until section IV B unless sufficient data were available for an analysis of variance test (ANOVA). The standard penetration test, USCS group symbols, plastic limits, and other indices derived from Atterberg limits will be presented only for discussion in part V.

Within some tills, no quantitative comparison of data may be made for one of two reasons: 1) insufficient data are available at each site for statistical analysis, or 2) data were collected for only one site. Data points are coded by site within each of the four diagrams for each unit. Refer to Plate 1 for the location of sites. County names and section, township, and range numbers are provided for the sites in an appendix. The site numbers are consistent throughout text, illustrations, and appendices.

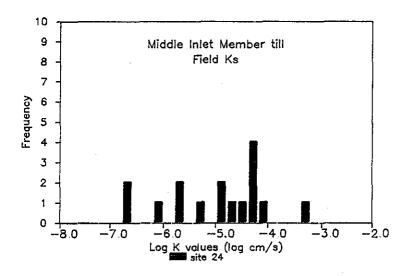
1. Kewaunee Formation

Figures 8a through 8h illustrate the hydraulic conductivities, grain size analyses, and plasticity charts for the tills in members of the Kewaunee Formation. Due to the geographic distribution of both the landfills and the Branch River Member, no data for the Branch River Member were recorded. Although some data for the Silver Cliff Member may have been recorded, I could not differentiate it from other Kewaunee Formation sediments.

a. Hydraulic conductivities measured in the field

In the Middle Inlet (figure 8a) and Kirby Lake (figure 8b)

Members on the west side of the Green Bay Lobe, field hydraulic conductivities have the widest range, varying over four orders of magnitude. Tills in other members may have an equal range, but data are too sparse to show it. Sufficient samples for the Kruskal-Wallis test were available in both the Kirby Lake and Glenmore Members (figure 8c). In the Glenmore Member, I rejected the null hypothesis that two independent samples, sites 1 and 10 (figure 8c), are from



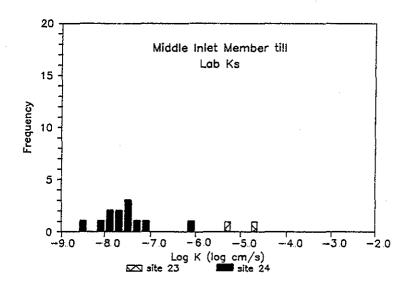
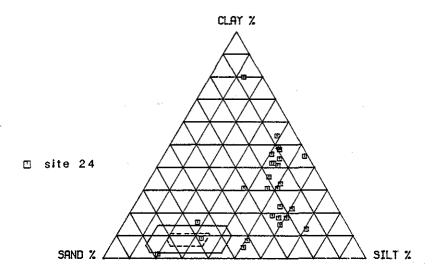


Figure 8a. Data for till in the Middle Inlet Member of the Kewaunee Formation. Field K means hydraulic conductivity measured in the field. Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.



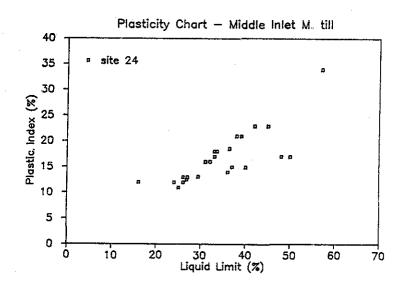
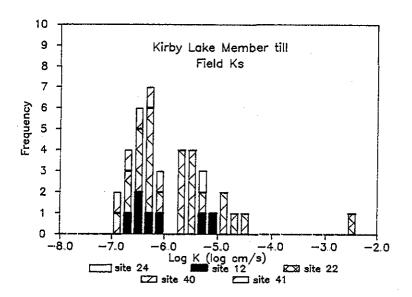


Figure 8a, cont. Data for till in the Middle Inlet Member of the Kewaunee Formation. Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the source.



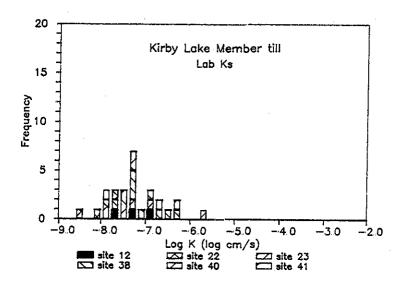
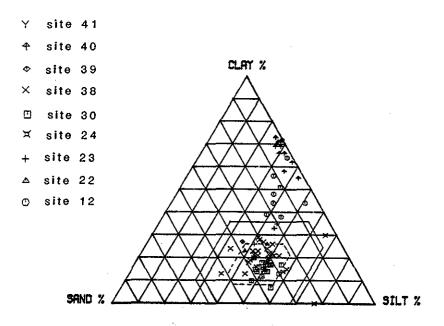


Figure 8b. Data for till in the Kirby Lake Member of the Kewaunee Formation. Field K means hydraulic conductivity measured in the field. Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.



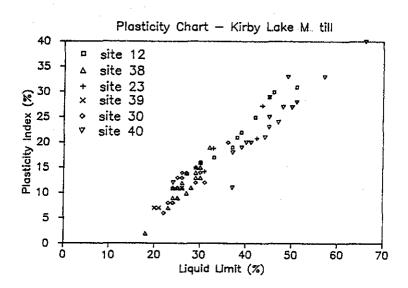
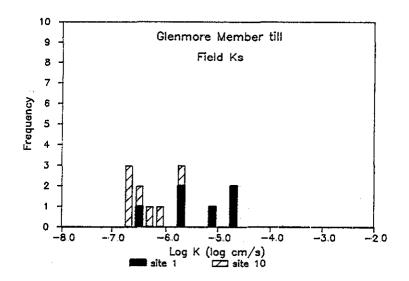


Figure 8b, cont. Data for till in the Kirby Lake Member of the Kewaunee Formation. Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the source.



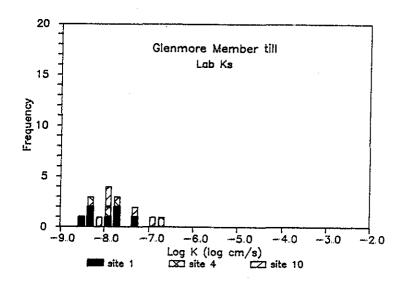
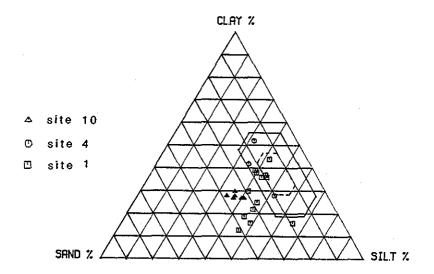


Figure 8c. Data for till in the Glenmore Member of the Kewaunee Formation. Field K means hydraulic conductivity measured in the field. Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.



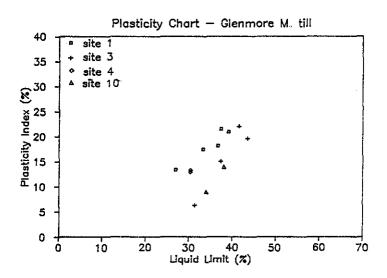
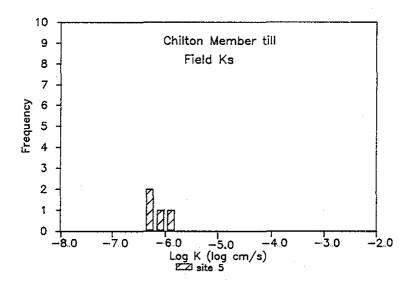


Figure 8c, cont. Data for till in the Glenmore Member of the Kewaunee Formation. Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the source.



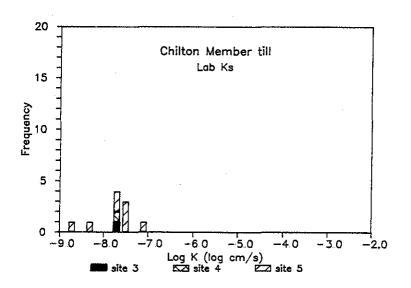
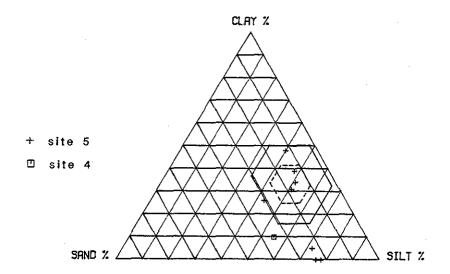


Figure 8d. Data for till in the Chilton Member of the Kewaunee Formation. Field K means hydraulic conductivity measured in the field. Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.



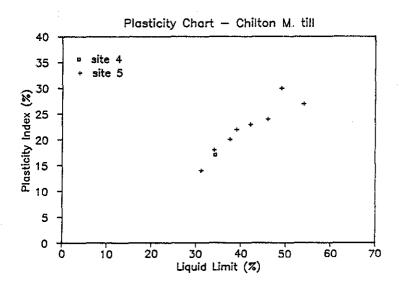


Figure 8d, cont. Data for till in the Chilton Member of the Kewaunee Formation. Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the site.

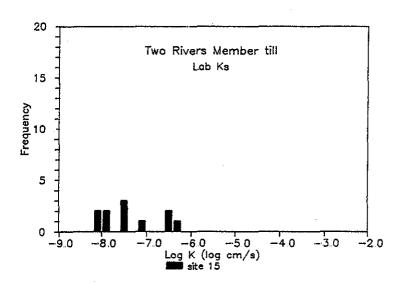


Figure 8e. Data for till in the Two Rivers Member of the Kewaunee Formation. No values of hydraulic conductivity measured in the field were compiled. Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.

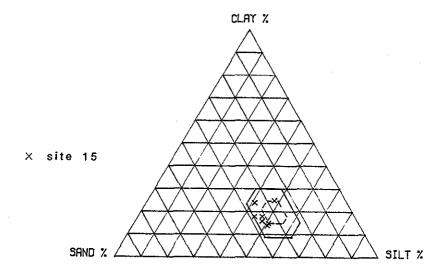


Figure 8e, cont. Data for till in the Two Rivers Member of the Kewaunee Formation. Sand, silt, and clay percentages are for the less than 2 mm fraction. No Atterberg limit data were compiled. Data are plotted with a symbol indicating the source.

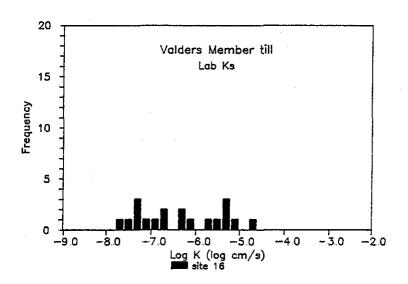
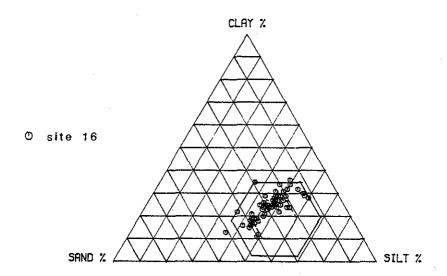


Figure 8f. Data for till in the Valders Member of the Kewaunee Formation. No values of hydraulic conductivity measured in the field were compiled. Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.



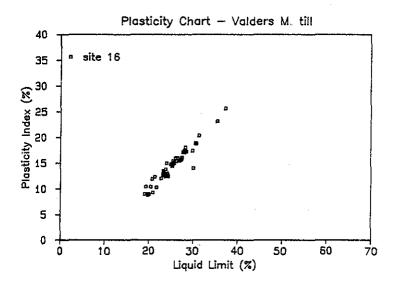
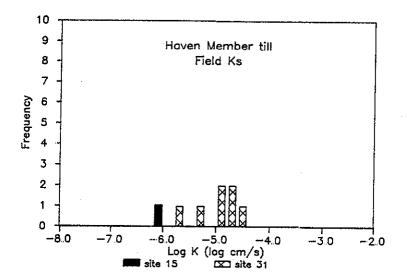


Figure 8f, cont. Data for till in the Valders Member of the Kewaunee Formation. Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the source.



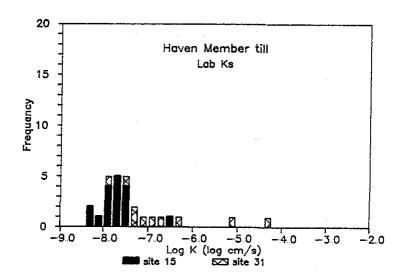
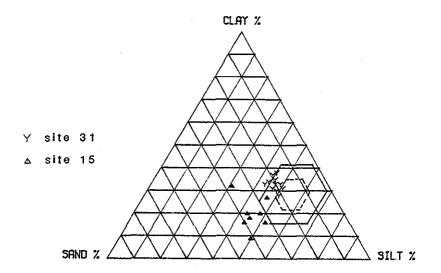


Figure 8g. Data for till in the Haven Member of the Kewaunee Formation. Field K means hydraulic conductivity measured in the field. Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.



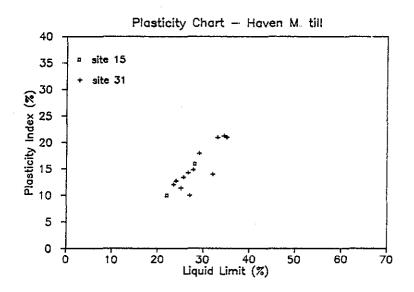


Figure 8g, cont. Data for till in the Haven Member of the Kewaunee Formation. Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the source.

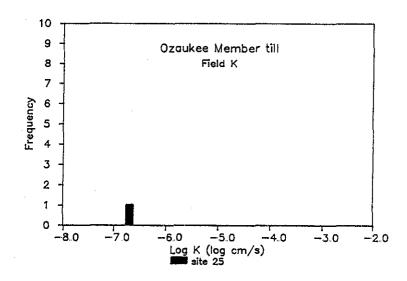
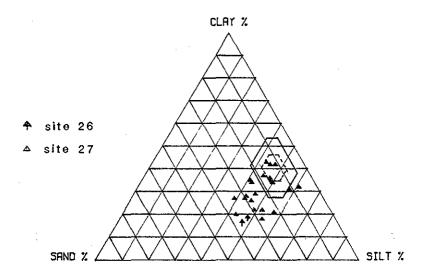


Figure 8h. Data for till in the Ozaukee Member of the Kewaunee Formation. Field K means hydraulic conductivity measured in the field. No values of hydraulic conductivity measured in the laboratory were compiled.



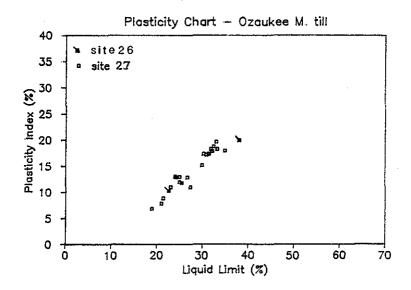


Figure 8h, cont. Data for till in the Ozaukee Member of the Kewaunee Formation. Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the source.

identical populations (Walpole and Myers, 1978, p. 495). There was insufficient evidence to reject the same null hypothesis in the Kirby Lake Member for sites 12, 40, and 41 (figure 8b).

b. Hydraulic conductivities measured in the laboratory

Values of hydraulic conductivity measured in the laboratory range over at least two orders of magnitude in the Kewaunee Formation tills, and range over four orders of magnitude in both the Middle Inlet (figure 8b) and Haven Members (figure 8g). Sufficient data are available in the Haven, Glenmore, and Kirby Lake Members for the Kruskal-Wallis test. I rejected the null hypothesis that two independent samples are from identical populations in the Haven (sites 15 and 31, figure 8g) and Kirby Lake Members (sites 38 and 40, figure 8a), but there was not sufficient evidence to reject the null hypothesis for the Glenmore Member (sites 1 and 10, figure 8c).

c. Textural triangles

I used statistical summaries from McCartney and Mickelson (1982) and Acomb, Mickelson, and Evenson (1982) to construct the envelopes drawn on the textural triangles. The dashed lines represent one standard deviation and the solid lines represent two standard deviations from a mean. The compiled data clearly do not always plot within the confidence levels for each unit determined by previous authors. This is conspicuously true for tills in the Kirby Lake (figure 8a), Middle Inlet (figure 8b), Glenmore (figure 8c), and Ozaukee (figure 8h) Members.

d. Plasticity charts

The plasticity charts illustrate consistent trends at individual sites within each unit. Tills tend to plot in a long cluster with a positive slope. I regressed plasticity index on liquid limit for sites 12, 30, 38, and 40 in the Kirby Lake Member (figure 8b). At these sites, approximately 95, 74, 86, and 84% of the variation in plasticity index was accounted for by a straight line regression equation with liquid limit. The regressed lines for sites 12 and 30 are nearly identical. The 95% confidence levels for all the lines overlap.

2. Oak Creek Formation

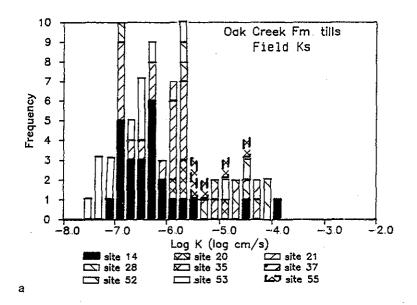
Data for tills of the Oak Creek Formation are summarized in figure 9.

a. Hydraulic conductivities measured in the field

Field hydraulic conductivities in the Oak Creek Formation range over four orders of magnitude, but at least two subgroups can be distinguished by looking carefully at the histogram (figure 9a). Sites 35, 37 and 55 have generally greater hydraulic conductivity than sites 14, 21 and 53, for example. An analysis of variance test at the 95% confidence level resulted in rejection of the null hypothesis that all site medians are equal.

b. Hydraulic conductivities measured in the laboratory

Hydraulic conductivities measured in the laboratory for samples of till from the Oak Creek Formation range over nearly three orders of magnitude, but subgroups are not as easily seen in the histogram (figure 9b) as for hydraulic conductivity measured in the field



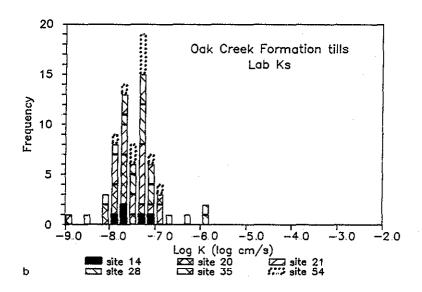
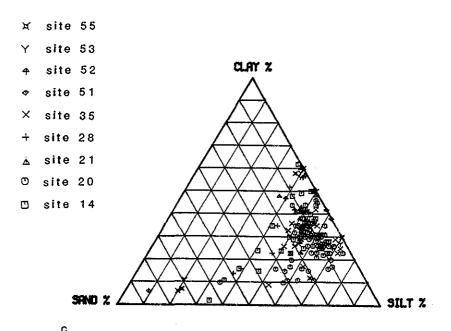


Figure 9. Data for till of the Oak Creek Formation. a) Field K means hydraulic conductivity measured in the field. b) Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.



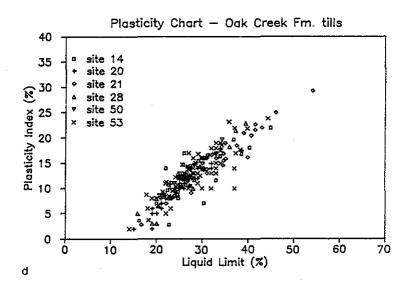


Figure 9, cont. Data for till of the Oak Creek Formation. c) Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the source.

(figure 9a). The results of an ANOVA test indicate that separate populations do exist, however. The null hypothesis that six independent samples (sites 14, 20, 21, 28, 35, and 54) are from the same population was rejected at a 99.5% confidence level.

c. Textural triangle

The particle size distribution of till in the Oak Creek Formation has not been statistically summarized, but "... the average composition is about 12 percent sand, 43 percent silt, and 45 percent clay ... The texture of the till ranges from silty clay through clay loam and silty clay loam to silt loam" (Mickelson and others, 1984, p. A8-2). The data in figure 9c exhibit a quite similar distribution (refer to figure 2 for textural terms). The numerous analyses from site 20 cover nearly the entire range.

d. Plasticity chart

The plasticity chart (figure 9d) shows that data for till from different sites in the Oak Creek Formation plot within the same cluster. I regressed plasticity index on liquid limit and plotted the least squares regression lines for sites 14, 21, 28, 35, 37, 50, 52, 53, and 54. At these sites, 59, 93, 94, 89, 69, 79, 96, 90, 98, and 89% of the variation in plasticity index was accounted for by a regressed straight line equation with liquid limit. The lines for sites 14, 52, 21, and 35 have lower slopes than the others, but all the lines cross one another between liquid limits of 20 and 45. They are not significantly different.

e. Pocket penetrometer

Pocket penetrometer measurements on Oak Creek Formation tills range over the entire discrete scale, from 0.5 to 4.5 tsf. Pocket penetrometer data are not presented graphically except for comparison between lithostratigraphic units in a later section; the data are discussed here because there are sufficient values to statistically analyze variation within the till unit. Measurements at sites 21 and 28 yield relatively low values, with medians of 2.5 and 2.6 tsf. Medians at the other sites are between 3.0 and 3.3 tsf. Site 31 has the highest median, 4.0 tsf. The Kruskal-Wallis ANOVA test (95% confidence) indicated that the medians at independent sites are not from the same population.

f. Dry unit weight

Dry unit weights range from 89.0 to 140.0 pcf in tills of the Oak Creek Formation. Dry unit weight data are not presented graphically except for comparison between lithostratigraphic units in a later section; the data are discussed here because there are sufficient values to statistically analyze variation within the till of the Oak Creek Formation. Median values at individual sites range from 115.0 to 120.8 pcf at sites with greater than 5 samples. A Kruskal-Wallis test at the 95% confidence level did not indicate that separate populations exist at sites 21, 28, 35, and 54.

3. Horicon Formation

Figure 10 includes graphical summaries of values of hydraulic conductivity, grain size analyses, and a plasticity chart for till of the Horicon Formation.

a. Hydraulic conductivities measured in the field

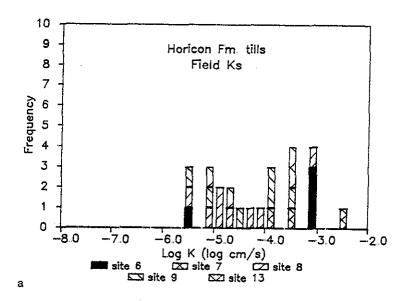
Field hydraulic conductivities range over three orders of magnitude (figure 10a). Nearly the entire range is present at sites 8 and 9. Sufficient data were available at these two sites for a Kruskal-Wallis ANOVA test. Insufficient data are available to reject the null hypothesis of equal medians at the two sites.

b. Hydraulic conductivities measured in the laboratory

Since the Horizon Formation till matrix is typically 60-80% sand (Mickelson et al., 1984, p. A9-2), the collection of an undisturbed sample for a laboratory hydraulic conductivity test is difficult. I suspect that the values of hydraulic conductivity measured in the laboratory for site 8 may be recompacted, molded samples unrepresentative of in-situ conditions (figure 10b). These samples are included here because they were not recorded as recompacted. Sites 8, 13, and 29 have five samples each, enough for a Kruskal-Wallis ANOVA test. The test resulted in a rejection of the null hypothesis of equal median hydraulic conductivity values at all sites.

c. Textural triangle

Relatively few analyses of till were completed to the clay size fraction (figure 10c). This lack of data results from the mandated



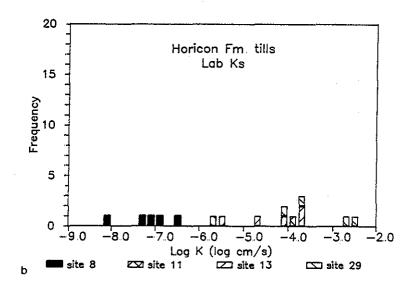
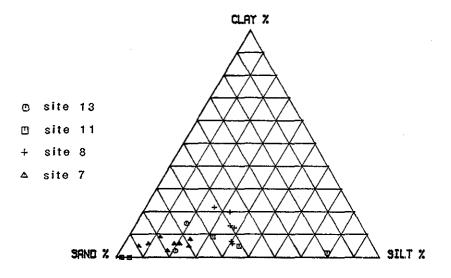


Figure 10. Data for till of the Horicon Formation. a) Field K means hydraulic conductivity measured in the field. b) Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.



¢

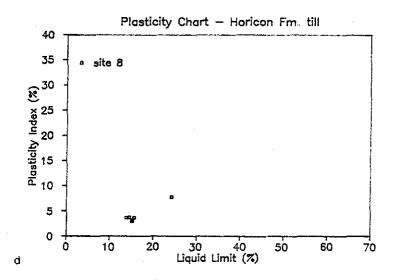


Figure 10, cont. Data for till of the Horicon Formation. c) Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the source.

use of the unified soil classification system (USCS). The dotted lines represent two standard deviations from sand, silt, and clay means determined by McCartney (1979, p. 11) for basal till in the Mapleview Member of the Horicon Formation. Statistical summaries are not available for the Liberty Grove Member, but the analyses at sites 7, 8, and 13 are similar texturally to the Mapleview Member.

d. Plasticity chart

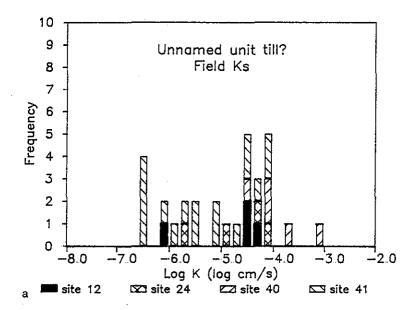
Few samples of Horicon till (figure 10d) are so fine-grained that completion of liquid limit and plastic limit tests and plotting on a plasticity chart is necessary for classification in the USCS. The samples with Atterberg limits plot in a small cluster with a lone point indicating the same general trend seen in other tills.

4. Unnamed unit

A material similar to till of the Horicon Formation but much siltier than the Mapleview and Liberty Grove Members was identified at several sites near Lake Winnebago. Figure 11 contains graphs of the data. This material may represent a member of the Horicon Formation. A geologic investigation is required to determine the nature of its occurrence.

a. Hydraulic conductivity measured in the field

The range of field hydraulic conductivity values measured in the field covers four orders of magnitude (figure 11a). Application of an ANOVA test to data from sites 40 and 41 resulted in rejection of the null hypothesis of equal medians at a 95% confidence level.



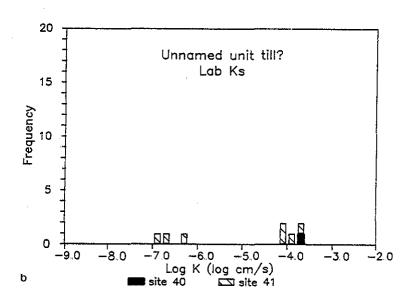
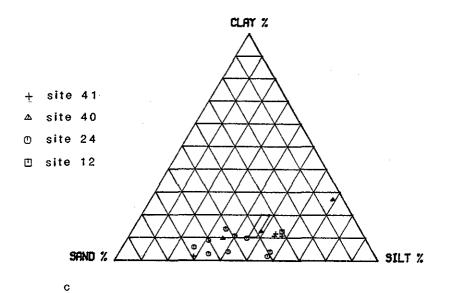


Figure 11. Data for an unnamed unit, possibly till of the Horicon Formation. a) Field K means hydraulic conductivity measured in the field. b) Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.



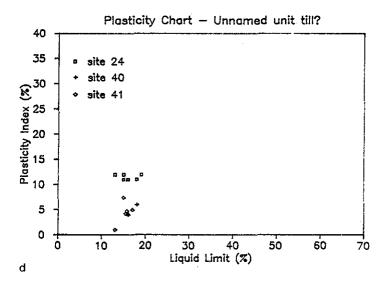


Figure 11, cont. Data for an unnamed unit, possibly till of the Horicon Formation. c) Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the source.

b. Hydraulic conductivity measured in the laboratory

The data here appear bimodal (figure 11b), and I again suspect that some of the hydraulic conductivity values measured in the laboratory may be for recompacted samples although they were not recorded as such.

c. Textural triangle

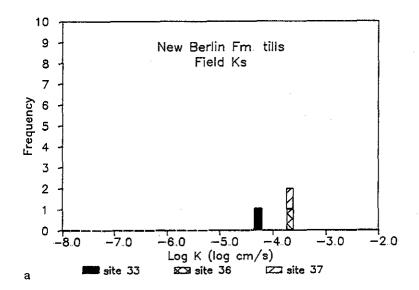
Textures for samples analyzed to 0.002 mm include sandy loam, loam, and silt loam (figure 11c). An envelope of texture for till of the Wayside Member of the Horicon Formation in Brown County described by Need (1985) is included for comparison.

d. Plasticity chart

The unnamed unit is roughly 30% stone (over 2 mm diameter) so that few samples have values of P200 greater than 50% by weight. Consequently, determination of Atterberg limits is not necessary for classification in the USCS. Data from sites 40 and 41 plot in the pattern expected for tills (figure 11d). Although the liquid limits at site 24 have the same range as sites 40 and 41, the data cluster separately.

5. New Berlin Formation

Few hydraulic conductivity data for till of the New Berlin Formation were compiled (figures 12a and 12b), and no statistical analysis of variation within the unit is possible. The particle size analyses compiled graph in a fairly tight cluster except for the Washington County sites (34 and 36, figure 12d).



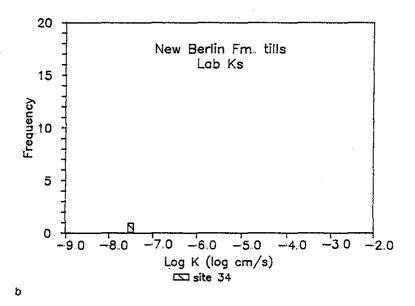
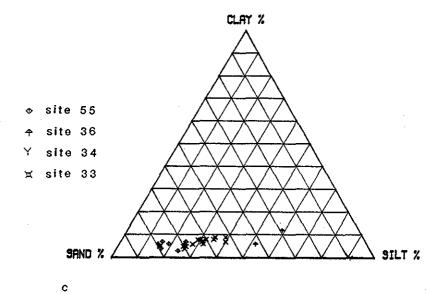


Figure 12. Data for till of the New Berlin Formation. a) Field K means hydraulic conductivity measured in the field. b) Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.



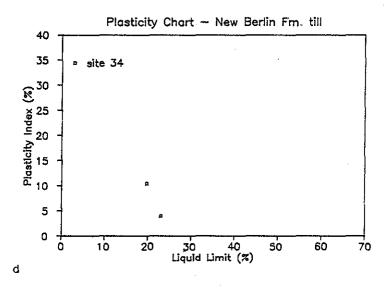


Figure 12, cont. Data for till of the New Berlin Formation. c) Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the site.

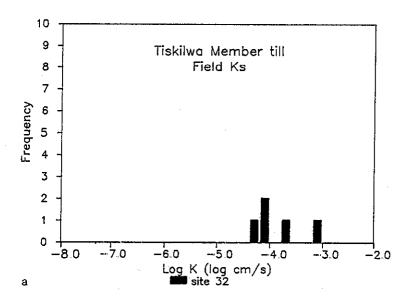
6. <u>Tiskilwa Member of the Zenda Formation</u>

Data for the Tiskilwa Member were collected from only one site in the Lake Michigan Lobe, so no analysis of variance within the member from one site to another is possible. The available data are summarized graphically in figure 13. Hydraulic conductivities measured in the field range over 1 1/2 orders of magnitude at site 32 (figure 13a). Only one value of hydraulic conductivity was measured in the laboratory for till of the Tiskilwa Member (figure 13b). On the plasticity chart, till of the Tiskilwa Member plots in an elongate cluster with positive slope (figure 13d).

- B. Variation between tills of lithostratigraphic units
- 1. Interunit comparisons of hydraulic conductivity measured in the field

a. The Green Bay Lobe

There is a statistically significant difference in hydraulic conductivity between till of the Middle Inlet and Kirby Lake Members of the Green Bay Lobe. I rejected the null hypothesis that the median log values of hydraulic conductivity measured in the field for till in the Middle Inlet Member and for till in the Kirby Lake Member are equal at the 99.5% confidence level. It is apparent from the boxplots in figure 14 that portions of the fourth spread overlap for these till units. The median hydraulic conductivity measured in the field for till of the Middle Inlet Member is about an order of magnitude greater than the median value for till of the Kirby Lake Member.



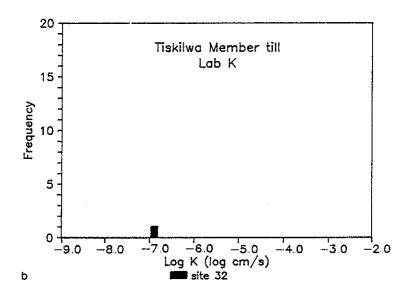
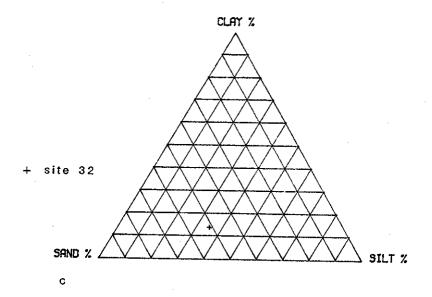


Figure 13. Data for till of the Tiskilwa Member of the Zenda Formation. a) Field K means hydraulic conductivity measured in the field. b) Lab K means hydraulic conductivity measured in the laboratory. Data are plotted with a pattern indicating the source.



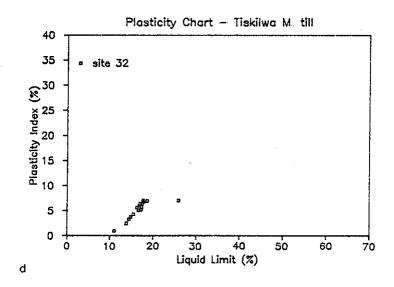


Figure 13, cont. Data for till of the Tiskilwa Member of the Zenda Formation. c) Sand, silt, and clay percentages are for the less than 2 mm fraction. Data are plotted with a symbol indicating the source.

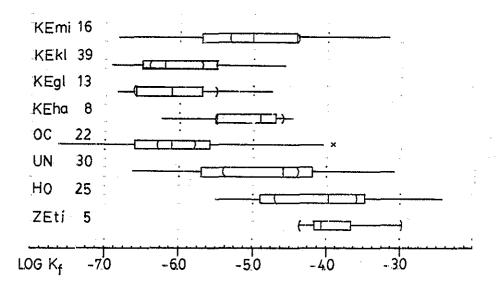


Figure 14. Boxplots for interunit comparison of hydraulic conductivity measured in the field $(K_{\mbox{\scriptsize f}})$. Boxplots are constructed for till units with at least 5 values. The number of values is given with the abbreviated unit name.

As mentioned in the section on variation within units, the unnamed unit stratigraphically below the Kewaunee Formation could be a member of the Horicon Formation. I rejected the null hypothesis that the medians of log hydraulic conductivity measured in the field in till of the unnamed unit and in till of the Horicon Formation are equal with a confidence level of 99%. Median log hydraulic conductivity measured in the field for these two tills differ by 0.6 order of magnitude.

To the east, the location of the batch median for the Glenmore Member may be compared to the data available for till of the Chilton Member (figure 14 and figure 8d). Each of the four measurements in till of the Chilton Member are within the 95% confidence limits for till of the Glenmore Member. The unnamed unit discussed in the preceding paragraph may also underlie the Kewaunee Formation on the eastern side of the Green Bay Lobe. The Horicon Formation does extend eastward to the Lake Michigan Lobe (see Plate 1).

b. Lake Michigan Lobe

Hydraulic conductivity data from field measurements are not available for till in each member of the Kewaunee Formation.

Insufficient data (fewer than 5 samples) are available for tills in the Haven and Ozaukee Members to test a null hypothesis, but the boxplot for till of the Haven Member in figure 14 may be compared to data for the Ozaukee Member in figure 8h. The single value for till

of the Ozaukee Member lies outside the range of 95% confidence for the median value of field hydraulic conductivity in the Haven Member.

Hydraulic conductivity data from field measurements of till in the Oak Creek Formation are relatively plentiful. In spite of the range over four orders of magnitude (figure 9), the range of the 95% confidence level for the median is only half an order of magnitude wide (figure 14).

Data compiled for the New Berlin Formation contain only four values of hydraulic conductivity measured with field tests (figure 12). Hydraulic conductivity values in till of the New Berlin Formation are 3 to 4 orders of magnitude greater than the median value for tills of the Oak Creek Formation in figure 14. Values of hydraulic conductivity measured in the field in tills of the New Berlin Formation have a range similar to till in the Tiskilwa Member of the Zenda Formation. A boxplot of hydraulic conductivity values measured in the field for till in the Tiskilwa Member is included in figure 14.

2. <u>Interunit comparison of hydraulic conductivity measured in the</u> laboratory

The median values hydraulic conductivity measured in the laboratory for each till have narrower approximate 95% confidence intervals than do the median values of hydraulic conductivity measured in the laboratory (note the scale differences before comparing figures 14 and 15). As for values of hydraulic conductivity measured in the field, boxplots have been constructed for tills with five or more

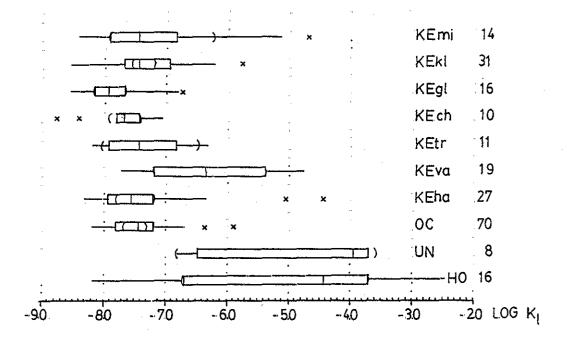


Figure 15. Boxplots for interunit comparison of hydraulic conductivity measured in the laboratory (K_1) . Boxplots are constructed for till units with at least 5 values. The number of values is given with the abbreviated unit name.

values available. ANOVA tests were applied to tills of overlying members. Refer back to figures 12 and 13 for the New Berlin and Zenda Formations.

In the Green Bay Lobe, insufficient data were available to reject the null hypothesis of equal median values of hydraulic conductivity measured in the laboratory for tills of these stratigraphically superposed lithostratigraphic units: Middle Inlet and Kirby Lake Members, Glenmore and Chilton Members, and the unnamed unit and the Horicon Formation. In the Lake Michigan Lobe, I rejected the same null hypothesis at a 99.5% confidence level for tills in both the Two Rivers and Valders Members and the Valders and Haven Members.

3. Vertical differences in texture

a. Green Bay Lobe

The tills of superposed members have similar textural ranges on both the east and west sides of the Green Bay Lobe. On the west side, the Middle Inlet Member analyses show greater scatter than those of the Kirby Lake Member below and include some samples that are much sandier than till of the Kirby Lake Member. On the east side of Green Bay, the till unit in the Glenmore Member is also slightly sandier than till of the underlying Chilton Member. Tills of the Horicon Formation are distinguished from tills in the Kewaunee Formation by their abundant sand content.

b. Lake Michigan Lobe

As in the Green Bay Lobe, till of the Two Rivers Member (figure 8e) is texturally very similar to till of the underlying Valders Member (figure 8f). The cluster of points for till of the Two Rivers Member illustrates a sandier 'average' texture than the cluster of till analyses for the Valders Member. Thus, texture in the upper two tills in the Green Bay and Lake Michigan Lobes changes in the same way, with increasing sand content upwards. The textures determined for till of the Haven Member (figure 8g) are less silty but otherwise very similar to till of the Valders Member (figure 8f). Till of the Ozaukee Member (figure 8h) contains more silt and clay than till of the Haven Member.

Below the Kewaunee Formation, till of the Oak Creek Formation is very similar to till in the Ozaukee Member. Many more particle size analyses are available for the Oak Creek Formation tills, and a wide range in texture is apparent. The tills of the New Berlin Formation, like till in the Horicon Formation, is distinctively sandy with a very low clay content. Only one complete analysis for till in the Tiskilwa Member was recorded. This single sample contains more clay than the 'average' till samples from the New Berlin Formation.

4. Interunit comparison of plasticity charts

Scatterplots of plastic index and liquid limit for the till units overlap. If the mean liquid limit and plastic index are used to represent each till as in figure 16, the same general trend emerges as from the individual plots with finer grained units farther from the origin.

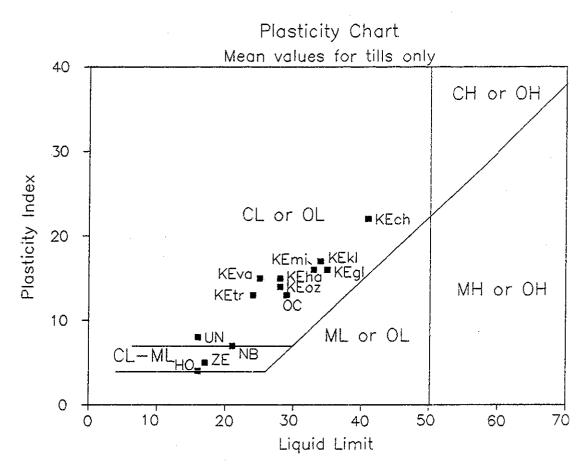


Figure 16. Plasticity chart with mean values of plasticity index and liquid limit for tills of lithostratigraphic units.

5. Interunit comparison of dry unit weight

Figure 17 consists of boxplots of dry unit weight for those units with five or more measurements. Dry unit weight data are summarized in table 4. The median dry unit weight of tills are very similar in superposed members of the Kewaunee Formation on the west side of the Green Bay Lobe (Middle Inlet and Kirby Lake Members) and in the Lake Michigan Lobe (Two Rivers, Valders, and Haven Members). Till of the Ozaukee Member is more similar to till of the Oak Creek Formation than to other Kewaunee Formation tills with respect to dry unit weight. A null hypothesis of equal median dry unit weights for the Haven and Ozaukee Member tills was rejected at a level of 99% confidence. The same null hypothesis could not be rejected for tills of the Ozaukee Member and the Oak Creek Formation or for other members in the Kewaunee Formation.

The median dry unit weight for the Horicon Formation exceeds all other medians by 15 pounds per cubic foot. This is most likely due to the unit lithology since the specific gravity of dolomite is greater than the specific gravity typically assumed for soils. Alternatively, the difference may be caused by the coarse particle size. No dry unit weight data were compiled for the New Berlin Formation, but it probably also has a relatively high dry unit weight because its lithology and particle size distribution resembles that of the Horicon Formation.

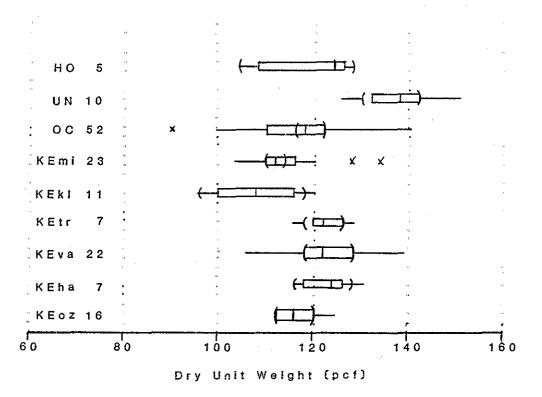


Figure 17. Boxplots for interunit comparison of dry unit weight. Boxplots are constructed for till units with at least 5 values. The number of values used to construct the boxplot is given with the abbreviated unit name.

Dry unit weight (pounds per cubic foot)

<u>till</u>	<u>N</u>	Median	Minimum	Maximum
KEmi	23	112.0	103,2	133.1
KEkl	11	107.0	611	119 8
KEgl	2	114.5	114O	115.0
KEch	0	_	· _	•
KEtr	7	122.0	115.5	127.9
KEva	22	122.4	99., 7	138.5
KEha	7	123.0	115.4	129.7
KEoz	16	116 . 1	111.1	123.0
oc	52	117.8	890	140.0
NB	0		-	~
ZEti	0	-	-	
НО	10	138.7	125.8	150.6
UN	5	123.9	104 . 7	128 . 1

Table 4. Statistical summary of dry unit weights in pounds per cubic foot for tills in lithostratigraphic units (except for 'UN') with number of samples (N), median values, minimum value, and maximum value.

6. Pocket Penetrometer

Surprisingly, the median pocket penetrometer measurement is significantly different for Lake Michigan Lobe tills in superposed lithostratigraphic units. Pocket penetrometer data is presented graphically in figure 18. The ranges are almost identical for all units. I tested and rejected the null hypothesis of equal medians for one way ANOVA of tills in the Two Rivers and Valders Members (97.5% confidence level), the Valders and Haven Members (99.5% confidence level), and the Ozaukee Member and the Oak Creek Formation (99.5% confidence level). The same null hypothesis could not be rejected for tills of superposed members in the Green Bay Lobe.

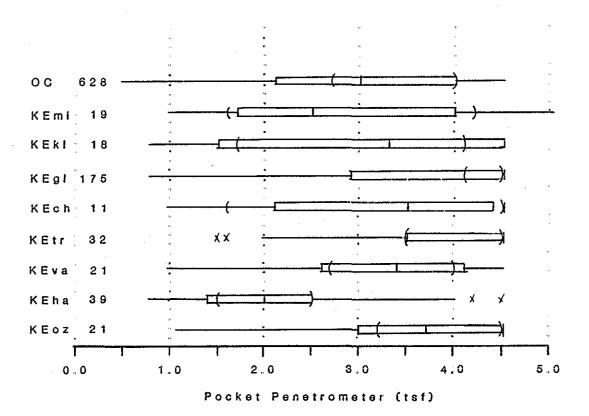


Figure 18. Boxplots for interunit comparison of pocket penetrometer measurements. Boxplots are constructed for till units with at least 5 values. The number of values is given with the abbreviated unit name.

V. Discussion of data

This section contains a discussion of the data presented in part IV, emphasizing the test methods and relations to other tests in till units. I use correlation and regression analysis to determine which tests are meaningful to hydrologic or geologic interpretation. These correlations and regressions do not imply cause and effect relationships.

A. Approximations of strength

1. Standard penetration test

There is a great deal of disagreement over how useful the standard penetration test is to hydrogeologists. Blow counts (N) from the Standard Penetration Test (SPT) (D1586-84, ASTM, pp. 298-303) have been used with limited success as an index test of strength and a predictor of deformation. Blow counts have been correlated with the Dutch Cone Test, the friction angle of sand, density of sands, shear strength in clay, modulus of compressibility of sands, and liquefaction potential with some success (Douglas, 1983; Dept. of the Navy, 1982; Dunn, Anderson, and Kiefer, 1980). However, ASTM D1586-84 states,

"Variations in N-values of 100% or more have been observed when using different standard penetration test apparatus and drillers for adjacent borings in the same formation. Current opinion, based on field experience, indicates that when using the same apparatus and driller, N-values in the same soil can be reproduced with a coefficient of variation of about 10%" (ASTM, 1986, p. 299).

Similarly, Baecher attributed 50% of observed scatter in SPT data to measurement noise (1984, p.11). Little emphasis was placed on

collection of SPT data for this study because different test apparatus and drillers generated the data and because glacial tills are known to contain boulders that inflate SPT estimates of strength.

2. Pocket penetrometer

Pocket penetrometer readings are commonly reported (in tons per square foot, tsf) for fine-grained sediments but rarely correlated with any other parameters. They are a relative measure of the unconfined compressive strength of a material. The ASTM has not published a standard method for use of the pocket penetrometer; use of a vane shear device is preferred and has been quantitatively correlated with other tests. The Dept. of the Navy Soil Mechanics Design Manual includes the following brief statement about pocket penetrometers: "The tool is an aid to obtaining uniform classification of soils. It does not replace other field tests or laboratory tests" (1982, p. 7.1-97). Pocket penetrometer measurements were typically recorded only for samples having hydraulic conductivity or grain size analyses.

3. Applications of approximations of strength

Strength data is relevant to geologic interpretation, but most authors who refer to it combine it with data not included in this study's database. For example, Scott and St-Onge (1969) recommend use of the pocket penetrometer to estimate the compactness of till. They write, "Compactness . . . embodies concepts of cohesion, consolidation, shear strength, and, because of the range in grain size of till, also relative density and consistency" (1969, p. 4). They

define a compactness ratio, C_r , equal to bulk density divided by void ratio and apparently then use the compactness ratio to characterize till units (1969, p. 6). Other authors have related shear strength to geologic stress history (Mickelson, Acomb, and Edil, 1979), deposition of cementing agents from the ground water (Baracos et al., 1983), clay mineralogy (Grim, 1962), density (Lutenegger, Kemmis, and Hallberg, 1981), and weathering profiles in till (Eyles and Sladen, 1981). It is important to note that these authors used laboratory determinations of shear strength, not a field approximation like the pocket penetrometer or a method characterized by high variation, like the standard penetration test. Although median pocket penetrometer measurements differ for individual till units, the data give little information about specific characteristics of the tills.

I investigated the relationship between density from SPT blow counts and hydraulic conductivity. One engineering firm implied that increasing blow counts correlate with decreasing field measurements of hydraulic conductivity. The data for till units are not suitable for correlation because they are not paired—blow counts vary over the screened interval used to determine field hydraulic conductivity.

SPT data show no correlation between blow counts and depth. From soil mechanics theory, I expect blow counts to increase with depth as the thickness of material over the interval measured increases. Figure 19, a scatterplot of SPT blow counts versus depth in the Oak Creek Formation, illustrates no correlation for these till,

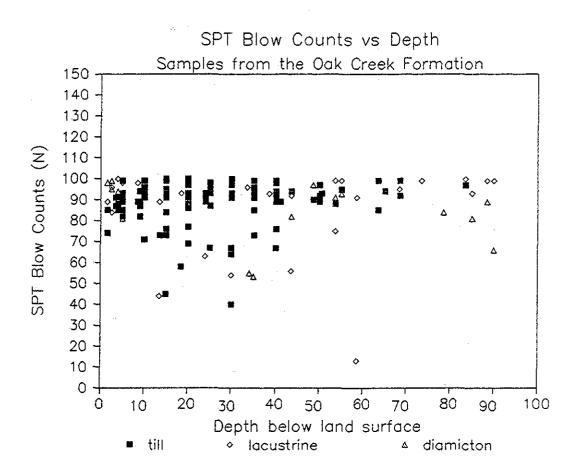


Figure 19. Plot of SPT blow counts as a function of depth below the land surface for sediments in the Oak Creek Formation.

lacustrine, or diamicton sediments, possibly because "... the testis conducted in a dynamic form and while the limited volume of material is in a state of failure and high disturbance" (Johnston, 1983, p. 12).

SPT blow counts have been correlated with shear strength in clay (e.g., Stroud and Butler, 1975) and pocket penetrometer measurements approximate unconfined compressive strength. However, a plot of SPT blow counts versus pocket penetrometer measurements for 453 samples of till from the Oak Creek Formation (figure 20) shows that a wide range of SPT blow counts may be anticipated for any pocket penetrometer measurement. Clearly, SPT blow counts and pocket penetrometer measurements are not directly related. A straight line, least squares regression indicates that 19% of the variation in blow counts may be explained by variation in pocket penetrometer measurements. Similar but not identical variables probably affect the two tests.

In individual boreholes considered in this study, pocket penetrometer readings tend to reach a maximum within several feet of the land surface. This maximum may reflect overconsolidation due to repeated wetting and drying within the capillary fringe, but appropriate consolidation data are not available to confirm this relationship. Moreover, pocket penetrometer readings should not be used to determine the elevation of the modern water table since the climate has changed following deposition of the sediment, and the zone of higher readings may represent past conditions.

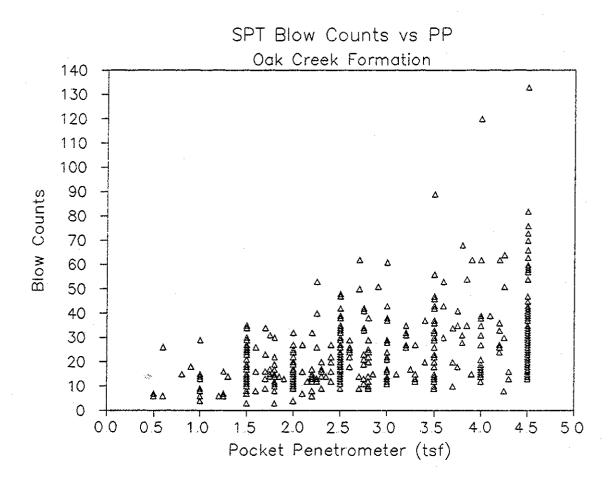
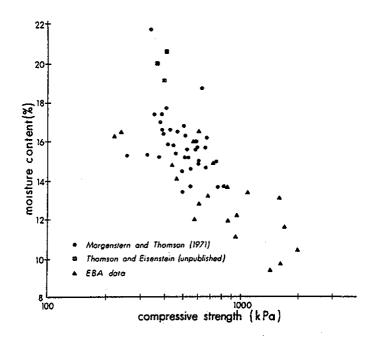


Figure 20. Plot of SPT blow counts as a function of pocket penetrometer measurements for samples of till in the Oak Creek Formation.

May and Thomson found higher strengths to be associated with lower moisture contents for selected till units of the Edmonton area (1978,p. 368). Figure 21 illustrates the relationship between natural moisture and log pocket penetrometer measurements for fine-grained till units included in this study. The individual units scatter throughout the large cluster without any indication of a trend characteristic of a single till or site. Similarly, Muldoon (1987), working with pre-late Wisconsin fine-grained till units in central Wisconsin, found no significant relationships between log pocket penetrometer and moisture content. Muldoon reported that other authors described a strong relationship between natural moisture and log pocket penetrometer for different Wisconsin till units.

B. Particle size analysis

The particle size divisions entered to the database include the percent of the sample greater than 2 mm, the percent sand, silt, and clay of the less than 2 mm fraction, and the P200 (percent passing the #200 sieve, 0.075 mm diameter). These categories were chosen to accommodate the different classification systems used by engineers and geologists. I recorded P200 values because this percentage is necessary for classification in the USCS and because analyses frequently are not completed beyond this particle size. Values of P200 are not presented except in the appendices because this percentage varies considerably with measurement technique. Values of P200 determined by dry sieving tend to be lower than those determined



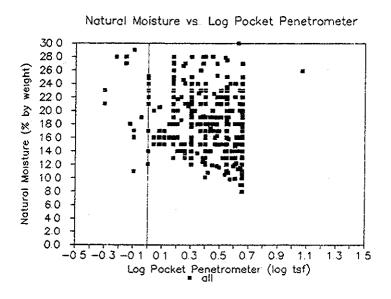


Figure 21. Relationship between natural moisture content and log pocket penetrometer. a) From May and Thomson (1978, p. 368). b) For fine-grained till units in eastern Wisconsin.

by wet sieving, and hydrometer analysis measurements of P200 tend to be greater than those determined by sieving. P200s may be used to check the USCS group symbol.

Wisconsin Geological and Natural History Survey (WGNHS) reports use the sand, silt, and clay divisions indicated in figure 3.

Percentages of these particle sizes are reported as matrix percent (that is, percent of the less than 2mm fraction of the sample) to normalize samples collected by different methods because the distribution of particles larger than 2 mm has a much greater spatial variability than the matrix percent in basal till. Furthermore, most sedimentological work uses these sand, silt, and clay classes and they are compatible with terms used in the geologic literature (see Folk, 1958, p. 5). Both sedimentologists and engineers, however, present grain size analysis in graphs of cumulative percent versus grain size diameter. Geologists who study Quaternary materials in Wisconsin adopted use of the textural triangle because early soil surveys placed a greater emphasis on soil parent material.

Considerable geologic interpretation was necessary to assign data to lithostratigraphic units. Frequently, the only type of information common to the definition of the lithostratigraphic units and the geotechnical data was particle size analyses. Discussion of particle size analyses will be limited to till units with observable trends or in which the texture of the matrix can be related to geologic processes or local sources. Sites are consistently identified by

number throughout the figures in part IV, on plate 1, in the appendices, and in the following text.

1. Till of the Middle Inlet Member of the Kewaunee Formation

As noted in the data presentation section, the textural analyses compiled for this study do not always plot within the confidence levels determined by the geologist who originally defined the lithostratigraphic unit associated with the till. For example, in the Middle Inlet Member, only two of the data points fall within the 95 percent confidence interval determined by McCartney (1979). I attribute this difference to the limited area from which data was collected in this study. McCartney based her definition of the Middle Inlet Member on particle size analyses of basal till samples from Marinette and Oconto Counties. Later analyses completed in the Quaternary Laboratory at the University of Wisconsin-Madison for till of the Middle Inlet Member farther southeast more closely resemble the data plotted in figure 8a. Need (1985) reported textural analyses for till of the Middle Inlet Member in Brown County. The mean sand, silt, and clay percentages in Brown County are 40, 40, and 20 for till of the Middle Inlet Member, compared to 22, 47, and 30 at site 24 (32 samples) in this study.

Within till of the Middle Inlet Member in Marinette and Oconto Counties, to the northwest of site 24 (plate 1), McCartney noted an increase in silt content which she attributed to the "incorporation of loess and weathered dolomite over Paleozoic rock in the southeast" (1979, p. 62). McCartney also noted that a similar trend of

increasing carbonate to the south may have the same cause as the increasing silt content to the southeast:

"... the carbonate increases to the south with increasing incorporation of the fine-grained, carbonate-rich material as the ice moved south into the lake-filled basin. This may also be the cause of the increase in silt content to the south" (1979, p. 86).

Initially, interpretation of the stratigraphy at site 24 was blocked by the marked difference between the textures at the site and the published definition. The location of site 24 is between McCartney and Mickelson's (1982) solid line border of the Middle Inlet Member and the Fox River. Site stratigraphy affirms the identification as till of the Middle Inlet Member: the Two Creeks Forest Bed underlies this till at site 24. Site 24 is a good example of how tills of lithostratigraphic units may be identified using the criteria listed in table 1a (stratigraphic position and particle size analysis/texture) and familiarity with the literature.

2. <u>Till of the Kirby Lake Member of the Kewaunee Formation</u>

The same deviation from McCartney's statistical summary is seen in till of the Kirby Lake Member, especially at sites 40 and 12 (plate 1 and figure 8b), which are farther south and closer to the Fox River than the type and reference sections. The mean sand, silt, and clay percentages for each site with till of the Kirby Lake Member are presented in table 5 with the number of analyses, N.

McCartney noted that till in the Kirby Lake Member appears texturally to be a reworked lake sediment that experienced little reduction in particle size due to glacial crushing before deposition (1979, p. 55, 73). Another investigator of till in the Kirby Lake

Till o	f the 1	Kirby La	ake Mem	ber						
	West	_							Eas	st
Site	38	39	22	:	23	30	40	41		12
N	24	4	2		4	1	13	1		8
% > 2 :	mm 7	4	11		40	1	1	.7		9
% sand	33	34	33	:	27	35	3	38	;	13
% silt	46	45	42	•	46	51	31	52		40
% clay	21	22	25	:	27	17	67	11	4	48
Till of the Cak Creek Formation										
	est									East
Site	55	35	53	21	14		51	52	20	28
N	7	23	8	16	29		4	2	81	7
% > 2 mm	16	4	1	. 2	6		13	0	2	10
% sand	28	14	11	7	16		21	13	13	23
% silt	47	56	43	49	50		48	43	59	45
% clay	25	29	45	44	34	1	31	45	27	32

Till of the Horicon Formation								
No	rth	•	South					
Site	11	8	13	7				
N	5	7	2	8				
% > 2 mm	32	17	6	11				
% sand	64	51	71	77				
% silt	33	36	20	17				
% clay	3	14	9	6				

Till	of the Ne	w Ber Vest	lin Form	mation East
	-			
	Site	33	36	55
	N	15	3	8
	% > 2 mm	30	18	52
	% sand	64	27	75
	% silt	29	67	20
	% clay	6	6	6

Table 5. Mean values of % greater than 2 mm, matrix percent sand, matrix percent silt, and matrix percent clay for till units by site. The maximum, minimum, and median are just as important as the mean, and reference to the plot in figure 8b (Kirby Lake Member), figure 9 (Oak Creek Formation), figure 10 (Horicon Formation), and figure 12 (New Berlin Formation) should be made. Site locations are plotted on plate 1.

Member (Piette, 1963) experienced difficulty distinguishing the till from lacustrine sediment even with good field exposures in Brown County. Need characterized till of the Kirby Lake Member as composed of 16% sand, 46% silt, and 38% clay in Brown County (1985, p. 10). This statistical summary is considerably different from the summary determined by McCartney for Marinette and Oconto Counties (and plotted in figure 8b). Like Piette, I found it very difficult to distinguish between massive, clay-rich lacustrine sediment and till in the Kirby Lake Member, and I relied on the sorting evident in complete particle size analyses to distinguish the two

Assuming that the till in the Kirby Lake Member is indeed reworked glaciolacustrine sediment, it is reasonable to assume that it would become finer in the Green Bay lowland with increasing distance from the ice front. The particle size data summarized above indicates that till of the Kirby Lake Member is much finer in the Green Bay lowland than in Waupaca (sites 38 and 39), Oconto (sites 22 and 23), and Shawano (site 30) Counties to the north and west. Finer-textured till in the Kirby Lake Member should be expected near Lake Winnebago than to the north and west.

3. Till of the Glenmore Member of the Kewaunee Formation

Need (1985) and McCartney and Mickelson (1982) present statistical summaries of till in the Glenmore Member that differ by only one percent in the sand and clay fractions. Till of the Glenmore Member is siltier at site 1 and sandier at site 10 with less clay than the mean (plate 1 and figure 8c). Site 1 is in western Brown County

near the Niagaran escarpment and overlies a gray, stony, silty till (possibly the Wayside Member of Need (1985)). Thus, at site 1, the siltier till in the Glenmore Member may be attributed to local incorporation of the underlying silty till. At site 10, in Door County, till of the Glenmore Member is lodged against the Niagaran escarpment of the Door Peninsula. Higher sand content at site 10 may be due to glacial erosion and mechanical weathering of bedrock or to incorporation of sand beaches.

4. <u>Till units of the Chilton, Two Rivers, Valders, Haven, and Ozaukee</u> Members of the Kewaunee Formation

Data for till units of the Chilton, Two Rivers, Valders, Haven, and Ozaukee Members are plotted in figures 8c through 8h. Although some of these particle size analyses plot outside the confidence intervals determined by the geologist who defined the lithostratigraphic units, I could not attribute the differences to geologic process or to provenance. In fact, particle size analyses of till from the Chilton Member are from the northern and southern extremes of the Chilton Member's mapped extent, but the few data do not illustrate trends like those in till units of the west side of the Green Bay Lobe. As previously mentioned, discrepancies between published particle sizes and data compiled here may be due to use of only basal till in the definition of the lithostratigraphic unit.

5. <u>Till of the Oak Creek Formation</u>

Schneider and Need (1985) discuss the texture of glacial sediments in the Oak Creek Formation, but use 0.004 mm as the division

between silt and clay size fractions. Thus, the textural envelope provided by Schneider and Need has not been reproduced in figure 9. Schneider and Need report average grain-size composition of till units equivalent to Oak Creek Formation till units from Wisconsin and In Wisconsin, the mean of 68 samples was 12% sand, 44% silt, and 44% clay (<0.004 mm) (Schneider and Need, 1985, p. 58). The very sandy outliers apparent in figure 9 probably represent blocks of sandy sediment locally incorporated into till. Means of sand, silt, and clay for the data plotted in figure 9 are summarized in table 5 by site with left-to-right representing west-to-east. Unlike the particle size analyses for till of the Kirby Lake Member, no clear trend is apparent in till units of the Oak Creek Formation at this scale, and variability at one site, 20, covers nearly the entire range (figure 9). Interbedded silty or sandy sediments and till were recorded as '99' during data collection and were not genetically interpreted.

6. Till of the Horicon Formation

The southern extent of the Horicon Formation has not been geologically studied and divided into members, so few references on particle size analyses are available. The analyses plotted in figure 10 may not be representative of the till because only relatively fine-grained samples would have particle size analyses completed to 0.002 mm for classification purposes at landfill sites. Sand, silt, and clay means are presented in table 5 by site with north to south approximately represented by left to right. Site 11 in Brown County

and probably contains till of the Wayside Member (Need, 1985). Sites 8, 13, and 7 are in Dodge, Green Lake, and Dane Counties, respectively; these sites show a progressive fining to the south. This could result from deposition by a glacier that readvanced over proglacial or post glacial lake sediments in the Green Bay lowland, or it could indicate that debris entrained in the glacier was more thoroughly reduced in size before it was deposited during ice wasting and glacial retreat to the north.

7. Till of the unnamed unit

Particle size analyses of till from sites 12, 24, 40, and 41 in Fond du Lac, Outagamie, and Winnebago Counties (figure 11) demonstrate the existence of a till unit much siltier than expected in the Horicon Formation and stratigraphically below the Kewaunee Formation. McCartney and Mickelson assert that there are no till units correlative to the Oak Creek Formation till units in the Green Bay lowland (1985, p. 301). Their research did not provide sufficient data to support this contention because it did not extend farther south than the north end of Lake Winnebago. The data compiled for this study are not adequate to test the hypothesis that the sediments at these sites (and possibly at site 1 in Brown County) represent a unit correlative with the Oak Creek Formation in the Lake Michigan basin. In support of this hypothesis, ice in the two lobes seems to have behaved similarly during deposition of the Horicon and New Berlin Formations and during deposition of the Kewaunee Formation as indicated by interlobate moraines and outwash surfaces. I know of no

evidence indicating that ice in the two lobes did not behave similarly during retreat from a middle Woodfordian maximum.

8. Till of the New Berlin Formation

Schneider and Need report the following average texture for till of the New Berlin Formation: 58% sand, 29% silt, 13% clay (<0.004 mm) for 15 samples (1985, p. 58). The envelope they plot for till has not been reproduced in figure 12 because of the difference in size classes. The textures of samples from all the sites contain less clay than those reported by Schneider and Need. Presumably, this is due to the differing definitions of clay since no obvious trend is apparent when data from the three sites are separated. Mean size classes are presented in table 5 with left to right representing west to east. Sites 33, 36, and 55 are in Walworth, Washington, and Waukesha Counties, respectively. The large variation in mean particle size class from site to site may be due to local influences or may result from an unrepresentative, small number of analyses.

9. Till of the Tiskilwa Member of the Zenda Formation

The single textural analysis of till at site 32 (figure 13) indicated a composition between the "typical" (42% sand, 35% silt, and 23% clay) and "sandy phase" (65% sand, 24% silt, 11% clay) (Mickelson et al., 1984, p. A6-6).

C. Atterberg Limits

1. Background

Atterberg limits have been used primarily as an aid to classification in the Unified Soil Classification System (USCS), but this classification is of little use to glacial geologists or to hydrogeologists except in a very general way. Complete particle size analyses give much more information about depositional process than Atterberg Limits as they are determined for use in the USCS. I studied the references available on Atterberg Limits to determine whether the limits and indices derived from them could be of use to hydrogeologists or geologists.

A. Atterberg, a swedish scientist, established his "limits of consistency" in 1911 in an attempt to classify soils in their plastic state by their water content. Of Atterberg's original six consistency limits, only the liquid limit (LL), plastic limit (PL), and shrinkage limit (SL) have been incorporated into geotechnical practice. The liquid limit is the lower limit of viscous flow, and the plastic limit is the lower limit of the plastic state. (See Casagrande, 1932 for a more detailed summary of Atterberg limits.) Figure 22 illustrates the physical meaning of these three limits. Atterberg also defined the plasticity index as the difference between the liquid limit and plastic limit (PI = LL - PL). The ASTM standard method for determining Atterberg limits specifies use of the less than 0.425 mm fraction of the sample (D4318-84, ASTM, 1986).

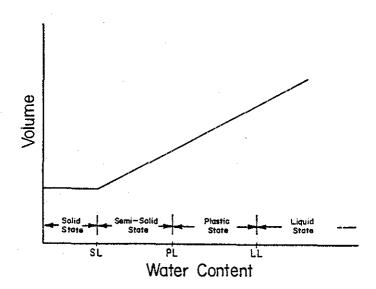


Figure 22. Atterberg limits related to volume and water content. The increase in volume from the shrinkage limit to the plastic limit is part air—and part water—filled void space. The soil is saturated at the plastic limit and increases in volume from the plastic limit consist of water. (From Dunn, Anderson, and Kiefer, 1980, p. 28.)

Atterberg limits have received considerable attention in the geotechnical and soils literature, but are sometimes used inappropriately in contexts for which they were not developed. For example, they have been interpreted to indicate pollutant attenuation potential or cation exchange capacity when too little information is available for such inferences. Atterberg limits have been correlated with compressibility, compactability, shrink-swell, shear strength (ASTM, 1986), specific surface area, geometric properties of clay, physical-chemical factors (Nagaraj and Jayadeva, 1981), organic matter content, percent clay, and clay mineralogy (Odell, Thornburn, and McKenzie, 1960). Farrar and Coleman (1967) found a high correlation between liquid limit and cation exchange capacity and specific surface area. Atterberg limits are influenced by mixing and drying of the sample, particle size distribution, presence of organic matter (Casagrande, 1932), mineralogy, and pore fluid chemistry (Yong and Warkentin, 1975), and a concise interpretation depends on an accurate definition of the variables in the soil-water system. Moreover, the determination of Atterberg limits destroys the soil's structure so that Atterberg limits yield information about material properties which are not necessarily the same as in-situ properties.

2. Plasticity charts

Casagrande, or plasticity, charts consist of liquid limit on the x-axis and plasticity index on the y-axis. Casagrande plotted an "A-line" on the chart to classify soils. Glacial sediments, like any other sediments, should plot in an elongate cluster parallel to the A-

line. Decreasing particle size within the fraction tested increases both the liquid limit and plastic limit, but increases the liquid limit more (White, 1949). An elongate cluster of data with positive slope results from the variation in particle size distribution within the fractions tested. Muldoon found that increasing matrix percent sand correlated negatively with Atterberg limits (1987, p. 86); the presence of fine sand in the less than .425 mm fraction for the Atterberg limits test suppressed limit values. Chassefiere and Monaco (1983) found the location of sediments along the A-line to be a function of the degree of evolution of the sedimentary facies (sorting) and the smectite content. Figure 23 shows the general relationship between liquid limit and plastic index for several sediment and soil types.

Boulton and Paul (1976) tried to relate Atterberg limits to glacial sediments and introduced a "T-line" for tills which they plot on plasticity charts. Boulton and Paul found that melt out tills occupy a field on the plasticity chart similar to that for englacial debris and lodgement till from the same glacier. Given an understanding of why sediments and soils plot in elongate clusters on a plasticity chart, the T-line is superfluous—especially since it does not differentiate between glacial facies and is not part of a classification system.

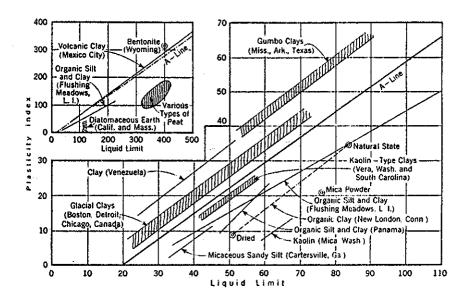


Figure 23. Plasticity chart for a variety of soils. (From Casagrande, 1947, p. 803.)

3. Clay mineralogy

Atterberg limits may be related to geology in a way not illustrated by the plasticity chart and have been used to identify clay minerals. For example, Bain (1971) plots plastic limit on the yaxis against plasticity index on a log x-axis to separate clay mineral clusters. Figure 24 shows plots of this type for till units from eastern Wisconsin. Mickelson et al. (1984) report semi-quantitative x-ray diffraction analyses for clay minerals in some of eastern Wisconsin's till units; these are included in the same figure. These plots indicate agreement with published clay mineral analyses. in the Oak Creek Formation has the highest illite content and since illite has low plasticity, plots closer to the y-axis. Although clay mineral analyses are not available for the Kirby Lake, Glenmore, and Chilton Members, I infer from the plots that the mineralogy of these till units resembles the other members in the Kewaunee Formation. The influence of fine sand and silt in the less than 0.425 mm fraction complicates interpretation of these plots.

4. Activity

Atterberg limits have been used to derive indices in addition to the plasticity index. For example, activity is defined as the plasticity index divided by the percent less than 0.002 mm (A = PI / % clay). Sediments with activities less than 0.75, between 0.75 and 1.25, and greater than 1.25 are classified as inactive, normal, and active (Grim, 1962). Professionals concerned with the suitability of material for liners and caps would prefer to use materials that are

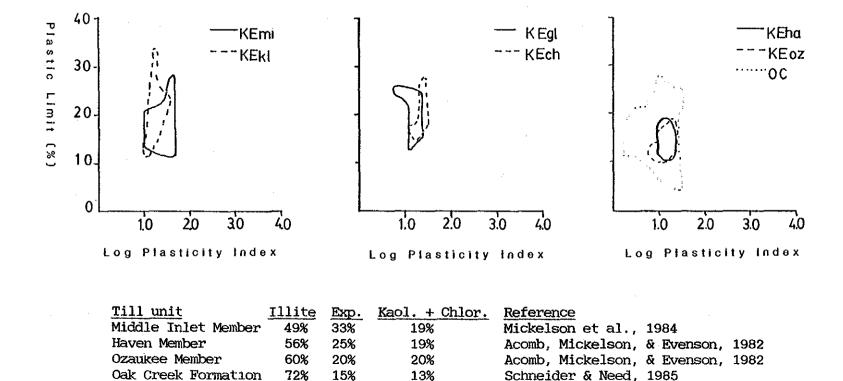


Figure 24. Plots of plastic limit versus log plasticity index for till units in superposed lithostratigraphic units. These plots (after Bain, 1971) indicate agreement with the published clay mineral analysis for till units—only the till in the Oak Creek Formation is considerably different. I infer from the plots that the clay mineralogy of the Green Bay lobe till units in the Kewaunee Formation is similar to those analyzed.

inactive and unlikely to heave or shrink and swell. According to Terzaghi (1955), activity varies with particle size, adsorption complex, and mineralogy. Activities for samples of till with both plasticity indices and percent clay are summarized in table 6. Only till units in the Kirby Lake and Middle Inlet Members of the Kewaunee Formation included samples that were classified as active. These two till units also included proportionally more samples classified as normal. Most of the late Wisconsin till units in eastern Wisconsin are inactive.

Grim (1962) associates the following qualities with active clays: relatively high water holding capacity, high compaction under load, high cation exchange capacity, variation in properties with variation in exchangeable cations, high thixotropy, low permeability, low resistance to shear, and strength dependent on cohesion (p. 219). Uehara and Gilman find that tropical soils with low activity

" do not shrink or swell greatly, are generally well aggregated, and therefore have higher water intake rates, which in turn reduces hazards from erosion. They can accommodate traffic more readily after heavy rains and offer less resistance to tillage implements than do soils with high-activity clays of comparable textures" (1981, pp. 99-100)

Presumably Uehara and Gilman's observations about activity are not limited to the tropics, and most late Wisconsin till units in the eastern third of Wisconsin are not expected to cause problems for the geotechnical engineer. If Atterberg limits are determined for the entire sample rather than for the fraction less than 0.425 mm, the sample may be classified by its potential for volume change (Dept. of the Navy, 1982, p. 7.1-38).

Activity classification				Lie	Liquidity index classification				Consistency index		
Till unit	N	Inactive	Normal	Active	N	Solid	Plastic	Thixotropic	N	mean	std. dev.
KEmi	23	18	2	3	23	17	6	0 .	23	1.8	0.8
KEkl	67	51	14	2	67	47	20	0	67	1.6	0.7
KEgl	4	4	-	-	4	4	o	0	4	1.9	ο.
KEch	8	6	2	-	8	8	o	0	8	1.9	0.2
KEtr	0	-		4	0	0	0	0	0		-
KEva	53	48	5	***	53	29	24	0	53	1.3	0.5
KEha	13	12	1		13	13	0	0	13	1.9	0.3
KEoz	22	21	1		22	5	17	0	22	1.0	0.6
НО	6	6		***	6	. 6	0	0	6	4.1	0.7
oc	106	105	1	414	102	81	21	0	104	2.2	1.4
NB	1	1	-		1	1	0	0	1	5.8	-
ZEti	1	1	-	=	1	1	0	0	1	2.9	_

Table 6. Summary of classication using activity and liquidity index with N, total number of samples representing the till of a lithostratigraphic unit, and the number of samples in each category. Summary of consistency index with number of samples per till (N) in a lithostratigraphic unit, mean, and standard deviation.

5. Liquidity index

The liquidity index is also derived from Atterberg limits. Liquidity index is defined as the quantity natural moisture content minus plastic limit divided by plasticity index (LI = (nm% - PL) / PI). If the liquidity index is less than 0, between 0 and 1, or greater than 1, then the material is solid, plastic, or thixotropic (regains strength over time), respectively (Chassefiere and Monaco, 1982, p. 174). A high liquidity index is probable in highly porous, fine-grained sediments with high natural moisture. Such conditions might be met by a clay-sized material that flocculated to silt-size sediment—for example, by a water-laid till or lacustrine sediment—but are more likely in an aqueous than a sub-ice environment.

Boswell (1961) associated decreasing liquidity indices with increasing geologic age. He suggested that the liquidity index would be negative in Paleozoic clays and shales and occasionally negative in Cenozoic and Mesozoic clays. Boswell expected glacial and recent clays to have liquidity indices equal to 2.0 or 3.0 (p. 68). In contrast to Boswell, Skempton and Northey (1952) explain that glacially overconsolidated clays don't regain strength because their liquidity index roughly equals zero. Thus, there is no possibility for age-hardening.

Liquidity indices for the till units included in this study are summarized in table 6. As might be expected, most till units were classified as solid, but a significant proportion of the till samples in the Middle Inlet, Kirby Lake, Valders and Ozaukee Members and in

the Oak Creek Formation are plastic. Since consolidation is really a dewatering process that doesn't affect Atterberg limits (water is added to the sample to determine Atterberg limits), higher liquidity indices should be associated with less well consolidated sediments regardless of their age.

6. Consistency index

Boswell (1961) defines another index derived from Atterberg limits, the consistency index, CI = (LL - % nm) / PI. Boswell writes, "In high moisture sediments it becomes zero or negative and tends to increase as deposits become older and to possess lower Atterberg limits" (1961, p. 68). It is clear from the equation that the consistency index approaches zero and negative values when the natural moisture content is high. Values of the consistency index are given in table 6. The consistency index increases with geologic age of the sediments only if the natural moisture content decreases and all the variables affecting Atterberg limits remain constant. The consistency index appears to have no applications for geotechnical engineers or geologists.

D. Classification in the Unified Soil Classification System

The only benefit of using the USCS appears to be establishment of a common language among professionals, but lack of a common reference restricts this benefit. I recorded USCS group symbols from grain size curves or descriptions of samples given on lab sheets and from boring log descriptions when a more specific source was not available. Even

though these symbols are "standardized", not all the engineering consulting firms use the USCS in a consistent way. Group symbols are reported combined by hyphens, slashes, commas, and 'and'. The Casagrande chart typically used in textbook descriptions of the USCS shows only one combined symbol, CL-ML, although the ASTM references (D2487-85 and D2488-84) include discussions of when hyphenated symbols and symbols with a slash may be used. The USCS, a revised version of the Airfield Classification (AC) System developed in 1947 by Casagrande, was not specifically intended for hydrogeologic assessment.

A sixty-page discussion of the AC system in Casagrande's 1948 publication documents a variety of misgivings about application of the system for all purposes. In fact, Casagrande emphasized that group symbols are no substitute for detailed descriptions (1948, p. 917). The system was intended for field classification under circumstances such that only manual techniques are practical. Criticisms of the AC system include: that the system ignores fundamental soil properties (Hough, p. 987), that the system is actually a plasticity classification for fine-grained soils and a textural classification for coarse-grained soils (Lane, p. 952), that further confusion of plasticity and consistency would result from its use (Sowers, p. 959), and that it is frequently appropriate to use at least several classifications for describing soils (Spangler, p. 978; all in Casagrande, 1948).

Figure 16 clearly shows that the USCS can not distinguish between till units in the Kewaunee Formation or Oak Creek Formation. The USCS usually does differentiate between outwash and fine-grained till in the Kewaunee and Oak Creek Formations, but does not differentiate between till and outwash in the sandier Horicon Formation. Batches of hydraulic conductivity data for till of lithostratigraphic members have been compared, and ANOVA tests indicate that the hydraulic conductivity values are from populations with statistically significant differences. The USCS does not distinguish between genetic units; thus it gives no clues about geometry of the soil material (on the scale of this study). Neither the USCS nor the lithostratigraphic classification distinguish materials with statistically significant different hydraulic conductivities.

E. Hydraulic conductivity

Hydraulic conductivity is the most important material parameter determined during assessment of site conditions for waste disposal systems. Accordingly, assembling available hydraulic conductivity data for the various geologic units has been a major focus of this project. Recompacted samples were not included in the hydraulic conductivity data collection because the project focuses on characterization of in-situ materials. Other investigators (Muldoon, 1987; Herzog and Morse, 1984; Olson and Daniel, 1981) have reported that various methods of hydraulic conductivity measurement can yield widely varying results, and that laboratory and field measurements of

hydraulic conductivity may vary from each other due to problems of scale and disturbance.

In a thorough review article, Olson and Daniel (1981) list six major causes for higher field than lab hydraulic conductivity:

"(1) a tendency to run laboratory tests on more clayey samples; (2) the presence of sand seams, fissures, and other macrostructures in the field which are not represented properly in laboratory tests; (3) the use of lab k values back-calculated from consolidation theory rather than directly measured values; (4) measurement of vertical flow k in the laboratory and horizontal flow k in the field; (5) the use of distilled water in the laboratory; (6) air entrapment in laboratory samples" (p. 54).

When laboratory and field hydraulic conductivity data compiled for this study are sorted by till units, the laboratory and field data differ by at least an order of magnitude for a combination of all these reasons. Many of the landfill studies are for proposed zone of saturation sites. Thus, consultants may have been concerned with finding a material suitable for use as clay liner material and may have selected finer-grained samples for laboratory testing. Connell (1984) and Fleming (1986) document the existence of fractures and/or joints in the clayey till units included in this study. Written descriptions of samples used for laboratory measurement of hydraulic conductivity almost never include these structures. Relatively few of the lab hydraulic conductivity data were determined using a method derived from Terzaghi's consolidation theory. Olson and Daniel (1982) ascribe the discrepancies between conventional permeability tests and consolidation theory to ". . . the fact that the classical theory of consolidation makes no adjustment for the structural viscosity of the soil" (p. 25). In contrast, Houston and Kasim (1982) write that the

consolidation test is usually the most satisfactory method for clays with low hydraulic conductivity and high compressibility of the material skeleton (p. 152).

Scale is perhaps the most important factor influencing the differences between lab and field hydraulic conductivity in this study. There is little or no evidence that vertically oriented samples of less than 5 inches diameter taken from a borehole and tested for hydraulic conductivity in a laboratory yield values of vertical hydraulic conductivity appropriate for use in the field at a site of many acres. The fractures and/or joints evident in the field (sometimes identified by gleyed colors, oxidized rims, manganese precipitate, calcite crystals, or silt coats) most likely have a profound, positive influence on vertical hydraulic conductivity and rate of groundwater recharge. These fractures may account for much of the discrepancy between lab and field values.

Unfortunately, neither field nor lab hydraulic conductivity data are suitable for a quantitative comparison of the accuracy of measurement methods. I attempted a two-way analysis of variance test for hydraulic conductivities measured in the laboratory for samples of till from the Oak Creek Formation. Till properties vary from site to site, and I had hoped to determine whether one test method consistently gave higher or lower values at individual sites.

However, consistent test methods are usually used at single sites, and two-way analysis of variance requires the same variety of methods at all sites.

Direct comparison of lab and field hydraulic conductivity and comparison of measured hydraulic conductivity with grain size methods of estimating hydraulic conductivity require that the tests and measurements be made on paired samples. Very few lab hydraulic conductivity tests were performed on samples opposite piezometer screened intervals with field test data. Complete grain size data were not available for many samples with hydraulic conductivity data. Muldoon (1987) controlled the selection of samples for testing and was able to regress many variables, including grain size data, against hydraulic conductivity.

1. Field hydraulic conductivity

Using dissimilar sources of hydraulic conductivity data presents several inherent problems. First, the choice between rising and falling head tests could induce variation by a factor of 500 according to Milligan (Houston and Kasim, 1982). Second, several reports included more than one value of hydraulic conductivity for the same well or piezometer, and some values of hydraulic conductivity were determined by Bureau of Solid Waste Management tests and calculations. In these cases, both values are reported in the appendices, but Bureau of Solid Waste Management values were used for the statistical analysis of hydraulic conductivity. Third, a lack of consistently organized raw data in the database prevented consistent recalculation of all hydraulic conductivity values.

The nature of the geotechnical investigations limits the choice of a field method. Many of the piezometers with hydraulic

conductivity determinations are also used to detect changes in static water level or for water quality monitoring. Consultants are reluctant to introduce water to such wells, and prefer to bail down the water level for rising head tests. Thus the removal of the 'slug' of water is not instantaneous. Piezometers with ten-foot-long screened intervals were common. Shorter screened lengths, such as three feet, are preferred for better resolution of head (a 'point' measurement) and to prevent down— and up— hole dilution and/or contamination in the event of leachate movement.

The implementation of field methods has changed rapidly since 1980. In particular, the use of field measurements of hydraulic conductivity has become a legal necessity and improved implementation of the technique may have been concurrent. Most of the data included here are from baildown tests. Whether the same values would result from use of a pressure transducer and continuous recorder is not known. Firms referred to journal articles (Bouwer, 1961; Bouwer and Rice, 1976; Cooper, Bredehoeft, and Papadopulos, 1967; Papadopulos, Bredehoeft, and Cooper, 1973) and standard references (Department of the Navy, 1971; Chow, 1964; Freeze and Cherry, 1979; Hvorslev, 1951) to document their methods. These references focus primarily on choice of an appropriate equation for data analysis, and little attention is devoted to the technique of performing the field test, well construction techniques, or analysis of experimental error.

Scarrow (1985) discussed the effect of screen length on field determinations of hydraulic conductivity and concluded that longer

screen lengths give lower values of hydraulic conductivity (pp. 65, 66). The data compiled for this study do not support Scarrow's assertion. Figure 25 indicates that the length of the saturated interval tested does not have a dominant influence on the value of hydraulic conductivity. Scarrow also concluded that "the method chosen to analyze slug test data does not have any measurable impact on the accuracy of the subsequent conductivity estimate" (1985, p. 72). The several orders of magnitude variation seen within till units, then, must reflect variation within the till units according to Scarrow's analysis.

2. Laboratory measurements

Laboratory measurements of hydraulic ocnductivity are used in several phases of the landfill siting and approval process, and it was necessary to read the consultants' reports to determine whether reported laboratory measurements of hydraulic conductivity represented 'undisturbed' conditions. Nearly all the reports lack a description of the laboratory equipment used. The frequent absence of references for the laboratory hydraulic conductivity method used indicates that standard methods for laboratory measurement of natural materials in their native state do not exist. Herzog and Morse (1984) and Muldoon (1987) emphasize description of the laboratory apparatus for this reason. Most laboratory data were labelled as rising or falling head but recompacted samples from clay liners were not always clearly identified. I avoided errors in interpretation of the data by reading the accompanying text. Reading errors could be eliminated by

Till of the Oak Creek Formation

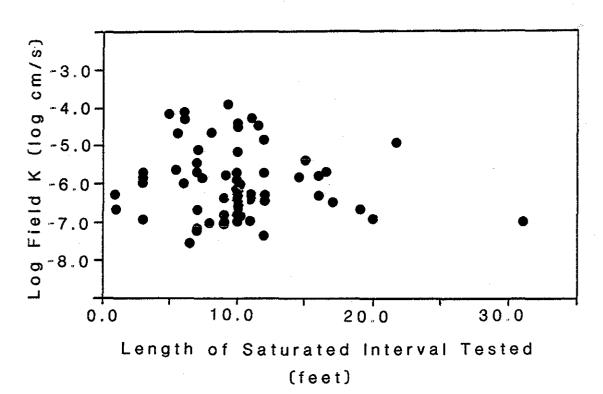


Figure 25. Log hydraulic conductivity from field measurements versus length of the saturated interval tested.

reporting field compacted (liner), lab recompacted, and in-situ values in separate columns or tables.

F. Dry unit weight

Hydrogeologic assessments do not require determination of dry or moist unit weight but hydrologic use may be made of the data.

Materials frequently tested for dry unit weight include potential lining materials for which standard or modified proctor compaction tests are run. The relationship between dry unit weight and porosity should follow weight-volume equations established by soil mechanics theory. The equations of interest are in figure 26. Assuming a specific gravity for the glacial sediment, the void ratio and porosity may be calculated from the dry unit weight. Porosities are needed to calculate average linear velocity and travel times (Feinstein and Anderson, 1987, p. 95).

Samples are typically removed from below the water table. Then, assuming saturation, natural moisture content should equal porosity and be related to void ratio. At low porosity, dry unit weights should be higher. Plotted data illustrate this relationship (figure 26). The straight-line fitted equation explains 80% of the variation in natural moisture content for samples from the Oak Creek Formation. For example, the 95% confidence interval for an individual natural moisture content ranges from 14.9 to 21.7% when the dry unit weight equals 115 pcf. The 95% confidence interval for the mean of all natural moisture contents ranges from 17.9 to 18.8% when the dry unit

$$gamma_d = \frac{G}{1 + e} \qquad e = \frac{G * gamma_w}{gamma_d} - 1$$

$$e = \frac{n}{1 - n} \qquad n = \frac{e}{1 + e}$$

Where: G = specific gravity, unitless

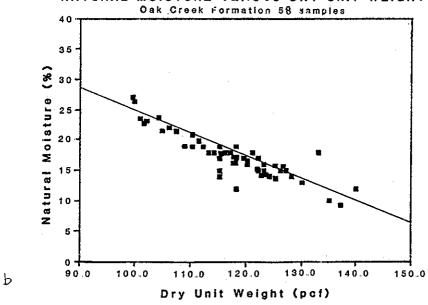
gamma_d = dry unit weight, from data

gamma_w = unit weight of water, 62.5 pcf

e = void ratio

n = porosity

NATURAL MOISTURE VERSUS DRY UNIT WEIGHT



The regression equation is nm % = 60.0 - (0.36 * dry pcf)

0

Coef. Std. dev. of the Coef. t-ratio A (y) 60.01 2.82 21.28 b (x) -0.36 0.02 -15.15 s = 1.726 $R^2 = 80.4\%$ R^2 (adj.) = 80.0% The t-value corresponding to 56 degrees of freedom and 95% confidence is 1.96.

Figure 26. a) Equations for the calculation of porosity from dry unit weight. Specific gravity is usually estimated as 2.65 (Dunn, Anderson, and Kiefer, 1980, p. 19). b) Natural moisture versus dry unit weight.

weight equals 115 pcf. A regression of dry unit weight on natural moisture content also indicates a statistically significant relationship. The regression results are included in figure 26.

G. Relationships between hydraulic conductivity and other tests.

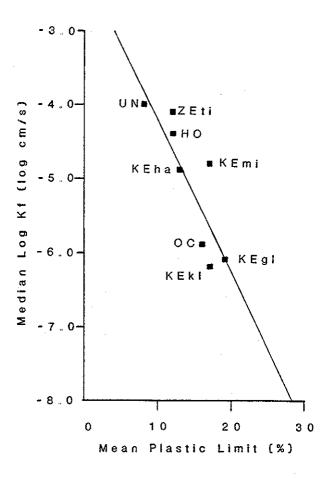
As previously stated, investigation of the relationship between textures and hydraulic conductivity using correlation and regression is not possible because the data are not paired. For the same reasons, exploratory data analysis of relationships between hydraulic conductivity and other data parameters is limited to plots of median values for lithostratigraphic units.

1. Hydraulic conductivity and plastic limit

Previous work suggests that a relationship may exist between plastic limit and hydraulic conductivities measured in the field.

Connell (1984) observed a weak negative correlation between plastic limit and the frequency of vertical joints. A good correlation between the log of hydraulic conductivities measured in the field and plastic limit would be expected if a relationship exists between plastic limit, fracture frequency, and field hydraulic conductivity in these data. I plotted the median value of hydraulic conductivities measured in the field versus the mean plastic limit for till units with more than 5 values of each.

Although the data in figure 27 appear to illustrate a trend and the straight line regression equation explains 67% of the variation in log median hydraulic conductivity measured in the field, the



The regression equation is Log
$$K_f = -2.14 - (0.206 * PL)$$
 Coef. Std. dev. of the Coef. t-ratio A (y) -2.14 0.779 -2.75 B (x) -0.21 0.053 -3.88
$$s = 0.509 \quad R^2 = 71.4\% \quad R^2 \; (adj.) = 66.7\%$$

The t value corresponding to 6 degrees of freedom and 95% confidence is 2.45.

Figure 27. Regression of median log hydraulic conductivity measured in the field on mean plastic limit.

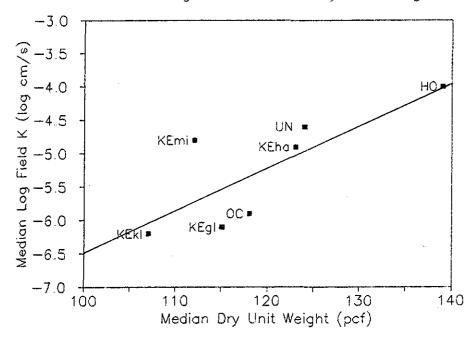
relationship has limited practical applications because medians and means are used. Despite this, the results of the statistical analysis can be used to predict field hydraulic conductivity from plastic limit. For example, the 95% confidence interval for a single hydraulic conductivity (median) value when (mean) plastic limit equals 17% ranges from 5.0×10^{-5} to 1.0×10^{-7} cm/s.

2. Hydraulic conductivity and dry unit weight

Hydraulic conductivity is intuitively related to dry unit weight (bulk density) because fluid flow requires permeability and porosity, and more porous soils are expected to be have lower bulk density. Porosity and hydraulic conductivity are commonly thought to be related, especially in granular porous media: porosity is included in the parameter 'C' in Darcy's equation and as 'n' in the Kozeny-Carmen and Fair-Hatch equations (Freeze and Cherry, 1979, pp. 27, 351).

I plotted median field hydraulic conductivity against median dry unit weight for each till unit with greater than five data values to determine whether such a relationship deserves further attention (figure 28). (Like many other parameters in the database, measurements of hydraulic conductivity and density are not paired.) The median dry unit weights are lower for finer grained till units with higher natural moisture contents, as suggested by figure 26b for sediments in the Oak Creek Formation. High porosity is associated with fine-grained materials but high porosity does not always result in greater values of hydraulic conductivity. High permeability is

Median Log Kf vs Median Dry Unit Weight



The regression equation is Log $K_f = -13.0 + (0.065 * dry pcf)$

Coef. Std. dev. of the Coef. t-ratio A
$$(y)$$
 -12.96 2.67 -4.85 B (x) 0.06 0.02 2.91 $R^2 = 62.8\%$ $R^2 (adj.) = 55.4\%$

The t value corresponding to 5 degrees of freedom and 95% confidence is 2.56.

Figure 28. Regression of median log hydraulic conductivity measured in the field on median dry unit weight for till units.

required in addition to high porosity for high hydraulic conductivity.

Figure 28 indicates that coarser-grained units have greater

permeability. The poor fit of the regressed equation confirms that

multiple variables influence the value of hydraulic conductivity.

According to straight-line linear regression results, 55% of the variation in median log hydraulic conductivity from field measurements can be explained by the fitted equation. As was the case for plastic limit, the regression of median log hydraulic conductivity on median dry unit weight has limited practical applications. For example, the 95% confidence interval for a single median hydraulic conductivity field measured value corresponding to a dry unit weight of 112 pcf ranges from 1.1×10^{-4} to 3.5×10^{-8} cm/s. A more narrow range of values can be predicted for the mean median log hydraulic conductivity at a given dry unit weight (Ryan, Joiner, and Ryan, 1985, p. 233).

3. Hydraulic conductivity and pocket penetrometer measurements

I also investigated the relationship between hydraulic conductivities measured in the field and pocket penetrometer measurements because pocket penetrometer data has been thought to indicate density. A similar correlation coefficient (r^2 =0.64) resulted from a straight line linear regression of the median log field hydraulic conductivity on the median pocket penetrometer measurement for till units. Despite the value of r^2 , statistical analysis (a t-test of the null hypothesis that B=0 (Ryan, Joiner, and Ryan, 1985, p. 292)) implies that the pocket penetrometer is not a

useful predictor of log hydraulic conductivities measured in the field.

H. Relationships between lithostratigraphic units and hydrostratigraphic units

Laney and Davidson (1986) discuss the definition of the hydrogeologic framework in much the same way as Mickelson *et al.*(1984) discuss the lithostratigraphic framework. Laney and Davidson write:

"In hydrogeologic studies, as in purely geologic investigations, the orderly, consistent designations of pertinent parts of the geologic framework is essential to a clear reporting and understanding of the study results. In ground-water studies, this involves definition and correlation of water-yielding rock materials, and relating those rock materials to established rock-stratigraphic units" (p. 9).

In this study, the hydrologic and geotechnical properties of till units were emphasized although data for both local and extensive sand and gravel bodies and till units were compiled.

Till units function as aquifers or aquitards depending on local conditions that frequently are a function of the unconformities and depositional environments noted in sections II-D and III-A. The till units are heterogeneous since hydraulic conductivity values at separate sites differ significantly within a single till and since a wide range of values is present at single sites.

Similarly, Feinstein and Anderson (1987) did not use formal lithostratigraphic units but did use genetic terms to define hydrostratigraphic units in Brown County, within the area glaciated by the Green Bay Lobe in late Wisconsin time. Feinstein and Anderson

divided till of single lithostratigraphic units into separate hydrostratigraphic units (clayey, loamy, or stony till; clayey or silty lacustrine; silty sand; sand, gravel, some silt) on the basis of piezometer tests of hydraulic conductivity. That approach was not possible for this study because the entire study area has not been mapped in the same detail as Brown County was by Need (1985). The lack of control over placement of piezometers also restricted application of this approach. Feinstein and Anderson combined Need's map units into hydrostratigraphic units.

I. Recommendations for sampling and testing procedures

Following Laney and Davidson's lead, I recommend that both geologic interpretation (genesis) and USCS classification be required on boring logs. The USCS can provide a common language for communication of observations if a standard reference is used, such as ASTM D2488-84 (ASTM, 1986, pp.411-424), and it provides information of interest to geotechnical engineers. The geologic interpretation is critical to inferences regarding the geometry of the materials. Use of the USCS alone to identify major soil layers and to determine the number of samples required means that two till units or a till unit and a clayey lacustrine unit could be present at one site, but only one would be sampled. Complete particle size analyses are necessary for geologic interpretation. Thorough description of samples, including notes on lithologies, structures, mottling, evidence of leaching, reaction, staining, and Munsell color would aid

identification of lithostratigraphic units considerably. Continuous sampling methods and continuous cores are preferable to split spoon samples at five foot intervals because continuous samples are more likely to indicate the presence of small sand layers affecting the flow of groundwater.

The variability of field measurements of hydraulic conductivity within one till requires further investigation. Error analysis of hydraulic conductivities requires documentation of sampling, measurement, and calculation methodology. Placement of the screened interval of a piezometer should be within only one genetic unit. Piezometers screened in silty or sandy sediments and finer-grained till units probably result in values of hydraulic conductivity representative of the non-till sediments. Until thorough error analysis of hydraulic conductivity tests has been completed, short piezometer screens located in one genetic unit are preferred. A carefully designed experiment should be completed to assess the effects of different field measurement techniques.

Several methods for the calculation of hydraulic conductivity from field tests require selection of data points and regression of a best-fit least-squares line. The selection of data points introduces individual bias to test results. Muldoon (1987) and Feinstein and Anderson (1987) calculate hydraulic conductivity between each recorded measurement during a field test, then report a geometric mean for the entire test. This reduces the subjectivity of data interpretation, but the method would be more resistant to the influence of very high

initial changes in head (possibly caused by the well screen's sand pack) if the median value rather than the mean is reported.

Throughout the data collection phase of this study, I was impressed with the number of borings completed at individual sites. I was also surprised by how few tests of hydraulic conductivity and complete grain size analyses are completed. Presumably, a large number of borings will provide data necessary to assess on-site stratigraphy, but the boring descriptions yield little information about hydraulic conductivity. The purpose of the geotechnical investigation is to determine the hydrogeologic setting and availability of suitable materials for landfill construction, but remarkably few hydrogeologic data results. This study indicates that there is a great deal of on-site variability, and the three values of hydraulic conductivity required by Wisconsin Administrative Code NR 180.13 for each major soil layer do not necessarily represent the range in hydraulic conductivity of a single stratum. Many of the data used in this study resulted from remedial action investigations at sites established prior to 1980. In modern waste disposal, the engineering design of sites is emphasized and relied upon to protect groundwater and surface water from contamination. These engineered sites have been in operation for a relatively short time and have provided geotechnical surprises in terms of gas build-up, leachate generation, and settlement. Incorporation of site-specific data into a more regional context can help resource managers anticipate problems at sites that otherwise seem to have nothing in common.

VI. Summary and Conclusions

A. Summary

This study was carried out in response to the long term objectives listed in the introduction. Compilation of the database used in this study addressed the first objective, to identify the hydrogeologic and geotechnical properties of Pleistocene materials in eastern Wisconsin. Hydraulic conductivity values, particle size analyses, Atterberg limits, approximations of strength, and dry unit weights have been compiled from reports on file at the Wisconsin Department of Natural Resources and assigned to one of five formations (one formation includes ten lithostratigraphic members) in eastern Wisconsin.

Association of the data with extensive lithostratigraphic units that have been associated with mapped ice margin positions partially meets the second objective—to associate the properties with mappable, extensive hydrostratigraphic units that can be identified in the field. The lithostratigraphic units are characterized with values of hydraulic conductivity, but are not divided into hydrostratigraphic units. No hydrostratigraphic units are designated because sources of data are not evenly distributed throughout the units and because an appropriate scale for the definition of hydrostratigraphic units has not been defined.

The data have been statistically analyzed to assess the variability and expected range of values within the individual till

units, accomplishing the third objective. Several till units are demonstrably heterogeneous, both with respect to grain size and to hydraulic conductivity, and statistically significant differences within a single till are documented.

The fourth objective is to develop field and laboratory methodologies for the evaluation of hydrogeologic and geotechnical properties in previously untested areas. Several recommendations follow the conclusions.

B. Conclusions

This study leads to the following general conclusions.

- 1. The quality of geotechnical investigations has improved in response to recent modifications of Wisconsin Administrative Code.

 However, the three values of hydraulic conductivity required by Wisconsin Administrative Code Chapter NR 180 for each major soil layer do not necessarily represent the range in hydraulic conductivity and grain size of a single stratum at a single site. This study indicates that more testing of samples is necessary for characterization of variability.
- 2. Field measurements of hydraulic conductivity in one of the most variable tills, the till in the Middle Inlet Member, range from 10^{-7} to 10^{-3} cm/s while less variable tills such as the till in the Haven Member range over only two orders of magnitude.
- 3. Median field measurements of hydraulic conductivity are at least an order of magnitude greater than laboratory measurements in fine-

grained till units. In coarse-grained till units, median field measurements of hydraulic conductivity are half an order of magnitude greater than the median laboratory measurements.

- 4. Compilation of geotechnical data makes it more accessible and provides a reference database. Incorporation of site-specific data into a more regional context can help resource managers anticipate problems at sites that otherwise seem to have nothing in common.
- 5. Particle size analysis to .002 mm is necessary for confident determination of sediment genesis. Geologists should provide complete grain size curves in addition to textural classification so that individuals familiar with other classifications can use geologic data. Textures of till samples from specific sites deviate from the published lithostratigraphic definition, but in some cases consideration of local sediment sources and glacial processes may explain the deviation.
- 6. Geotechnical index tests, such as Atterberg limits, can be used as lithic criteria to characterize lithostratigraphic units, but like other criteria used by geologists, can not distinguish lithostratigraphic units in all cases.
- 7. Atterberg limits plotted on plasticity charts do not distinguish till units from each other. Glacial sediments plot in elongate clusters on a plasticity chart. Most till units in the study are "inactive" and "solid," but some are "normal" and "plastic."
- 8. No meaningful relationships were found between standard penetration test data and depth or pocket penetrometer measurements.

The pocket penetrometer correlations found by previous investigators were not corroborated in this study.

- 9. Dry unit weight data may be used in calculations of void ratio, porosity, and average linear velocity of advective flow. A weak linear relationship exists between median log hydraulic conductivity measured in the field and median dry unit weight for till units.
- 10. Values of plastic limit may be used to constrain the predicted range in values of hydraulic conductivity measured in the field for till units.
- 11. Incorporation of more refined genetic terms into a geotechnical and hydrogeologic data base like the one used in this project could provide data for facies models and perhaps improve prediction of hydrogeologic conditions at sites prior to investigation.

C. Recommendations

- 1. All new data submitted to DNR for report approval should be compiled in a summary form similar to the database used for this study.
- 2. Data in geotechnical reports would be more easily accessed if boring locations were reported using a global coordinate system that follows simple, consistent rules of orientation. If only 3 points at each site had global coordinates, the remainder could be easily digitized.
- 3. More than one classification system (USCS, geologic, and possibly

- others) should be used to describe samples with standard terminology from a reference cited in Wisconsin Administrative Code.
- 4. Shorter piezometer screens should be installed to improve point measurements of hydraulic head and to avoid potential movement of contaminants between units. Piezometers should be screened in only one genetic unit.
- 5. Standard references for determining the hydraulic conductivity of undisturbed fine-grained samples in the laboratory should be developed if such tests continue to be used. Laboratory values of hydraulic conductivity are of questionable value to hydrogeologic assessments of *in-situ* conditions.
- 6. No improvement in the precision of hydraulic conductivity testing should be expected until the experimental error and variation in field tests has been analyzed. Without such an analysis, the variation in hydraulic conductivity values is usually attributed to variation in the materials tested. To test this assumption, a carefully designed experiment should be completed in which data are recorded from field tests that use different methods of lowering and raising the water level in correctly placed and constructed piezometers and different methods of recording the data (continuous strip recorders vs. taped measurements). If one aspect of the experiment is changed while holding all others constant, values of hydraulic conductivity could be statistically analyzed using two-way analysis of variance. The method of calculating hydraulic conductivity from field test data should be

standardized, and a variation of the method reported by Muldoon (1987) could be used.

7. A more refined definition of hydrogeologic units requires complete definition of the lithostratigraphy, particularly in the central portion of the Green Bay lowland (from Green Bay to south of Lake Winnebago). Units of extensive lake sediments and outwash should be mapped in the areas glaciated by the Green Bay and Lake Michigan lobes.

WORKS CITED

- Acomb, L. (1978). "Stratigraphic relations and extent of Wisconsin's Lake Michigan lobe red tills." M. S. thesis, University of Wisconsin-Madison.
- Acomb, L., D. Mickelson, and E. Evenson (1982). Till stratigraphy and late glacial events in the Lake Michigan lobes of eastern Wisconsin. *Geological Society of America Bulletin* 93, 289-296.
- Alden, W. (1918). "The Quaternary geology of southeastern Wisconsin."
 U. S. Geological Survey Professional Paper 106. Government
 Printing Office, Washington.
- American Society for Testing Materials (1986). "Annual book of ASTM standards." Volume 4: Construction. Volume 04:08 Soil and Rock; Building Stones (R. Stour et al., Ed.). American Society for Testing Materials, Philadelphia.
- Attig, J. (1985). "Pleistocene geology of Vilas County, Wisconsin." Information circular 50. Wisconsin Geological and Natural History Survey, Madison.
- Attig, J., L. Clayton, and D. Mickelson (1985). Correlation of late Wisconsin glacial phases in the western great lakes area. Geological Society of America Bulletin 96, 1585-1593.
- Baecher, G. (1984). Just a few more tests and we'll be sure! In "Probabilistic characterization of soil properties: bridge between theory and practice" (D. Bowles and H. Ko, Ed.), pp. 1-17. American Society of Civil Engineers, New York.
- Bain, J. (1971). A plasticity chart as an aid to the identification and assessement of industrial clays. Clay Minerals 9, 1-17.
- Baracos, A., J. Graham, B. Kjartanson, and D. Shields (1983). Geology and soil properties of Winnipeg. *In* "Special publication on geological environment and soil properties" (R. Yong, Ed.), pp. 39-56. American Society of Civil Engineers, New York.
- Boswell, P. (1961). "Muddy sediments: some geotechnical studies for geologists, engineers, and soil scientists." W. Hefner and sons, Cambridge.
- Boulton, G. and M. Paul (1976). The influence of genetic processes on some geotechnical properties of glacial tills. *Quarterly Journal of Engineering Geology* 9, 159-194.

- Bouwer, H. (1961). A double tube method for measuring hydraulic conductivity of a soil in situ above a water table. *Soil Science Society Proceedings* 25(5), 334-339.
- Bouwer, H. and R. Rice (1976). A slug test for determining hydraulic conductivity of unconfined aquifers with completely or partially penetrating wells. Water Resources Research 12(3), 423-428.
- Casagrande, A. (1932). Research on the Atterberg limits of soils. Public Roads 13(8), 121-136.
- Casagrande, A. (1947). Classification and identification of soils.

 Proceedings of the American Society of Civil Engineers 73, 783-810.
- Casagrande, A. (1948). Classification and identification of soils with discussion. *American Society of Civil Engineers Transactions* 113, 901-991.
- Chassefiere, B. and A. Monaco (1983). On the use of Atterberg limits on marine soils. *Marine Geotechnology* 5(2), 153-179.
- Chow, V., Ed. (1964). "Handbook of applied hydrogeology." McGraw-Hill, New York.
- Clayton, L. (1986). "Pleistocene Geology of Florence County,
 Wisconsin." Information circular 51. Wisconsin Geological and
 Natural History Survey, Madison.
- Clayton, L. (1986). "Pleistocene Geology of Portage County,
 Wisconsin." Information circular 56. Wisconsin Geological and
 Natural History Survey, Madison.
- Clayton, L. and S. Moran (1974). A glacial-process model. Chapter 3 in "Glacial geomorphology" (D. Coates, Ed.), pp. 89-119. Publications in Geomorphology, State University of New York, Binghamton.
- Connell, D. (1984). "Distribution, characteristics, and genesis of joints in fine-grained till and lacustrine sediment, eastern and northwestern Wisconsin." M. S. thesis. University of Wisconsin, Madison.
- Cooper, H., J. Bredehoeft, and I. Papadopulos (1967). Response of a finite-diameter well to an instantaneous charge of water. Water Resources Research 3(1), 263-269.

- Department of the Navy, Naval Facilities Engineering Command (1982).
 "Soil mechanics design manual 7.1." (NAVFAC DM 7.1) Government
 Printing Office, Washington.
- Dixon, H. (1974). Large dams and Dr. Karl Terzaghi In "Terzaghi memorial lectures on soil mechanics and foundation engineering" (S. Tezcan and A. Yalcin, Ed.), pp. 230 ff. Istanbul, Bogazici University Printing Office.
- Douglas, D. (1983). The standard penetration test. *In* "In-situ testing for geotechnical investigations" (M. Ervin, Ed.), pp. 21ff.
- Dreimanis, A. (1976). Tills: their origin and properties. *In* "Glacial till." Special publication 12, pp. 11-49. Royal Society of Canada, Ottawa.
- Dunn, I., L. Anderson, and F. Kiefer (1980). "Fundamentals of geotechnical analysis." John Wiley and Sons, New York.
- Evenson, E. B. and D. M. Mickelson (1974). A re-evalutation of the lobation and red till stratigraphy and nomenclature in part of eastern Wisconsin. *In* "Late Quaternary environments of Wisconsin" (J. Knox and D. Mickelson, Ed.), pp. 102-117. Wisconsin Geological and Natural History Survey, Madison.
- Eyles, N. and J. Sladen (1981). Stratigraphy and geotechnical properties of weathered lodgement till in Northumberland, England. Quarterly Journal of Engineering Geology 14, 129-141.
- Farrand, W., D. Mickelson, W. Cowan, and J. Goebel, Compilers (1984). Quaternary geologic map of the lake superior 4° x 6° quadrangle, United States and Canada. *In* "Quaternary geologic atlas of the United States" (G. M. Richmond and D. S. Fullerton, Ed.). Miscellaneous investigations series. U. S. Geological Survey, Washington.
- Farrar, D. and J. Coleman (1967). The corrlation of surface area with other properties of nineteen British clay soils. *Journal of Soil Science* 18(1), 118-124.
- Feinstein, D. and M. Anderson (1987). "Recharge to and potential for contamination of an aquifer system in northeastern Wisconsin."

 Technical Report WIS WRC 87-01. Water Resources Center,
 University of Wisconsin, Madison.
- Fleming, A. (1986). "The determination of joint system characteristics from azimuthal resistivity surveys." M.S. thesis. University of Wisconsin, Madison.

- Folk, R. (1958). Petrology of sedimentary rocks. Hemphills, Austin.
- Fookes, P., L. Hinch, M. Huxley, and N. Simons (1978). Some soil properties in glacial terrain—the Taff Valley, south Wales. In "The engineering behaviour of glacial materials." 2d edition, pp. 93-116. Geo Abstracts Limited, University of East Anglia, Norwich, England.
- Freeze, R. and J. Cherry (1979). "Groundwater." Prentice-Hall, Inc., Englewood Cliffs.
- Frye, J. and M. Willman (1960). "Classification of the Wisconsin Stage in the Lake Michigan lobe." Circular 285. Illinois Geological Survey, Urbana.
- Fulton, R. and V. Prest (1987). The laurentide ice sheet and its significance. Geographie physique et Quaternaire 41(2), 181-186.
- Gordon, M. and P. Huebner (1984). An evaluation of the performance of zone of saturation lanfills in Wisconsin. *In* "Seventh Annual Madison Waste Conference," pp. . Department of Engineering Professional Development, University of Wisconsin, Madison.
- Grim, R. (1962). "Applied clay mineralogy." McGraw-Hill Book Company, New York.
- Hansel, A., D. Mickelson, A. Schneider, and C. Larsen (1985). Late Wisconsinan and Holocene history of the Lake Michigan basin. *In* "Quaternary evolution of the great lakes" (P. Karrow and P. Calkin, Ed.), pp. 39-53. Geological Association of Canada; GAC Publications (distributor), Toronto.
- Herzog, B. and W. Morse (1984). A comparison of laboratory and field determined values of hydraulic conductivity at a waste disposal site. *In* "Seventh annual Madison waste conference," pp. 30-52. Department of Engineering and Applied Science, University of Wisconsin-Extension, Madison.
- Hoaglin, D., F. Mosteller, and J. Tukey (1983). "Understanding robust and exploratory data analysis." Wiley series in probability and mathematical statistics. John Wiley and Sons, Inc., New York.
- Houston, W. and A. Kasim (1982). Physical properties of geologic materials. *In* "Recent trends in hydrogeology," GSA special paper 189, (T. Narasimhan, Ed.), pp. 143-162. Geological Society of America, Boulder.

- Hvorslev, M. (1951). "Time lag and soil permeability in groundwater observations." Bulletin 36. U. S. Army Corps of Engineers Waterways Experiment Station, Vicksburg.
- Johnston, I. (1983). Why in-situ testing. *In* "In-Situ testing for geotechnical investigations" (M. Ervin, Ed.), pp. 1-19. AA Balkema, Rotterdam.
- Kenney, T. C. (1976). Formation and geotechnical characteristics of glacial-lake varved soils. In "Laurits Bjerrum memorial volume: contributions to soil mechanics" (N. Janbu, F. Jorstad, and B. Kjoernsli, Ed.), pp. 15-39. Norwegian Geotechnical Institute, Oslo.
- Laney, R. and C. Davidson (1986). "Aquifer nomenclature guidelines."
 U. S. Geological Survey Open-File Report 86-534. U. S. Geological Survey, Reston.
- Leighton, M. and M. Willman (1950). Loess formations of the Mississippi valley. *Journal of Geology* 58, 599-623.
- Lineback, J., N. Bleuer, D. Mickelson, W. Farrand, and R. Goldthwait, Compilers (1983). Quaternary geologic map of the Chicago 4° x 6° quadrangle, United States. *In* "Quaternary geologic atlas of the United States" (G. M. Richmond and D. S. Fullerton, Ed.). Miscellaneous investigations series. U. S. Geological Survey, Washington.
- Lo, Y. and G. McCabe (1984). Characteristics of Indiana soil properties. In "Probabilistic characterization of soil properties: bridge between theory and practice" (D. Bowles and H. Ko, Ed.), pp. 106-118. American Society of Civil Engineers, New York.
- Luttenegger, A., T. Kemmis, and G. Hallberg (1983). Origin and properties of glacial till and diamictons. *In* "Special publication on geological environment and soil properties" (R. Yong, Ed.), pp. 310-331. American Society for Civil Engineers, New York.
- May, R. W. and S. Thomson (1978). The geology and geotechnical properties of till and related deposits in the Edmonton, Alberta area. *Canadian Geotechnical Journal* 15, 362-370.
- McCartney, M. (1979). "Stratigraphy and compositional variability of till sheets in parts of northeastern Wisconsin." PhD. thesis. University of Wisconsin, Madison.

- McCartney, M. (1983). Stratigraphy of till sheets in part of northeastern Wisconsin. Geoscience Wisconsin 8, 1-21.
- McCartney, M. and D. Mickelson (1982). Late woodfordian and greatlakean history of the green bay lobes, Wisconsin. Geological Society of America Bulletin 93, 297-302.
- Mickelson, D., L. Acomb, N. Brouwer, T. Edil, C. Fricke, B. Haas, D. Hadley, C. Hess, R. Klauk, N. Lasca, and A. Schneider (1977).

 "Shore erosion study technical report: shoreline erosion and bluff stability along Lake Michigan and Lake Superior shoreline of Wisconsin." Wisconsin Coastal Management Program, Department of Natural Resources, Madison.
- Mickelson, D., L. Acomb, and T. Edil (1979). The origin of preconsolidated and normally consolidated tills in eastern Wisconsin, USA. In "Moraines and varves: origin/genesis/classification" (Ch. Schlucter, Ed.), pp. 179-187. Proceedings of an INQUA symposium on genesis and lithology. A. Balkema, Rotterdam.
- Mickelson, D., L. Clayton, R. Baker, W. Mode, and A. Schneider (1984).
 "Pleistocene stratigraphic units in Wisconsin." Miscellaneous
 paper 84-1. Wisconsin Geological and Natural History Survey,
 Madison.
- Mickelson, D. and E. Evenson (1974). Large scale involutions (convolutions? -pots?) in red till in the Manitowoc-Two Rivers-Two Creeks area of Wisconsin--periglacial features or load structures. *In* "Late Quaternary Environments of Wisconsin" (J. Knox and D. Mickelson, Ed.), pp. 182-186. Wisconsin Geological and Natural History Survey, Madison.
- Moran, S. (1971). Glaciotectonic structures in drift. *In* "Till/a symposium" (R. Goldthwait et al., Eds.), pp. . Ohio State Univerity Press, Columbus.
- Mudrey, M. Jr., B. Brown, and J. Greenberg (1982). "Bedrock geologic map of Wisconsin." University of Wisconsin - Extension, Geological and Natural History Survey, Madison.
- Muldoon, M. (1987). "Hydrogeologic and geotechnical properties of pre-late Wisconsin till units in western Marathon County, Wisconsin." M. S. thesis. University of Wisconsin, Madison.
- Murray, R. (1953). The petrology of the Cary and Valders tills of northeastern Wisconsin. *American Journal of Science* **251**, 140-155

- Nagaraj, T. and M. Jayadeva (1983). Critical reappraisal of plasticity index of soils. *Journal of Geotechnical Engineering* 110(9), 1367-1368.
- Need, E. (1985). "Pleistocene Geology of Brown County, Wisconsin." Information circular 48. Wisconsin Geological and Natural History Survey, Madison.
- Neuman, S. (1982). Statistical characterization of aquifer heterogeneities: an overview. *In* "Recent trends in hydrogeology," GSA Special Paper 189 (T. Narasimhan, Ed.), pp. 81-102. Geological Society of America, Boulder.
- North American Commission on Stratigraphic Nomenclature (1983). North American code of stratigraphic nomenclature. *American Association of Petroleum Geologists Bulletin* 67(5), 841-875.
- Odell, R., T. Thornburn, and L. McKenzie (1960). Relationships of Atterberg limits to some other properties of Illinois soils. Soil Science of America Proceedings 24(4), 297-300.
- Olson, R. and D. Daniel (1981). Measurement of the hydraulic conductivity of fine-grained soils. *In* "Permeability and groundwater contaminant transport," ASTM STP 746 (T. Zimmie and C. Riggs, Ed.), pp. 18-64, American Society for Testing Materials, Philadelphia.
- Papadopulos, S., J. Bredehoeft, and H. Cooper (1973). On the analysis of 'slug test' data. Water Resources Research 9(4), 1087-1089.
- Piette, C. (1963). "Geology of Duck Creek Ridges, east-central Wisconsin." M. S. thesis. University of Wisconsin, Madison.
- Quigley, R. (1980). Geology, mineralogy, and geochemistry of Canadian soft soils: a geotechnical perspective. *Canadian Geotechnical Journal* 17, 261-285.
- Raukas, A., D. Mickelson, and A. Dreimanis (1978). Methods of till investigations in Europe and North America. *Journal of Sedimentary Petrology* **48(1)**, 285-294.
- Richards, A. (1976). Marine geotechnics of the Oslofjorden region.

 In "Laurits Bjerrum memorial volume: contributions to soil mechanics" (N. Janbu, F. Jorstad, and B. Kjoernsli, Ed.), pp. 41-63. Norwegian Geotechnical Institute, Oslo.
- Richmond, G. and D. Fullerton (1986). Introduction to Quaternary glaciations in the United States of America. *Quaternary Science Reviews* 5, 3-10.

- Rodenbeck, S., W. Simpkins, K. Bradbury, and D. Mickelson (1987).

 Merging geotechnical data with Pleistocene lithostratigraphy—
 examples from eastern Wisconsin. *In* "Tenth annual Madison waste conference" pp. 454-467. Department of Engineering Professional Development, University of Wisconsin, Madison.
- Ryan, B., B. Joiner, and T. Ryan, Jr. (1985). "Minitab Handbook." 2d edition. Duxbury Press, Boston.
- Scarrow, J. (1985). "A study of the slug test method for determining hydraulic conductivities." Unpublished independent study project for M. S., Dept. of Civil Engineering, University of Wisconsin, Madison.
- Schneider, A. and E. Need (1985). Lake milwaukee: an "early" proglacial lake in the Lake Michigan basin. *In* "Quaternary evolution of the great lakes" (P. Karrow and P. Calkin, Ed.), pp. 55-62. Geological Association of Canada; GAC Publications (distributor), Toronto.
- Scott, J. and D. St-Onge (1969). "Guide to the description of till."
 Paper 68-6. Geological Survey of Canada, Department of Energy,
 Mines, and Resources. The Queen's Printer, Ottawa.
- Singh, P., S. Tatioussian, and C. Flagg (1983). A study of the geotechnical properties of Milwaukee area soils. *In* "Special publication on geological environment and soil properties" (R. Yong, Ed.), pp. 269-309. American Society of Civil Engineers, New York.
- Skempton, A. and R. Northey (1952). The sensitivity of clays. Geotechnique 3(1), 203-208.
- Soil Survey Staff (1981). Examination and description of soils in the field. Chapter 4 (Supplement issued in May, 1981 replaces previous Chapter 4). In "Soil Survey Manual." USDA Agriculture Handbook no. 18. U. S. Department of Agriculture, Washington.
- Stroud, M. and F. Butler (1978). The standard penetration test and the engineering properties of glacial materials. *In* "The engineering behavior of glacial materials." 2d edition, pp. 117-128. Geo Abstracts Unlimited, University of East Anglia, Norwich, England.
- Terzaghi, K. (1955). Influence of geological factors on the engineering properties of sediments. *In* "50th anniversary volume of economic geology" (A. Bateman, Ed.), pp. 557-618. Economic Geology Publishing Co., Lancaster.

- Thwaites, F. (1943). Pleistocene of part of northeastern Wisconsin.

 Bulletin of the Geological Society of America 54, 87-144.
- Thwaites, F. and K. Bertrand (1957). Pleistocene geology of the Door Peninsula, Wisconsin. Bulletin of the Geological Society of America 68, 831-880.
- Uehara, G. and G. Gilman (1981). "The mineralogy, chemistry, and physics of tropical soils with variable charge clays." Westview tropical agriculture series no. 4. Westview Press, Boulder.
- United States Environmental Protection Agency (1987). "Wellhead protection: a decision-maker's guide." Office of Groundwater Protection, United States Environmental Protection Agency. US EPA, Washington.
- Walpole, R. and R. Myers (1978). "Probability and Statistics for Scientists and Engineers." 2d edition. Macmillan Publishing Co., New York.
- White, G. (1973). History of investigation and classification of Wisconsinan drift in north-central United States. *In* "The wisconsinan stage" (R. Black, R. Goldthwait, and H. Willman, Ed.), pp. 3-34. GSA Memoir 136. Geological Society of America, Boulder.
- White, G. (1974). Buried glacial geomorphology. Chapter 13 in "Glacial geomorphology" (D. Coates, Ed.), pp. 331-349. Publications in Geomorphology, State University of New York, Binghamton.
- White, W. (1949). Atterberg plastic limits of clay minerals. American Mineralogist 34, 508-512.
- Willman, H. and J. Frye (1970). "Pleistocene stratigraphy in Illinois." Bulletin 94. Illinois Geological Survey, Urbana.
- Wisconsin Administrative Code.
- Yong, R. and B. Warkentin (1975). "Soil properties and behaviour."

 Developments in geotechnical engineering 5. Elsevier Scientific Publishing Company, New York.

Appendix 1 Data required by Wisconsin Administrative Code

NR 51.10 (1)(c) states that

"A report shall accompany the plans indicating: . . . (3) Geological formations and ground water elevations to a depth of at least 10 feet below proposed excavation and lowest elevation of the site. Such data shall be obtained by soil borings or other appropriate means."

The same phrasing was used in NR 151.10(1)(c); apparently, only the numbering was changed.

NR 151.12(5) (1976) indicates growing concern in the Department of Natural Resources and reflects the influence of federal and state statutory laws. The requirements for geotechnical information are more specific:

NR 151.12(5)(c): "An acceptable report on geological formations based on soil borings. The minimum number of borings to be taken is based on site size according to the following schedule:

- 3 borings for a site of up to 5 acres in size.
- 2. 1 boring for each additional 5 acres or portion thereof up to 50 acres
- 3. 1 boring for each additional 10 acres or portion thereof over 50 acres.

Borings shall be arranged as nearly as possible to form a grid pattern over the site, to provide a subsurface investigation representing the entire site, and to facilitate analysis. When information is insufficient to adequately evaluate the site, additional deeper borings may be required. All borings shall extend to a depth of at least 15 feet below the lowest proposed elevation of waste disposal in the areas of the borings. Boring holes shall be refilled with a bentonite-earth slurry prior to disposal of solid waste." (Register, June 1976, No. 246, Environmental Protection, p. 118-2)

Both NR 51 and NR 151 required only one phase of investigation prior to site development. As the expense of more detailed investigations became a factor, the code changed to require two phases of investigation—initial site reports (ISRs) and feasibility reports,

completed at different levels of detail--prior to approval and prior to further investment in the proposed site.

NR 180 (1980) requires that submitted ISRs and feasibility reports be prepared in the following manner: under the direction of a registered professional engineer, using standard procedures approved by the department, in a standard format, using a site-specific grid and containing appendices listing all references, all necessary data, procedures, and calculations (Register, February, 1980, No. 290, Environmental Protection, pp.686-9 to 10). Both initial site and feasibility reports must contain regional geotechnical information including topography, hydrology, geology, hydrogeology, and water quality (Register, March, 1984, No. 339, Environmental Protection, p. 686-34). The code clearly states the minimum field and lab investigations required for a feasibility report:

NR 180.13(6)3a: "Sufficient soil borings to adequately define the soil, bedrock, and groundwater conditions at the site. Under most site conditions, 5 soil borings for the first 5 acres and 3 borings for each additional 5 acres or portion thereof should be performed. A lesser number of borings may be made based on specific site conditions and site design. The borings shall be located in a grid pattern such that there is a minimum of one boring in each major geomorphic feature (e.g. ridges, lowlands and drainage swales). All borings shall extend a minimum of 25 feet below the anticipated site base grade or to bedrock, whichever is less."

NR 180.13(6)3b.: "Where soil conditions permit, soil samples shall be collected utilizing standard undisturbed soil sampling techniques. Samples shall not be composited for testing purposes. Soil samples shall be collected from each major soil layer encountered and at maximum 5-foot intervals. All soil samples shall be described."

NR180.13(6)3c.: "Boring logs shall be recorded for all borings. Each log shall include soil and rock descriptions and method of sampling, sample depth, date of boring, water level measurements and dates, and soil test data. All elevations shall be corrected to USGS datum."

NR180.13(6)3d.: "For each major soil layer encountered, at least 3 soil samples shall be analyzed for grain size distribution (mechanical and/or hydrometer as appropriate to the soil type) and classified according to the unified soil classification system."

NR180.13(6)3e.: "A minimum of 3 permeability tests shall be conducted for each major soil layer. At least one of the 3 tests shall be performed utilizing in-field testing procedures."

NR180.13(6)4a.: "All raw data such as boring logs, well logs, soil tests and water level measurements shall be included in the report appendix."

(Register, February, 1980, No. 290, Environmental Protection, pp. 686-36 to 686-37)

In addition to the data collection outlined above, the BSWM requires an investigation to document the availability of a suitable fine-grained material for use as a recompacted liner if no fine-grained sediment is available on-site. These "clay liner investigations" typically include boring logs of the same quality as required for feasibility reports and complete grain size analyses.

Appendix 2 Location summary by site: latitude and longitude

Site	minimum	maximum	minimum	maximum	default	default
#	latitude		longitude	longitude	latitude	longitude
-			•	_		
1	443021	443029	875010	875045	443099	875099
2	443041	443103	880913	880940	443099	880999
3	442409	442439	880019	880059	442499	880099
4	443142	443153	875949	880016		
5	440609	460619	881128	881137		
6	430434	430445	891142	891156		
7	430105	430131	892007	892055		
8	431854	432333	885133	890145	432399	885299
9	432729	432808	883304	883335		
10	445145	445150	872638	872709	_	
11	452305	452310	835608	865304	452399	865399
12	434917	434932	883138	883201		
13	435728	435744	885426	885452	435799	885499
14	423506	423550	880213	880247		
15	442822	442835	873440	873515		
16	441004	441046	874937	875012	441099	874999
1'7	451411	451429	880532	880542	451499	880599
18	not ass:	igned				
19	434703	434716	892841	892858		
20	425007	425031	875017	875052	425099	875099
21	425037	425112	880329	880410	425199	880499
22	445142	445154	880923	880940		
23	443921	445026	880602	881027		
24	441717	441755	882003	882107	441799	882199
25	432141	432151	875427	875429		
26	432539	432600	875104	875121		
27	432647	432702	875138	875156		
28	424218	424240	875120	875154		004400
2 9	432041	432247	894250	894557	432199	894499
30	444608	444821	883330	883345	444699	883399
30	(Clay so				444899	883699
31	434136	434157	874703	874725		
32	424529	424610	882440	882511	424699	882599
33	413918	423910	884305	884329	423999	884399
34	431744	431756	881128	881158	404400	000400
35	431115	431157	880315	880453	431199	880499
36	431747	431755	881037	881041		
37	430245	450258	880847	880911		
38	442621	442630	885822	885837		
39	442017	442034	885655	885706	4.40500	000000
40	440500	440523	883215	883327	440599	883399
41	470330	470354	883327	883407	470399	883499

41-49 no	t assigned.	Bill	Simpkins	provided	data	for	sites	50-55
50	425145	425216	875041	. 87510	6			
51	425206	425215	875245	87525	8			
52	425503	425524	875152	87520	1			
53	425115	425131	880246	88045	2			
54	425005	425029	875019	87505	0			
55	425324	425356	881029	88110	9			

Appendix 2 Location summary by site: topographic quadrangle,

section, township, & range

County	Site Site name	7.5' map name	Sec., Township, & Range
Brown	1 Baeton	New Franken	Sec 33, T24N, R22E
Brown	2 Decaster	Oneida North	Sec. 25 & 26, T24N, R19E
Brown	3 Decleene	DePere	Sec 1 & 6, T23N, R20&21E
Brown	4 Northland Sludge	Green Bay E and W	T24N, R21E
Calumet	5 Calumet Co. LF	Chilton	Sec. 23, T19N, R19E
Dane	6 Hydrite Chemical Corp	Cottage Grove	Sec. 16, T7N, R10E
Dane	7 Libby Road	Madison East	Sec. 32, T7N, R10E
Dodge	8 Carl Schmitt	Lost Lake	Sec. 30, T11N, R14E
Dodge	9 Hechimovich & clay source		Sec. 35, T12N, R16E
Door	10 Door Co Balefill	Sturgeon Bay West	Sec. 34, T28N, R25E
Door	11 Town of Washington	Washington Island NW	Sec 32, T34N, R30E
Fond du Lac	12 Eldorado	Eldorado	Sec 25, T16N, R16E
Green Lake	13 Green Lake Co. LF	Berlin	Sec 11, T17N, R13E
Kenosha	14 Pheasant Run	Paddock Lake	Sec. 32, T2N, R21E
Kewaunee	15 Kewaunee Co LF	Kewaunee	Sec. 9, T23N, R24E
Manitowoc	16 Lemberger	Whitelaw	Sec. 26, T20N, R22E
Manitowoc	16 Proposed Co. LF	Whitelaw	Sec. 26, T20N, R22E
Manitowoc	16 Ridgeview	Whitelaw	Sec. 26, T20N, R22E
Marinette	17 Proposed Co. LF	Crivitz	Sec. 23, T32N, R19E
rada arrocco	18 not assigned	OLIVICE	20, 1027, 1402
Marquette	19 Marquette Co LF	Packwaukee	Sec. 8, T15N, R9E
Racine	20 Caledonia (WEPCO)	Racine North	Sec 1, T4N, R22E
Milwaukee	21 Metro	North Cape	Sec 31, T5N, R21E
Oconto	22 City of Oconto Falls	Oconto Falls South	Sec. 35, T28N, R19E
Brown	23a Oconto Co LF	Pulaski	Sec. 11, T25N, R19E
Oconto		Abrams	Sec 5, T27N, R20E
Oconto	23c Oconto Co. LF	Pulaski	Sec 35, T26N, R19E
Outagamie		Kaukauna	Sec. 7, T21N, R18E
Ozaukee	25 Anderson ISR	Cedarburg	Sec 5, T10N, R22E
Ozaukee		Port Washington East	Sec. 10, T11N, R22E
Ozaukee		Port Washington East	Sec. 4, T11N, R22E
Racine		Racine South	Sec. 23, T3N, R22E
Sauk		Baraboo	Sec. 6, T10N, R7E
Sauk	_ ·	Sauk Prairie	Sec. 14, T10N, R6E
Sauk		Sauk City	Sec. 1 & 14, T10N, R6E
Shawano		Shawano	Sec. 19 & 33, T27N,R16E
Sheboygan		Sheboygan Falls	Sec. 7, T14N, R23E
Walworth	-	East Troy	Sec. 31, T4N, R18E
Walworth	-	Delavan	Sec. 4 & 9, T2N, R15E
Washington			Sec. 25, T10N, R19E
Washington			Sec. 36, T9N, R20E
Waukesha	-		Sec. 1, T8N, R20E
Washington			Sec. 30, T10N, R20E
Waukesha			Sec. 20, T7N, R20E
Waupaca	_		Sec. 30, T23N, R13E
Waupaca Waupaca	_		Sec. 32, T22N, R13E
naupaca	OB TOWN OF MONATION	Weyawauga	OCC OC, IZZIV, INJOE

Winnebago	40 Bartlett	Oshkosh	Sec. 26, T19N, R16E
Winnebago	41 Winnebago Co. LF	Oshkosh	Sec. 2 & 3, T18N, R16E
Milwaukee	50 Bender Park	Racine North	Sec. 25, T5N, R22E
Milwaukee	51 Derosso ISR	Franksville	Sec. 27, T5N, R22E
Milwaukee	52 Falk LF	S. Milwaukee	Sec. 2, T5N, R22E
Waukesha	53 Future Parkland	North Cape	Sec. 36, T5N, R20E
Milwaukee	54 WEPCO2	Racine North	Sec. 1, T4N, R22E
Milwaukee	55 Muskego	Muskego	Sec. 18, T5N, R20E

Bill Simpkins collected data for sites 50-55. ISR stands for initial site report. LF stands for landfill.

APPENDIX 3 DATA REFERENCES AND DATA

Site 1

Donohue and Associates, Inc. (1980). Initial site report for Wisconsin Public Service Baeton Site STS Job 81085.

Donohue and Associates, Inc. (1982). Feasibility report for Wisconsin Public Service Baeton Site. STS Job 11119-A.

Site 2

Robert E. Lee and Associates (1973). Soils investigation for cell DC 3.

(1974). Soils investigation for cells DC 4 and DC 5.

Soils Testing Services, Inc. (1978). Soils report for Module 2. Job 8929.

Foundation Engineering, Inc. (1976) Subgrade and earth berm data and in place subgrade data. Job FE 76157

Foundation Engineering, Inc. (1979) Northern periphery of module 1 and southern periphery of module 2. Supplemental soils investigation. Job 7913.

Site 3

Brown County Brown County East Landfill monitoring well inventory.

Soil Testing Services (1983) Plan of Operation Approval Conditions.

Robert E. Lee and Associates (1984). Plan of Operation.

Site 4

Soils Testing Services, Inc. (198)

Site 5

Robert E. Lee and Associates, Inc. (1981). Calumet County initial site report - Behnke property. STS borings, Job 11513.

(1982) Calumet County feasibility report - Behnke property SIS Job 11513A

Site 6

Warzyn Engineering, Inc. (1982). Preliminary in-field conditions report Hydrite Chemical Company solvent processing facility, Cottage Grove, Wisconsin. Includes data from jobs C9555 and C10497

Warzyn Engineering, Inc. (1983). Phase II subsurface investigation Hydrite Chemical solvent processing facility, Cottage Grove, Wisconsin. Job C10834.

Warzyn Engineering, Inc. (1984). Report to Hydrite dated Jan. 9, 1984 including pump test results from Roy F. Weston, Inc.

Site 7

Residuals Management Technology, Inc. (1986). Madison Landfills, Inc. - Libby site

Site 8

Warzyn Engineering, Inc. (1984) Feasibility study Job C10863

Warzyn Engineering, Inc. (1982). Addendum to the initial site report. Job C9670B.

Warzyn Engineering, Inc. (1981). Initial site report. Job 9670.

Warzyn Engineering, Inc. (1985). Clay soils investigation, Carl Schmidt landfill, Town of Lowell, Dodge County, Wisconsin. Job 10863.

Site 10

Soil Testing Services of Wisconsin, Inc. (1980) Hydrogeologic study for proposed Door County landfill STS Job 8774

Robert E. Lee and Associates (1979). STS borings.

Becher-Hoppe Engineers, Inc. (1973). Idlewood project, Sturgeon Bay, Wisconsin. STS borings.

Site 11

Becher-Hoppe Engineers (1977). STS grain size analyses, 1976-1977.

Site 12

Foth and Van Dyke and Associates, Inc (1983) Feasibility study, Job FU 8301 Twin City Testing logs

Foth and Van Dyke and Associates, Inc. (1985) Addendum to the Feasibility study. Job FU 8301 Twin City Testing logs

Site 13

Foth and Van Dyke and Associates, Inc. (1982) Feasibility report for the proposed Green Lake Landfill, Inc. horizontal expansion

Foth and Van Dyke and Associates, Inc. (1983) Green Lake Landfill Feasibility Report Additional Information.

Residuals Management Technology, Inc. (1985). Green Lake sanitary landfill south and east expansion no. 1, NR 180.13 feasibility study prepared for Green Lake Landfill Company, Inc.

<u>Site 14</u>

Warzyn Engineering, Inc. (1985) Feasibility for northern expansion area of Pheasant Run sanitary landfill, Waste Management of Wisconsin, Inc. Job C12812 and 10812

Residuals Management Technology, Inc. (1978) In-field conditions and feasibility study for site expansion and partial abandonment of a landfill site owned by Keno Trucking, Inc.

Site 15

Robert E Lee and Associates, Inc. (1981) Kewaunee County solid waste management system balefill and processing facility feasibility report. STS job 10877

Robert E. Lee and Associates, Inc. (1982) Report of "as-built" conditions STS Job 10877.

Site 16

Residuals Management Technology, Inc (1981) Lemberger landfill site, horizontal expansion, feasibility report

Residuals Management Technology, Inc. (1980). Revised in-field conditions analysis and addendum to the site operations plan for the Lemberger landfill in the W 1/2, Sec. 26, T20N, R22E, Town of Franklin, Manitowoc County, Wisconsin. STS Job 5858E.

Foth and Van Dyke and Associates, Inc. (1983) Ridgeview regional sanitary landfill horizontal expansion - plan of operation, Town of Franklin, Manitowoc County, Wisconsin Volume I Design report/operations manual Volume II Appendices Prepared for Waste Management of Wisconsin, Inc.

Site 17

Foth and Van Dyke and Associates, Inc. (1981). Feasibility report for the proposed Marinette County sanitary landfill. STS Job 11330.

Foth and Van Dyke and Associates, Inc (1981) Initial site report for the proposed Marinette County sanitary landfill Giles Engineering Associates, Inc. job #810118

Site 19

Warzyn Engineering, Inc. (1980). Documentation of partial site preparations Marquette County sanitary landfill. Job C7204B.

Warzyn Engineering, Inc. (1978). Supplemental subsurface investigation proposed sanitary landfill site, section 18, T15N, R9E, Packwaukee, Marquette County, Wisconsin. Job 7284.

Site 20

Wisconsin Electric Power Company, Inc. (1985) Ash disposal feasibility report, Caledonia site, Town of Caledonia, Racine County, Wisconsin.

Site 21

Warzyn Engineering, Inc. (1981) Bound reference file feasibility data

Warzyn Engineering, Inc. (1982). Western expansion feasibility study, Metro landfill development project, Franklin, Wisconsin. Job C11272

Hydrosearch, Inc (1986) Hydrogeologic characterization and ground water quality program, Metro landfill and development project, Franklin, Wisconsin, Phase II

Hydrosearch, Inc. (1985). Hydrogeologic characterization and ground-water assessment program, Metro landfill and development project, Franklin, Wisconsin. Phase I.

Site 22

Soil Testing Services, Inc. (1986) Remedial action study City of Oconto Falls landfill Project #13682

Site 23

Foth and Van Dyke and Associates, Inc. (1984). Feasibility report for the Oconto County sanitary landfill.

Site 24

Donohue and Associates, Inc. (1986) Outagamie County landfill, Outagamie County, Wisconsin, groundwater investigation, Vol. I

Donohue and Associates, Inc. (1983) Landfill feasibility investigation for east landfill site expansion.

Donohue and Associates, Inc. (1983) Landfill feasibility investigation for east landfill site expansion (revised)

Donohue and Associates, Inc. (1981). Cell specific geotechnical report, Outagamie County, sanitary landfill expansion site.

Twin City Testing. Letter to Mr. Michael Marsden, Sept. 2, 1981. Subject: Field and laboratory tests, landfill expansion Outagamie County.

Twin City Testing Letter to Mr Michael Marsden, Sept 29, 1981 Subject: Field and laboratory tests second report landfill expansion Outagamie County

Donohue and Associates, Inc. Letter to Mr. Peter Kmet, August 4, 1980. Subject: 2nd addendum to 1979 feasibility. (Job 40021.0)

Donohue and Associates, Inc. Letter to Mr. Peter Kmet, March 26, 1980. Subject: Outagamie County landfill site expansion (Job 40021.0)

Donohue and Associates, Inc. (1979) Site feasibility and design investigations, Outagamie County, Wisconsin, sanitary landfill expansion plan

Site 25

Robert E. Lee and Associates, Inc. (1981). Ozaukee County, initial site report, Anderson property.

Site 26

Robert E. Lee and Associates, Inc (1982). Ozaukee County, initial site report, Didier property.

Site 27

Robert E. Lee and Associates, Inc. (1984). Ozaukee County, initial site report, WEPCO property.

Site 28

Mead and Hunt (1976). Hydrogeologic feasibility study.

Residuals Management Technology, Inc. (1981). Addendum to the feasibility study for Land Reclamation, Ltd.

Foth and Van Dyke and Associates, Inc. (1985) Initial site report (expansion)

Site 29

Warzyn Engineering, Inc. (1982). Geological and soils survey and groundwater monitoring program, Badger Army Ammunition Plant

Site 30

Nordin, S. and R. Pedersen (1985). Plan of operation, Shawano landfill, Phase 2, Shawano, Wisconsin.

Pedersen, R. W. (1984). Remedial action plan, Shawano landfill - Phase I, Shawano, Wisconsin.

Pedersen, R. W. (1984) Feasibility report, Shawano landfill, Phase 2 expansion (revised)

Pedersen, R. W. (1983). Feasibility report, Shawano landfill, Phase 2 expansion.

Site 31

Donohue and Associates, Inc. (1981). Initial site report for sanitary landfill, Bock/Grieg property, Town of Wilson, Sheboygan County, Wisconsin.

Donohue and Associates, Inc (1982). Landfill feasibility investigation former Bock/Grieg site, Town of Wilson (revised 1984).

Site 32

Residuals Management Technology, Inc. (1982) Troy area landfill, NR 180.13 feasibility report for the Troy area landfill located in Sec. 31, T4N, R18E, Town of East Troy, Walworth County, Wisconsin

Residuals Management Technology, Inc. (1986). Troy Area Landfill, Inc. plan of operation.

Site 33

Foth and Van Dyke and Associates, Inc. (1983). Plan of operation: Greidanus Enterprises, Inc. sanitary landfill horizontal expansion

Foth and Van Dyke and Associates, Inc. (1983). Initial site report for the proposed northeast landfill expansion, Greidanus Enterprises, Inc., Walworth County, Wisconsin.

Residuals Management Technology, Inc. (1982) Feasibility report horizontal expansion to the existing Greidanus Enterprises, Inc. Landfill, Walworth County

Warzyn Engineering, Inc. (1978) Additional feasibility information proposed Greidanus sanitary landfill expansion

Warzyn Engineering, Inc. (1977) In-field conditions report and geologic study, Greidanus landfill site, Delavan, Wisconsin

Site 34

Robert E. Lee and Associates, Inc. (1981). Washington County initial site report, Mertens property.

Site 35

Warzyn Engineering, Inc. (1983). Supplemental investigation for the design of reparative measures, Omega Hills North Landfill and recreational development project.

Warzyn Engineering, Inc. (1983) Design of environmental improvements, county line road and A-1 areas Omega Hills North landfill and development project

Warzyn Engineering, Inc. (1982). Omega Hills North In-field conditions report, Omega Hills Landfill and recreational development project.

Warzyn Engineering, Inc. (1981). Summary report, Omega Hills Landfill and recreational development project. Waste Management of Wisconsin, Inc., Village of Germantown, Washington Co., Village of Menominee Falls, Waukesha County, Wisconsin.

Warzyn Engineering, Inc (1986) Environmental improvements northwest sand seam/northern triangle Omega Hills North landfill, Germantown, Wisconsin

Warzyn Engineering, Inc. (1985). Northern area investigation, Omega Hills North Landfill.

Warzyn Engineering, Inc. (1985). Conceptual plan modification proposal, Omega Hills South Landfill, Waste Management of Wisconsin, Inc., Village of Menominee Falls, Wisconsin.

Site 36

Robert E. Lee and Associates, Inc. (1981). Washington County initial site report, Schowalter property.

Site 37

Warzyn Engineering, Inc. (1983) Brookfield sanitary landfill interim groundwater investigation

Emcon Associates (1976). Geotechnical investigation, Brookfield sanitary landfill, Waukesha County, Wisconsin.

Site 38

Donohue and Associates, Inc. (1984) Landfill feasibility report, Kempf property - Town of Little Wolf, Waupaca County, Wisconsin.

Site 39

Donohue and Associates, Inc. (1982). Initial site report Waupaca County property -Town of Royalton, Waupaca County, Wisconsin.

Site 40

Donohue and Associates, Inc. (1985). Landfill feasibility report Bartlett property -Town of Oshkosh, Winnebago County, Wisconsin. 3 Volumes.

Donohue and Associates, Inc. (1985) Bartlett property - Town of Oshkosh, Winnebago County, Wisconsin (initial site report)

Site 41

Soil Testing Services of Wisconsin, Inc. Data from Jobs 7801A (1977) through 7801K (1982).

	11111	į							•	HYDRAUL IC	į		+ GRAINSI	GRATINSTZE PERCENTABES	WEES		+ ENGINEERING PROPERTIES	340AG SMI	RTIES			
	ctrate	ģ +				ű	, in	6,44,7	+ * * * * * * * * * * * * * * * * * * *	EMEDICINALLY	Ě			Matrix X	Hatrix X Matrix X	Matrix 1	•					
+ County + (code) Y	unit Tear (code	* County unit Mat. Site * (code) Year (code) (code) Mo.		-	8	Brno. E		3 5	bottog +	Lab K	Seth	Fld K Reth	+ Bulk I (2.0 to			(0.0625 to	. Seite	_	Percent Boit Wt.	SPT Moist, Liquid Plastic. UC	Liquid Pia	stic. EC
2	1904 7561		•	1				:	١.					100000		700.00	i	į	rage.	UN COST. IL) INDIT		Juger (151)
					67500	5 2		9	e :				٠.,				đ			×		2.5
-					075045	āā		9.0	2.5				e ¹ C				ದ (\$		4.5
			F 3		015016	ä :		2.5	?				•				ದ					÷
		2 .		200	73042	2	Ė	2	C.12				•	≏	÷	8	ద	8		25		3
- ·	IVEN ACEL		.		2/2042	= ;	-	0	£1.12 12.13 13.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13 14.13								ದ			ន		5:0
_	2	٠. ت	. .		2000	=		8	5.5								ਰ			=		2:
		- ·	¥ :	113048	875045	#	3E.	S.	36.5								平 5			r		
- ·		→ •	∓ ∶		875045	=	7.1	0.0 4	4 0.5								25- 25-			90		
_			¥ -,		875010	껉	¥.	5.0									겁			×		7
_		** **	-		875010	껉	¥.3	20.0	30.5								겁			209		-
-	28 28 28	~	=		875010	멅	78.3	15.0	16.0				•	=	2	Ŧ	. C	26		200		
			¥		B75 016	絽	798.3	20.0	21.5							:	2			,		
墨			¥		B75010	2	788.3	22	26.5								2			; x		: -
西	193X 9861	25	Ŧ		875010	2	798.3	39.0	31.5								3 2			3 5		
¥		F (5)	∓		875616	2	2	Ę	4								3 2			3 8		: :
		→	=		875010	2	708.7	3									3 E			9		-
	1980 KES3		-		875.028	2	,		*								5 5 5 2			250		•
	1980 KF61		* *	447074	875/78	2 5	,	•	, ,								# ·			2		en.
	•	· ·			75038	2 2	701	2 4	777								nd ä					
					07440	2 3		9	?				i				9-15- 1					
		, - 5 =		0 12v217	075020	2 =		2 2	C 2				£5				\$P. ₩			2		
_	086				20.5	2 %		3 5	, t								9-8			8		
				443614 8	875028	2	,	,	. 5								3 2			3 ;		
	1980		=		875078	1 5	2	9	· ·								# 15 K			8 8		
				443622 B	875045	Z	788.8	4	2 4											700		٠
	1980 KE	· M	=		\$1504S	ä	90	9	; <u>;</u>								3 2			3 ;		⇒ i
	980 KFS1			ALTERNA	875A45	. 2	300		2 4								ಶ ಕ			73 1		3.5
					975745	6 8	100.0	2 6	2 2								5			e :		
-		· ·			075015	5 2	360.0	2 7	7								5,5			142		
-		· M	- 17		27070	6 2	100	,	20.5				\$				5. S.			2		
	98			20071	BYSASS	ā	700.0	2 4					77				Z .	7		280		
			. 3		875015	: 2	9	į	;								e c	_		ĝ		
		. M			875015	*	9	•									3 2					€.
	1980 KE			443022 8	875615	×	008	9									ತ ಕ					
		2	. .		B75015	2	800	8									3 2					
*	1980 KES1	81 3	∓		875015	2	890.9	5	10.0	2.285-08			•	8	5	×	5 2	7			-	;
-		61 3	¥	_	875015	22	800	10.0	11.5				•	1	•	3	\$ 5					-
_		Si 3	∓ 		875015	ĸ	900.9	15.0	16.5								3 2			Ş		;
-		61	-		875015	20	800.9	30.0	21.5								3 2			* F		-
_		53	¥		875015	22	800.9	2	27.0	395-08			•	=	4	7	\$ 2	· 5		9		- :
		61 3	∓		875015	47	9	S	2				•	:	‡	=						: <
蓋		25	∓		875015	82	900.4	35.0	37.0								7 T	_				
-		2	¥ •		875015	22	900	40.0	₹.5								3 3			2		
_	1982 KEB1	23	¥ .		835042	416	782.3	0.5	9									_		2		
-	1982 KEE1	61 3	-	H3017 B	875042	BIA	792.3	9.5	0.								ŧ z			•		
	-				025.44	:		1	:													

SPT Hoist, Liquid Pastic, BC + (10) cont. (2) limit ander (tat) + : 2 22.5 13.6 13.6 22.0 15.0 17.0 23.0 25.0 25.0 25.0 25.0 25.0 15.0 15.0 26.0 6.0 # 12 3 # R R \$ 4 4 8 8 2288 Unified Bulk Dry Soil Percent Unit Mt. Class. P200 (pcf) + ENGINEERING PROPERTIES ರದದರ್ವಹಹಹ್ಮವರದರಹಹಹಹಹಹದರವರದ ಕ್ಷಕ್ಷೆ ತೆರರರದರ ಕ್ಷಕ್ಷಣದರರಹಹಹಹಹ ಜಿ. ರ ಪ್ರದ ದ Matrix I Batrix I Hatrix I + + sand silt ciay + Bult I (2.0 to (0.0525 to +)2.0se 0.0525as) (0.002ss) ((0.002ss) + GRAINSTIE PERCENTAGES Fld K Neth (ca/s) code 1.06E-05 Lab K Keth (cs/s) code + HYDRAUR.IC + CONDUCTIVITY 14.0 22.0 22.0 23.0 23.0 25.0 25.0 25.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 792.3 792.3 792.3 792.3 792.3 792.3 792.3 792.3 792.3 792.3 792.3 792.3 792.3 792.3 792.3 792.3 792.3 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 793.7 8 11 A A 11 B 11 B 11 A A 11 B 11 B 11 A A 11 B 11 Brno. | no. 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 875042 87 H3047 H3047 H3047 H3047 H3047 H3047 H3039 + Litho-+ strat. + County unit Hat. Site + {code} Year (code)(code) No. + IDENTITY

Appendix 3 - Hydroseclogic and engineering data for byony county - Baeton Site

+ GRANKSIE PERCENTARES + ENGINEERING PROPERTIES + Matrix I Matrix I Natrix I + sand silt clay + Unified Bulk Dry + sand silt clay + Unified Bulk Dry + (cat + Bulk I (2.0 to (0.0625 to + Soil Percent Unit Mt. SPI Boixt. Liquid Plastic. UC + (cafs) code + 72.0ms 0.0625ms) 0.002mm) + Glass. P200 (pcf) (M) coot.(2) limit index (tsf) + 21.0 15.0 17.0 26.0 20.0 15.0 15.0 13.6 16.0 17.0 228 2 8 3 3 3 3 ## bottom + Lab K Neth
(ft) + (cs/s) code + HYDRAULIC + CONDUCTIVITY 1.805-08 Brng. 6 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 875035 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 87503 8750 443045
443045
443045
443045
443046
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039
443039 unit Nat. Site (code)(code) No. + County un + (code) Year (+ IDENTITY

Appendix 3 - HYBROGEOLOGIC AND ENSINEERING DATA FOR BROKN COUNTY - BAETON SITE

Appendix 3 - HYBROSCOLOSIC AND ENGINEERING DATA FOR BROAK COUNTY - BAETON SITE + IDENTITY + HYBRAR IC

th Fiek Neth + Bulk X (2.0 to (0.625 to silt to to (0.625 to to (0.625 to to to (0.625 to		Litbo							- •	F HYDRALE IC	ر بند بند		+ GRAINS	GRAINSTIE PERCENTAGES	IAGES		+ ENSINEERING PROFERITES	S PROPERTI	83			+
14.	strat.						Sir.	Sante	Sant		=			Matrix 2	Matrix I	Matrix 1	1					+
Lit. Long. no. (19) (11) (101) (101) (101) (101) (101) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (100) (10	unit		it. Site				Eler.		bottos	1 1 Sh K	Kety	Cld Y Noth		2 0 0	21115	Š		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		3	:	+
10 10 10 10 10 10 10 10) (ago	- E .	ode) Ko.		- 1	ė	₽.		€	(S/#3)	go a	ica/s) rode		0.062541)		((0.002an)		P200 i		7 Bost. 0 cont. (2)	Liquid Plastic. W limit index (t	*
90008 8118 782, 52.0 5.1.5 90008 8118 782, 52.0 5.1.5 90008 8118 782, 52.0 5.1.5 90008 8118 782, 52.0 5.1.5 90008 8118 782, 52.0 5.1.5 90008 8118 782, 52.0 5.1.5 90008 8118 782, 52.0 5.1.5 900008 812 784, 0.1.5 90008 812 784, 0.1.5 90008 812 784, 0.1.5 90008 812 784, 0.1.5 90008 812 784, 0.1.5 90008 812 784, 0.1.5 90008 812 784, 0.1.5 90008 812 784, 0.1.5 90008 812 784, 0.1.5 90008 812 784, 0.1.5 90008 812 784, 0.1.5 90008 812 784, 0.1.5 90008 812 784, 0.1.5 90008 812 784, 0.1.5 90008 812 784, 0.1.5 90008 812 784, 0.1.5 90008 812 784, 0.1.5 90008 812 784, 0.1.5 90008 812 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 813 784, 0.1.5 90008 913 784, 0.1.5 90008 913 784, 0.1.5 90008 913 784, 0.1.5 90008 913 784, 0.1.5 90008 913 784, 0.1.5 90008 913 784, 0.1.5 90008 913 784, 0.1.5 90008 913 784, 0.1.5 90008 913 784, 0.1.5 90008 913 784, 0.1.5 90008 913 784, 0.1.5 90008 913 784, 0.1.5 90008 913 784, 0.1.5 90008 913 784, 0.1.5 90008 913 784, 0.1.5 90008 913 784, 0.1.5 90008 913 784, 0.1.5 90008 913 784, 0.1.5 90008 913 784, 0.1.5 90008 913 784, 0.1.5 90008 913 784, 0.1.5 90008 91	£61		, . F3	443047			798.5		17.0								2		-	7		:
## 1978 111 7915 3.0 0. 2.2 Page 1978 112 7910 3.0 Page 1978 112 7	3		 P	443047					21.5								3 <i>3</i>		•			
## 1962 B 11 18 1963 3 50 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	š		,w.	150					29.3							•			•	•		
## PROOF BIT 7855 34.7 39.7 5.12F-06 ## B SS BENOME BIT 7855 34.7 39.7 5.12F-06 ## BENOME BIT 7850 5.14.7 9.5 0	5		·~	443047					31.0													
1,500	5		m	113017					35.2			-					. <i>T</i>					
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	3		·	443047					39.7		vi						<i>5</i> 5					
15,000 10,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 1	2		-	143041		812	74.0		2.0								ජ					
15.00 11.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.00 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5	93		. <u>.</u>	443043		112	794.0		6.5								4			=		
15.00 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.5	3		-	38		812	794.0		1.5											: 2		
17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.0	<u>e</u>		, <u>,</u> ,	#30F		B12	74.0		17.0								le					
17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.00 17.0	₹		**	#30#		B12	794.0		21.5	1.565.0			22		7		3 8	2		4.01		
850008 812 744,0 36,0 31,3 95,0 91,3 91,3 91,3 91,3 91,3 91,3 91,3 91,3	季		'n	13013		B 12	794.0		26.5		,		1		F		5 2	5	•	=		
17.00 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0	Ē			443041			794.0		3.5								8 2		•	.		
815728 813 772, 0 1.0 5.0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0 0 7.0	₹		~	443041			794.0		7								8 2		•	- 4		
815/268 813 772,0 5.0 7.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610 12.0 610	KEE		-	443036			792.0		4								% a		-	≥•		
853028 813 792.0 6.0.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0	193		m	443036			792.0		9								3 2			;		
98509 813 792.0 52.0 52.0 52.0 52.0 52.0 52.0 52.0 5	183		m	113036			262		2								3 8			0.0		
875028 813 772.0 20.0 22.0 24.5 24.6 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0 24.5 25.0	53			47074			202										ದ :			17.0		
Figure 11 Figure 12 Figure 13 Figu	29			120			707										ರ (24.6		
870.00 813 72.0 50.0 14.2 9.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8	₫			417074			702		2.10								d i					
## 175.03 #13 192.0 #5.0 #5.0 #14.0 #15.0 #14.0 #15.0 #14.0 #15.0 #14.0 #15.0 #14.0 #15.0 #14.0 #15.0 #14.0 #15.0 #14.0 #15.0 #15.0 #14.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0 #15.0	, 5		 . M	13036			792.0		e e								5 . 3		•	12		
875028 814 794,0 1.0 2.5 6.5 89 82038 814 794,0 1.0 2.5 6.5 89 82038 814 794,0 1.0 2.5 6.5 89 82038 814 794,0 1.0 2.5 6.5 89 82038 814 794,0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.	3		·	443034			797		3 5								5 8					
875028 B14 794.0 5.0 6.5 6.5 875 875 875 875 875 875 875 875 875 87	₹			143031			794.0		2.5								5 3		•	Ŀ		
B75028 B14 744,0 11,0 11,2 44 B75028 B14 774,0 13,0 11,0 11,2 44 B75028 B14 774,0 23,0 21,0 B 53 41 139 B75028 B14 774,0 25,0 24,0 B 53 41 139 B75028 B14 774,0 25,0 24,0 B 53 41 13,0 B75028 B14 774,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 B75028 B15 772,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 11,0 <td>.EB1</td> <td></td> <td></td> <td>443031</td> <td></td> <td></td> <td>794.0</td> <td></td> <td>5.9</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>d 2</td> <td></td> <td>•</td> <td>Ωŧ</td> <td></td> <td></td>	.EB1			443031			794.0		5.9								d 2		•	Ωŧ		
875028 B14 774.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15	£61		w 	443031			794.0		11.5				Ξ	3	5	2	ž Ž	٥		2 5		
675/28 814 794, 0 20.0 21.0 874 137 675/28 814 794, 0 25.0 26.0 14 52 40 8 58 41 180 675/28 814 794, 0 30.0 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6 30.6	盏		m	443031			794.0		16.0				•	\$	2	=	\$ 5	à	- :	f 9		
14 14 15 15 15 15 15 15	霻		 	443031			734.0		21.0								i i		3 =	÷ ≤		
075028 B14 794.0 30.0 30.6 878 818 792.0 10.0 11.5 878 818 818 792.0 10.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 818 792.0 11.5 8	5		, <u></u>	443031			794.0		26.0				2	5	9	œ	5 8	=	=	2		
875028 815 792.0 5.0 7.0 6.0 11.5 5.0 872.0 815 792.0 5.0 7.0 6.0 11.5 5.0 872.0 815 792.0 5.0 7.0 6.0 11.5 5.0 872.0 815 792.0 5.0 7.0 11.5 5.0 872.0 815 792.0 5.0 7.0 11.5 5.0 872.0 815 792.0 5.0 21.5 5.0 872.0 815 792.0 5.0 21.5 5.0 872.0 815 792.0 5.0 21.5 5.0 22.0 872.0 815 792.0 5.0 21.5 5.0 22.0 872.0 815 792.0 5.0 21.5 5.0 22.0 872.0 815 792.0 5.0 21.5 5.0 22.0 872.0 815 792.0 5.0 22.0 7.0 872.0 815 792.0 5.0 22.0 7.0 872.0 815 792.0 5.0 22.0 7.0 872.0 815 792.0 5.0 22.0 7.0 872.0 815 792.0 5.0 22.0 7.0 872.0 815 792.0 5.0 22.0 7.0 872.0 815 792.0 72.0 72.0 72.0 72.0 72.0 72.0 72.0 7	3		. <u>.</u>	113031			794.0		30.6				•	•	2	•	; <i>7</i> 5	7				
815028 815 792.0 1.2 5.0 7.0 7.0 815028 815 792.0 5.0 7.0 81508 815 792.0 5.0 7.0 815028 815 792.0 5.0 7.0 815028 815 792.0 5.0 7.0 815028 815 792.0 20.0 21.5 818 819 819 819 819 819 819 819 819 819	š		<u>-</u>	13031			791.0		36.0								<u>20</u>					
875/028 815 792.0 5.0 7.0 11.5 CL 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0	ž į		- ·	43028			792.0		5.0								귳					
875028 815 772.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15	ä :		- ·	113026			792.0		0.0								ರ			13.0	-	
815.028 815 772.0 15.0 16.0 838 879 872.0 15.0 16.0 838 879 872.0 15.0 16.0 16.0 838 815 772.0 20.0 21.5 838 815 772.0 20.0 21.5 838 815 772.0 20.0 21.5 838 815 772.0 20.0 20.0 20.0 20.0 20.0 20.0 20.	4			113076			792.0		::								ಕ			17.0	•	
875.028 815 792.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 2	5 3		- ·	97X1			792.0		9.0								ž		•			
915/028 815 792.0 25.0 26.0 Ss 24.0 Ss 24.0 Ss 25.0 Ss	5 :		· ·	413070			782.0		2:5								55		_	æ		
815/2028 815 792.0 30.0 30.2 SS	5		~	443026			792.6		26.0								8		=	.		
875028 815 792.0 35.5 35.5 35.5 35.5 35.5 35.5 35.5 35	\$		m	113026			792.0		30.2								S.		. ~	: 5		
875028 8146 792.8 1.0 5.0 13.0 13.0 13.0 13.0 13.0 13.0 13.0 13	5		·~·	443026			792.0		35.5								3		;	2 4		
875028 B164 792.6 5.0 7.0 13.0 13.0 13.0 14.0 15.0 12.0 12.0 12.0 14.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15	<u> </u>		'n	443021			792.8		5.0								ž		5			
875028 816A 772.8 10.0 12.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17	3		m	443021			792.8		7.0								\$ Z			9	*	
875028 8164 792.8 15.0 17.0 Ct. 24.0 875028 8164 792.8 20.0 22.0 Ct. 24.0 875028 8164 792.8 20.0 22.0 Ct. 24.0 875028 8164 792.8 20.0 27.0 Ct. 26.0 875028 8164 792.8 20.0 32.0 Ct. 26.0 875028 8164 792.8 20.0 32.0 Ct. 26.0 875028 8164 792.8 20.0 32.0 Ct. 20.0 Ct. 26.0 875028 8164 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 792 816 702 816 702 816 702 81	83		m	143021			792.8		12.0								t z				-	
875/28 8146 792.8 25.0 22.0 CL 24.0 CL 28.0 875/28 8146 792.8 25.0 27.0 CL 26.0 CL 28.0 CL 28.	93		. <u>.</u>	113021			302 8		5								3 2				₹ (
875028 B164 772.8 25.0 27.0 CL 26.0 B75028 B164 772.8 30.0 32.0 CL 26.0 CL 26.			. .	143021			76.0										#			74.0	7	_
26.0 875078 Block 172.8 35.0 32.0 875078 Block 172.8 17.0 32.0	93			1477			707		2.5								ಕ :			i		
87078 BIAA 1919 BIA 14.0	E91			143021			70.0		3.75								ಕ :			26.0	- i	.
	3		-	143021			767		2 2								ಕ ಕ					

Ξ

SPT Moist, Liquid Plastic, UC + (4) coat, (2) limit index (lsf) + 15.0 33.0 25.0 19.0 19.0 19.0 19.0 ዴ 8 % | Hatrix + ENGINEERING PROPERTIES # 12 # K \$ # 8 2 육 # 2 2 + BRAINSILE PERCENTAGES 22 22 1.588-05 1.568-05 Sample Sample +
top bottom + Lab K Meth
(ft) + (tm/s) code + KYTRAULIC + CONDUCTIVITY 5,10£-09 2,30£-08 1.305-07 2,906-09 Appendix 3 - Hydrobeologic and ensinkering data for brown county - breton site 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20 Brag. 1 strat. unit Hat. Site (code)(code) No. + County u + (code) Year (+ IDENTITY

5.5

ଅ ଅ

3.5

2.3 2.3

+ sand silt clay + Unified Bulk Dry + Houst I (2.0 to (0.0625 to + Soil Percent Unit Mt. SPT Moist. Liquid Plastic. UC + (ce/s) code + 72.0se 0.0625se) 0.002es) ((0.002es) + Class. P200 (pcf) (Mt cont.(I) limit index (185) + 2222 23.0 26.0 26.0 20.0 7.0 5.0 5.0 **\$ 2** 25 25 25 ន + ENGINEERING PROPERTIES 2 B + SRAINSIIE PERCENTOGES + HATTIX I + HATTIX I HATTIX I + H 2 23 0 క్ల **\$ ≓ =** 8 ¥ = 22 Sample Sample +
top bottom + Lab K Meth
(Ht) (Ht) + (cm/s) code + HYDRAULIC + COMBUCTIVITY 4.406-09 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25 775.0 775.0 775.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 776.0 Brng. 875015 875015 875015 875015 875015 875015 875015 875015 875015 875015 875015 875015 875015 875015 875015 875015 875015 875015 875015 875015 875015 875015 875015 8 Lat. + Litha-+ strat. + County unit Mat, Site + (code) Year (code) No. + IDENTITY

Appendix 3 - HYDROGECE DOLD AND ENSINEERING DATA FOR BROWN COLUNTY - BAETON SITE

+ Unified Bulk Bry + Soil Perceot Unif Mt. SPT Moist. Liquid Plastic. UC + Class. P200 (pcf) (M) cod.(I) lisit index (1sf) 26.0 26.0 22.0 25.0 26.0 B.0 16.0 23.0 25.0 11.0 22.0 5 9 9 9 9 9 **33 33** 8 + GRAINSIE PERCENTAGES + ENGINEERING PROPERTIES + Katrix I Natrix I + ರದರದದರ್ಷಕ್ಕಳದರದರರದಕ್ಕೆ ರ ದದರರದದರ±% + sand silt clay Fld K Neth + Bulk X (2.0 to (0.0425 to (te/s) code + 22.0se 0.0425as) 0.002as) ((0.002as) e Sample +
bottos + Lab X Neth F
(ft) + (cs/s) code (+ HYDRAIR IC + CONDUCTIVITY Appendix 3 - HYDROSECKOSIC AND ENGINEERING DATA FOR BROWN COLNTY - BRETON SITE Saple (ft) Surs. Brng. Elev. no. (ff) 875010 875010 875010 875010 875010 875015 875015 875015 875015 875015 875015 875015 875015 875010 875010 875010 875010 875010 875010 875010 875010 875010 875010 875010 875010 875010 875010 875010 H3021 H3022 H3022 H3022 H3022 H3022 H3022 H3022 H3022 H3023 H3023 H3034 + Litho-+ Strat. + County unit Nat. Site + (code) Year (code) Koo, + 10ENTITY

+ +	+ - 50 10 10 10 10 10 10 10 10 10 10 10 10 10	lex (tsf) +		3.5	1.0	0	; -		4
	Actal Actal	(N) cont. (I) limit index (tsf) +	831 795.0 5.0 6.5 23	11.0	18.0	22.0	27.0	25.0	4 71
	9	; 3	2						
OPERTIES	the Kein the Sand Silt clay thifted Bulk Bry Sid Kein the Sand Sanda Sail December Sail December Sail December Sail December Sail December Sail Sail	(pcf).							
+ EMSINEERING PROPERTIES	ied Bul	ss. P20	ದ	ದ	ದ	ಚ	ದ	ರ	Ŧ
1983	ig is	13							
T + M M	- 4	3							
Hatro	Clay.	((0,002)							
MAES Matrix I	sand silt clay	0.00201)							
+ GRAINSIZE PERCENTAGES • Astrix I Satr	Sand	625aa)							
321SK	2	, 30 • 40 • 40							
+ GRAINSI	+ +	× ×							
	Y C	1/s) code							
	_	L apos							
+ KYDRAULIC + CONDUCTIVITY		(S)							
+ KYDRAULIC + CONDUCTIVI		. <u>.</u>							
	Sample Sample +	1	6.5		17.0				3,40
	Samole	€.	5.0		5.0				35.0
	Surt.	€	795.0	795.0	795.0	795.0	795.0	795.0	795.0
	ر د د د	no. (ft)	331	Z	33	131	2	33	831
				875010	875010	975010	875010	835010	875016
		+ (code) Year (code) (code) No. Lat. Long.	443029					443029	
	9	ġ		-	-			_	_
	**	(code)	m	m	M	m	m	*	~
itho-	strat, unit Nat Site	+ (code) Year (code) (code) No.	KEBI		1937	<u> </u>	XEG	KE	3
تند		P.	BK 1982	1982	1982	1982	1982	1982	1982
IDENTITY L:	+ Founty	>-	i						

SPT Moist, Liquid Plastic, UC + (N) cont.(1) limit index (tsf) + 5555 3.7 5.5 3.3 2.5 12.0 917.0 19.0 21.0 5.0 8. 5.8.5 <u>~</u> 8 ድ ድ \$ S 2 + GRAINSIZE PERCENTAGES + EMBINEERING PROPERTIES
+ Asia Sand Silt clay + United Bulk Bry
Fld K Helh + Bulk I (2.0 to (0.0625 to + Soil Percent Unit Bry
(ce/s) code + 32.0mm 0.0625mm) ((0.0020mm) + Class. P200 (pcf) ರ ನದಲ್ಲಿರಲ್ಲಿ ಪಡೆದ ಪತ್ರದ ಪತ್ರವಾಗ ವಿಜ್ಞಾಗ ಕ್ಷಣ್ಣ ಪ್ರಚಾಣ ಪ್ರಚ 5.00E-07 2.00E-07 Appendix 3 - Hydroseologic and engineering data for brown county, decaster essona county Nesti site Sample Sample +
top bottos + Lab K Meth
(ft) (ft) + (cs/s) code + HYDRAULIC + COMBUCTIVITY 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 660.5 Surf. Brng. Elev. Long. av. (#1) 880971 MT 1880971 MT 1880972 MT 1880974 MT 1 443046 880921 443046 880921 443046 880921 443046 880921 443046 880921 443046 880921 443046 880921 443046 880921 443046 880921 443046 880921 443046 880921 443103 880922 443103 880922 443103 880922 443103 880922 443103 880922 443103 880922 443103 880922 443103 880922 443103 880940 443051 880940 443051 880940 443051 880940 443051 880940 443051 880940 443051 880940 443051 880940 443051 880940 443051 880940 443051 880940 443051 880940 443051 880940 443051 880940 443051 880940 443051 880940 443051 880940 443051 880940 + Strat. + Ecounty unit Mat. Site + (code) Year (code) No. + IDENTITY

2.0 2.8 2.8

3.5

SPT Moist, tiquid Plastic, UC (M) cont.(2) limit index (1sf) 20.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 3,0 12.0 21.0 11.0 11.0 15.0 15.0 24.0 28.0 28.0 **となるない 4 2** 2 22 - GRAINSIZE PERCENTAGES + ENGINEERING PROPERTIES

MATTIX Z MATTIX Z HATTIX + ENGINEERING BUIL Bry

SAIK Z (2.0 to (0.0625 to + Soil Percent Unit Nt.

) 2.088 0.06288) 0.00288 (0.00288) + Elass. P200 (pri) + sand silt clay + Bulk I (2.0 to (0.0625 to +)2.0ss 0.0625ss) 0.002ss) ((0.002ss) Fld K Keth (ce/s) code Aparadix 3 - Krorobeca,dolo and engineering data for brown county, decaster (brown county Nest) site Sample Sample +
top bottom + Lab K Neth
(ft) (ft) + (cm/s) code + HYDRAULIC + CONDUCTIVITY 691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
691.11
69 Sari. Brng. . 880939 880939 880939 880939 880939 680939 B80939 B80939 B80939 \$80939 1000 880932 880932 880932 £80932 £80932 680932 89952 880932 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 443059 4430 4430 4430 4430 4430 4430 4430 44 strat. unit Hat. Site r (code) (code) No. + County u + (code) Year (

23

2.5

□ # □ 9 9

SPI Moist, Liquid Plastic, UC + (N) cont.(1) limit index (tsf) + 22.0 22.0 22.0 22.0 22.0 19.0 19.0 19.0 28.0 28.0 28.0 21.0 ㅈ욢 Unified Bulk Dry Soil Percent Unit Mt. S Elass. P200 (pcf) (+ ENGINEERING PROPERTIES 2 2 3 5 2 3 4 5 4 8 85 Fld K fieth (ca/s) code Appeadix 3 - Hydroseolobic and ensineering data for brown county, decaster (brown county mest) site Sample Sample +
top bottom + Lab K Meth
(ft) (ft) + (cm/s) code + HYDRAULIC + CONDUCTIVITY 6. 20E-07 2. 20E-07 1.90E-07 657.4 657.4 657.4 657.4 657.4 657.4 657.4 657.4 657.5 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 655.2 Brng. I 880924 880924 880924 880924 880924 880924 680924 880924 880920 880920 880920 880920 880920 880920 880920 880920 880920 880920 880920 880920 880913 880913 880913 880913 880913 880913 880913 880913 880913 tong. 443041
443041
443041
443041
443041
443041
443041
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443058
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068
443068 + County unit Nat. Site + (code) Year (code) (code) No.

2.5 9.8 9.8 2.5

::2

2:2

22222

白鲜好民族 眼喉经路现象

2.

245568456 4114788845654565

SPT Moist, Liquid Plastic. UC + (M) cont.(1) limit index (tsf) + 这山丘蛇的种观察图列记忆的创新电线统统规处设计设建设设计图台设设设定的记录 化 的现代判别组 2 Unified Bulk Dry Soil Percent Unit Ht. Class, P200 (pcf) + ENGINEERING PROPERTIES 2222 **484878358488888888888448844888** + Matrix I Matrix I Matrix I + sand silt clay + Bulk I (2.0 to (0.0625 to + 72.0ss 0.0625sz) 0.002ss) ((0.002ss) GRAINSIZE PERCENTAGES eth code Fld K II Appendix 3 - HYDROGEOLOSIC AND ENGINEERING DATA FOR BROWN COUNTY, DECASTER IEROMN COUNTY WEST) SITE Ket Code * CONDUCTIVITY 305-05 2.605-06 4.506-07 2,30E-06 4.00E-08 9.80E-08 4.206-07 6.10E-08 9.20E-08 7.806-08 1.20E-07 5.60E-08 3.80E-08 1.905-06 Sample Sample +
top bottom + Lab K
(ft) (ft) + (co/s) 669.0 668.0 668.0 668.0 668.0 668.0 668.0 668.0 669.0 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 660.1 Surf. Brng. Elev. ao. (it) 880931 880931 880930 880930 880928 880924 880924 880937 880937 880937 880925 880925 880925 880925 880925 880924 880924 880923 B80936 880924 880937 680937 2003 **B**86926 880936 880936 880935 880935 880937 880927 880926 880936 ğ H3046 H3046 H3046 H3046 H3046 H3045 H3047 + County unit Mat. Site + (code) Year (code) (code) No.

ppeno		Appendix 3 - Hibridge Delic HWD ENGI	EULVO!	1	NO I NECK		ă	KORN LUK	-	200	EXCENS L	1100	PPEROOIX S - MIUNICELLUSIC FRU ENGINEERING DAIN TUR BRUNN LUCANIT, BELLASIEN (CRUMN LUCANIT MEUL) SLIE		rum balam (Loun)!, Betwaite (Balam Luchi)!										
TENTITY	<u>-</u>									+	+ RYDRAULIC	31		7	+ GRAINSIZE PERCENTAGES	RCENTAGES		+	ENERG	+ ENSINEERING PROPERTIES	RTIES				+
	_	Litho-								+	+ CONDUCTIVITY	WITY		+	Matr	1x 1 Patr	in I A	atrix 1 +							٠.
		strat.					ű		31445	Sable Saple +				••	35	sand silt clay	- -	clay +	Unifie	d Bulk	Š				+
County	_	unit	Hat. S	ite		Ä	ż	Ber.	to G	botton +	X qe1	Reth	F36 K	Neth + 1	Bulk X (2.0	to (0.06	25 to	+	Saii	Percent	Unit it.	SPT Moist.	140.0	lastic. l	+
(code)	Year	(code) Year (code) (code) No.	(code)	₫.	ij	Loog. no.			3	÷ ##	(ff) : (ca/s) code	ğ	(S/8J)	tode +	(ft) (ft) : (ta/s) code (ca/s) tode + >2.0mm 0.0625mm) 0.002mm) ((0.002mm) + Class. P200 (pcf)	Seri 9.0%)2mm) ((0,	.002es) +	C1 255	. 200	(pcf)	(N) cont.(I) limit index (tsf) +) lieit	index (1	st) +
25	1979	×	'n		H3044	880929	4	, ~:	12.0	13.0	3,306	25.5			\$				ರ	. P	_	30 23 9	ĸ	•	
蓋	1979	¥	š	7		380929	2	665.9	2.0	3.0	2.606-08	\$ 89			2				3	1 62		83	≈	12	
×	1979	¥	'n	7		380928		665.4	12.0	13.0					•				G	<u>.</u>		32	53	22	
蕊	1979	별	v	7		880928		645.4	3.0						м				ជ	 		3	83	2	
盃	1979	뽀	w	~		880927	22	663.1	12.0	13.0					۰				무	<u>۳</u>	_	23	82	_	
蓋	1979	¥	ĸ	7		780927	ě	663.1	2.0						۰				7	.9		4	₹	'n	
ă	1979	뽀	\$	7	443099	B80999		0.699		2.5													S	•	
æ	1979	벌	\$	7		380999		670.0															83	2	
盖	1979	별	\$	~		880999	#	691.0															23	22	
潇	193	쎂	\$	~		880999		669.0	2.0	3.0	1.015-05	5										2			
ПФ	4070	5	0	•		90000		4 677	4	4	A AA	5										:			

SPT Moist, Liquid Plastic, UC + (M) cont.(Z) Limit index (tof) + 3.0 .. ç: + Unified Bult Bry + Soii Percent Unit Ht. + Class. P200 (pcf) + ENGINEERING PROPERTIES Ratrix I Matrix I Matrix I + + sand milt tisy Fid K Meth + Bulk I (2.0 to (0.0625 to [ca/s] code + 22.0ms 0.0625ms) 0.062ms ((0.002ms) + GRAINSIZE PERCENTAGES e Saple +
bottom + Lab K Meth
(ft) + (cm/s) code + HYDRAULIC + CONDUCTIVITY 6.80E-04 Appendix 3 - HYBROSEOLOGIC AND ENGINEERING DATA FOR BROWN COUNTY - DECLERAE SITE Brag. 880028 880028 880028 880028 880028 880028 880028 880038 880038 880038 880038 880038 880038 880038 880038 880038 880038 880038 880038 880038 880038 880038 880038 880038 880038 880038 880038 880038 880038 880038 + strat.
• County unit Mat. Site
• (code) Year (code) (code) Mo.

							+ HYDRAULIC	31.0		+ 6RA1MS	+ SRAINSIZE PERCENTAGES	'AGES		96	+ EMBINEERING PROPERTIES	ROPERTIES			
							10X03 +	+ CONDUCTIVITY		•	Natrix 1	Natrix & Matrix & Natrix &	Natrix 1	•					•
strat.				ż	Surf. Sam	pie Saapi	+			+	ere:	silt	ciay	<u>=</u>	fied Bu	1k Dry			
unit Aat, Site	Site			Brng. Elev.	ev, top	botta	6 + L3b	K Meth	i Fid K Meth	1 + Bulk 1	(7.0 to	10.0425 to	-	S.	ii Per	cept Unit Mt	. SPI Moist.	Liquid Pla	tic. UC
ide) (rođe)	Ko	t (rode) Year (rode) (rode) No. Lat. Long.		10. (ft)	# #	æ	(ft) (ft) + ica/s) code	's) code	\$900 (\$/#3) i	+ 72.088	0.0625as)	0.06288) ((0.002sa)	ಪ +	ass. P2	(pcf)	(ca/s) code + >2.0as 0.0625as) 0.002as) ((0.002as) + Elass. P200 (pcf) (M) cont.(2) lisit ladex (tsf) +	lisit 18	dex (tsf)
BN 1983 KES1 3	m	3 442499 880099	880099 MA	127.	M27a 842.1 0.0 1.5	0.									8		BB 1983 KG61 3 3 44249 880059 NK72 842.1 6.0 1.5		
KES3 3	m	442499	ŝ	M27a 1	842.1 5	5.0 6.5									<u>ದ</u>		25		
*	n -	3 442499 88	8	HI27a	842.1 10	10.0 11.5	. ~								83		~		
5	•	000000 001010	5000			•									:				

SPI Noist. Liquid Plastic, UC + (M) cont.(X) limit index (tsf) + \$ 5.5 3.0 25.0 18.0 15.0 23.0 21.0 19.0 18.0 23.0 25.0 5.0 5.0 1.334 6.28 M ± 2 3 5 5 ± ± 2 5 + Unified Bulk Dry + Soil Percept Unit Mt. + Class. P200 (pcf) GRAINSIZE PERCENTAGES + ENGINEERING PROFERITES
MATRIX I MATRIX 1 MATRIX 2 + + sand silt clay + Bulk Z 12.0 to (0.0625 to +)2.0mm 0.0625mm (0.002mm) **%** 2 ន្តន 2 fld K Neth (cs/s) code Sample Sample + top button + tab X Neth (ft) (ft) + fcm/s) code + HYDRAULIC + CONDUCTIVITY 2.00E-07 i 2.10€-08 1.385.48 591.2 592.2 593.2 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 593.3 59 Suri. Elev. (#1) Brnd. BD. 880003 880003 880003 880003 880003 880003 880003 880003 880005 880005 880005 880005 880005 880005 880005 880005 880005 880012 B80012 880011 B80011 680000 860000 675958 875958 875958 875958 875958 875958 875959 875959 875959 875959 875959 875959 BB0003 BB0003 BB0003 41312 6 44312 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 6 44313 + County unit Mat. Site + (code) Year (code) (code) No. * IDENTITY

Appendix 3 - Hydfogedlogic and engineering data for brown county - northeand sludge site

															*****				******						
+ IDENTITY									+	+ HYDRAULIC	٠			+ SPAINSIZE PERCENTAGES	RENTAGE	•		*	INCER! NG	+ DASINEERING PROPERTIES	55				
															-	:									
•	Litho-								+	+ COMBICTIVITY	Ě			+ Hatr	1× 2 12	trix X	Strik	+							
•	strat.					Seri	Surt. Sa	S alder	anose +					*	2	sand silt clay +	Clay	5	ified	Pelle Pelle	<u>د</u>				
+ County	unit	Nat. Si			arg.	o. Eley	y. to	9	ottos +	Lab K	Keth	F36 K	Keth	+ Bulk I (2,0	to .00	0625 to		+	9 110	erceat this	it Ht.	PT Rois	t. Liau	id Plast	3
+ (code) Year (code) (code) No. Lat. Long. 1	er (tode) ((code)	fo.	ار. بر	od .pc	ap. (HE) (=	ت چ	÷	(cs/s)	Code	{c#/8]	ğ	(ft) (ft) + (ta/s) code (ta/s) code + 32.0as 0.062bas 0.002as ((0.002as) + Class. P200 (pcf) (H) cont.(I) linit index (tsf) +	San O.)) (ma200	9.00288)	+	3a55.	P200 (Ę	II) cost,	(Z) Jian	t inde	(tsf)
Bn KE 5 4 443150 8890.	52	2	1 4315	288		88	88 589.0 5.0 15.0	5.0	15.0	-		PO-305-04	-	11 88 589.0 5.0 15.0 6.56F-04 ?				1	fill, G.						
8	쌪	m	4 44315	443150 880011		38 58	589.0 24	28.0	30.0			2,705-07	~						<u> </u>						
æ	Œ	,,	4 44315	51 88	90100	22 22	586.5	10.0	11.5										겁			R			
å	7	ur.	21744 4	51 980	7010	90	COL R. 15.0		9 49										3			•	•		•

OPERTIES IX Dry Sub-Hole Me Col Majer Signid Disest		(pcf) (N)	(pcf) (B)	(pcf) (JO	(pc.f.) (N)	(bc) (H)	(pcf) (N)	(pcf)	(pcf)	(pcf) (b)	(B)	(BC) (BA)	(86)	(86) (90)
+ ENGINEERING PROPERTIES + Unified Bulk Dr - Coil Backet Hoit	-		B 71	4	_									
						d	ជ	r d	. d	d s s =	d * * =			o 82 888
. Matrix I clay	+ >2.0ag 0.0625es) 0.002gs) ((0.002as) +				82.0	8 -0	m.s	8 .0 -	2					
GRAINSIZE PERCENTAGES Hatrix X Hatrix I sand silt buts 12 0 to 00.055 to	0.00288		2 78	2 28	87 8	787) } } 1 1
GRAINSIZE PERCENTAGES Matrix X Hat sand s Ruth Y 12 0 to 0	0.0625ea)		22	2 2	3.3	2.2	2 2 2	2 2 2	2 2 2 2	22 2 22	22 2 28	22 2 22 22 22 22 22 22 22 22 22 22 22 2	22 23 25 25 25 25 25 25 25 25 25 25 25 25 25	3 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
	+ >2.0ae		=	= 0	20	20	70 *	T 0 **	70 -	3 0 • • • • • • • • • • • • • • • • • • •	T O ***	TO 0 0	TO 0 O.W	
÷	(ce/s) code				10.1	60.0	60.	7 60	60 7	7 60 7	7 60 7	7 60 7	7 60 7	6 6 6
. 4	code (ce.		-		£.7	4,706	4,79E-07	4,70E-07 2,60E-06 7,50E-07	4,706 2.606 7,506	4,70E 2,60E 7,50E	4,70E-07 2,60E-08 7,50E-07	4,70E 2,60E 7,50E	4,70E 2,60E 7,50E	7.50E
ა 55			8,305-08	8,30E-08	8,30E-08	8,30E-08 1,90E-08	8,30E-08 1,90E-08 2,30E-08	8, 30£-08 1, 90£-08 2, 30£-08	8, 30E-08 1, 90E-08 2, 30E-08 3, 40E-08	8, 30E-08 1, 90E-08 2, 30E-08 3, 40E-08 2, 00E-09	8, 30E-08 1, 90E-08 2, 30E-08 3, 40E-08 2, 00E-09	8.30E-08 1.90E-08 2.30E-08 3.40E-08 2.00E-09 3.20E-09	8.30E-08 1.90E-08 2.30E-08 3.40E-08 3.20E-09 3.20E-08	8.30E-08 1.90E-08 2.30E-08 3.40E-08 3.50E-09 4.50E-09
Saple +	#		12.0	12.0	12.0 15.0 15.0	12.0 12.0 15.0 40.3	12.0 12.0 15.0 16.3	12.0 15.0 15.0 16.3 3.5	12.0 15.0 15.0 16.3 19.5 17.0	12.0 15.0 15.0 10.0 17.0 17.0	12.0 15.0 15.0 17.0 17.0 14.4	72.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0	72.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0	55.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0
Saple	€													40 844446000 000 8 8 8 8 8 8 9 0 0
Surt.		:		12 916.6 5 918.0					_	_	_	_		
2	Long. no.	1	281136 2812	_										
														440616 8811 440616 8811 440616 881 440616 881 440619 881 440619 881 440619 881 440613 881 440613 881
:	, Ko.		*	o G	n w	n ev ev ev								
tho- rat.	ofe) (code)		111								•			
: Litho- : Litho- + Strat, noit Not Gita) Year (c	99	200	1981	1981 1982	1987	1981 1982 1982 1982	1982 1982 1982 1982	1982 1982 1982 1982 1982	1982 1982 1982 1982 1982 1982	1982 1982 1982 1982 1982 1982	1982 1982 1982 1982 1982 1982 1982	1982 1982 1982 1982 1982 1982 1982	2
+ 19km1111 + County	tcod.	•	3	ತ ಪ	ತರ ರ	3535	ತರದರೆದ	ವರದವರ ಪ	000000	555555555555555555555555555555555555555		005055555555555555555555555555555555555		a u p b 5 5 5 5 5 5 5 5

SPT Boist. Liquid Plastic. BC + (N) cont. (T) light index (tsf) + 2 2 2 2 ==== + Unified Bulk Unit + Soil Percent Bry Ht. + Elass, P200 (pcf) + ENGINEERING PROPERTIES 2 2 = 35 85 85 C., 54, 53 64, 53 ರವಜ ಕೃ ಹಿ 55-85-85 SH,58-55 ដភ្ជភ្ភុង្**ង** ជ ជជជ 58, 59-58 58, 58-58 58, 59-58 28,59-58 58,59-58 58,59-58 Hatrix & Hatrix & Hatrix & + + sand silt clay + Bulk I (2.0 to (0.0625 to + >2.0mm 0.0625mm) ((0.002mm) B Z + GRAINSIZE PERCENTAGES Fld K Beth (te/s) code 7.01E-04 2.20E-04 6.90E-04 9.00E-04 1.405-04 3.665-04 1,076-02 2,806-03 3,476-03 9,846-04 1,766-03 5,886-03 1,506-03 1,326-03 Appendix 3 - Hydrosedlosic and ensineering data for dane county - hydrite chemical corporation Reth code + HYDRAUE.IC + CONDUCTIVITY Saple Saple + top bottos + tab K) (ft) + (ca/s) c 13. 4 13. 5 13. 5 14. 5 15. 5 15. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16. 5 16 Surt. Brng. Elev. Long. no. (ft) 430438 691154 430438 891154 430438 891154 430438 891154 430438 891154 430438 891154 430438 891155 430438 891155 430438 891156 430438 891150 430438 891150 430438 891150 430438 891150 430438 891150 430438 891150 430438 891150 430438 891150 430438 891150 430438 891150 430438 891150 430438 891150 430438 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 430448 891150 43 ij + County wait Mat. Site + (code) Year (code) (code) No. DN 1984
DN 1984
DN 1984
DN 1984
DN 1984
DN 1984
DN 1984 + IDENTITY

3.385-06

SPT Moist. Liquid Plastic, UC + (N) cont.(1) Limit index (tsf) + 24.8 24.8 24.8 24.5 24.3 24.3 8 5288 ¥ + ENGINEERING PROPERTIES

1 +

+ Unified Bulk Unit

+ Soil Percent Dry Mt. S

1 + Class. P200 (pff) (<u>5</u>5 ರಹಕ್ಕರಹಕ್ ಹ ದ + Sulk X (2.0 to (0.6625 to + N.Oss 0.0625ss) 0.002ss) ((0.002ss) Hatrix & Matrix & Matrix & **23 222222** 유있 ≍ 23 88 E * SPAINSIZE PERCENTABES 竹の口口の口口 927 9 22 2 9 - 4 8 Fld K Neth (ra/s) code 3.406-03 306.0 3.00E-04 2,605-04 Sample Sample +
top bottom + Lab K Weth
(ft) (ft) + (ca/s) code + HYDRAULIC + CONDUCTIVITY Serf. 892041 118 892041 118 892041 118 892041 118 892042 128 892042 128 892042 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892043 118 892020 LTP17 892017 LTP19 892037 LTP22 Prag. 892041 892041 892035 892035 892042 892042 892028 892028 892043 892043 892043 892043 892043 892043 892043 Ęġ. + Eousty unit Hat. Site + (code) Year (code)(code) No.

Appendix 3 - Hydrdeedlobic and Engineering data for dane county libey road site

÷:

SPT Moist. Liquid Plastic. UC + (N) cont.(1) limit index (tsf) + 25 11.6 2 2 1.0 0.5 ? 2.4 3 ĸ 2 ĥ 22 ≈ 经银铁路路时间转换 æ 8. 8.0 19.2 2 2 2 2 3 3 4 7 2 3 3 2 ∺ \$ + Unified Bulk Dry + Sail Percept Unit Mt. + Class. P200 (pcf) + ENGINEERING PROPERTIES **\$ ⇔** € ŝ ង្គង្គង់ស្គឺក្នុងជ 28 8 8 8 ಹರ ವಹದ **ಷ**ದ **ಫ** ದ ಹ ವ Matrix I Matrix I Matrix I + + sand silt clay (cd/s) Keth + Bulk 1 (2.0 to (0.0625 to (cd/s) code + 72.0ss 0.0625ss) 0.002ss) ((0.002ss) ないおおおけになける 2 2 ねれななななななれれ 2 2 GRAINSTLE PERCENTAGES \$2080-20° S ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ P- P-1.136-05 2.05E-05 6.99E-05 5.18E-05 9.84E-05 9.80E-04 6.67E-06 1.40E-05 Reth Code ww + HYDRAULIC + CONDUCTIVITY 3.995-07 1.60E-06 4.30E-08 Sample Sample +
top Bottom + Lab K
(ft) (ft) + (ca/s) 7.306-09 9, 10£-08 5,90£-08 1.00E-07 1.00£-07 16.8 18.7 10.0 928.0 928.0 824.3 824.3 824.3 821.0 852.0 855.0 813.6 813.6 813.6 813.6 841.0 Surt. Elev. ##3 Brng. E Long 885248
885248
885248
885248
885252
885252
885253
885253
885253
885253
885253
885253
885253
885253
885253
885253
885253
885253
885253
885253
885253
885253
885253
885253
885253
885253
885253
885253
885253
885253
885253
885253 412335
423316
423316
423316
423316
423316
423316
423329
423329
423329
423329
423329
423329
423329
423329
423329
423329
423329
423329
423329
423329
423329
423329
433329
433329
433329
433329
433329
433329
433329
433329
433329
433329
433329
433329
433329
4333329
433329
433329
433329
433329
433329
433329
433329
433329
4333329
433329
433329
433329
433329
433329
433329
433329
433329
433329
433329
433329
433329
433329
433329
433329
433329 + County unit Nat. Site + (code) Year (code) (code) No. + 10ENTITY

Appendix 3 - HYDKOBEOLOGIC AND ENSINEERING DATA FOR BODSE COUNTY, CARL SCHMITT LANGFILL

t. SPT Moist, Elquid Plastic, UC + (W) cont.(2) Elsett index (156) + 5,5 けいには はない はない はない はいけい はんれ + sand silt clay + Unified Bulk Bry Fid K Meth + Bulk I (2.0 to (0.0625 to + 50il Perceat Unit Mt. (te/s) code + >2.0m 0.0625mb 0.002mb (0.002mb) + Elass, P200 (pcf) Matrix 2. Matrix 2. Matrix 3. + ENGINEERING PROPERTIES
Sand おおんせいにない おおいりょうになんかい 化刀付びに申引 計画 内容 川 窓 内 石 付 行 付 は + SRAINSIZE PERCENTAGES Sample Sample +
top bottom + Lab K Meth
(ft) (ft) + (cm/s) code + HYDRAULIC + CONDUCTIVITY Appendix 3 - HYDROSEOLOGIC AND ENGINEERING DATA FOR DODGE COUNTY, CARL SCHMITT LANDFILL 20.0 7.5 7.5 7.5 8.6 630.0 623.0 834.0 825.0 846.0 Surf. Brng. Elev. no. (ft) 432307 885303 432307 885303 432307 885303 432310 885303 432314 885303 432314 885203 432319 885209 432319 885209 432310 885209 432310 885209 432310 885209 432310 885209 432310 885209 432310 885209 432310 885300 432310 885300 432311 885300 432311 885300 432311 885300 432311 885300 43231 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 885300 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43281 88530 43 titho
* Strai.

* County unit Nat. Sife

* (code) Year (code) No.

SPT Boist. Liquid Plastic. UC + (N) cont. (2) limit index (tsf) + 222222222222223 なれなみはれなななななななななななななななな 22222222 Unified Bulk Dry Soil Percent Unit Mt. S + ENGINEERING PROPERTIES \$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac{1}{2}\$\frac ま % % ま 果 % 展 来 ま け ひ む ひ ね な な む ひ む む な お ひ む ひ む ひ む ひ む + 68alMS11E PERCENTAGES
+ Matrix Z. Matrix Z. :
+ sand silt ciay +
h + Bulk Z. (2.0 to (0.0625 to +
h + 7.04s 0.0626a) 0.002as) (40.002as) **232232222222222** Samie +
bottom + Lab K Neth Fld K Meth
(ft + (ra/s) code (ra/s) code 3,406-64 1,936-04 2,736-04 1,256-05 3,446-65 1,546-04 2.52E-04 1.49E-04 2.55E-04 3.05E-05 3.00E-06 + HYBRAULIC + CONDUCTIVITY Appendis 3 - Hydroseolesic and ensineering data flæ dabbe county, hechinovich site Saple S top b 930.0 980.8 980.8 980.8 932.3 932.4 935.9 975.0 977.0 977.0 977.0 977.0 977.0 977.0 977.0 977.0 977.0 977.0 Surf. Brng. Elev. no. (ft) 883315 883315 883306 883333 883333 883335 883335 883335 883335 883335 883335 883335 883335 883335 883335 883335 883335 883315 883326 883326 683314 683311 883311 883321 883321 412744 412748 412748 412748 412748 412748 412744 412744 412749 412749 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 412774 41 strat. unit Nat. Site r (code) (code) No. + County u

Appendix 3 - NYDROBEOLOBIC AND ENBINEERING DATA FOR GODE COLNYY BALEFELL

+ IBENTITY +	Litho-								•	EDMINICTEVETY	<u>.</u>		+ 06044	BRAINSIZE PERCENTAGES	E PERCENTAGES	Hateric 9		ENGINEERINS PROPERTIES	RTIES			
	strat.						Surt.	Suple	Saple Sample +					Sad a	5111		+ Unified	4 (12)	, di			•
+ County + (tode) Year		unit Kat. S (code)(code) N	ë Site	#		Brag. 1	Elev.	8 €	bottom + Lab K (ft) + fre/s)	Lab K	Reth rode	Fld K Neth		- W]	(0.0625 to	3	S		Percent Unit Mt.	SPT No.	SPI Boist, Liquid	Plastic. UC
1 -	1															· ·		3	- 1		177	16061 1657)
141	1000	9 P	2 5	241014	014779	2 2	9		0.0	:				7	=	23	_	22				
•		3 ~		2172	072,45	2 2	0.790		9.5	٠ ١	٠,				i	1	~					
_		۰,		151.7	257620	2	7 00 7	2 6	3 5	7.802-03	•			*	· ·	≈ ;		2 3 ;				
DR 1979		, P7	: ::	45147	672457	. 2	450	× ×	33.5		۰	, A0E-03	_	₹ •	3	23,	_					
_	XE61		•	45142	672652	2	5		35.		• •	4.10E-07										
DR 1979		m		145141	872700	B10	647.5		9.0	1.105-08	**							-				
		m	2	145343	872700	910	647.5		12.0			•		33	2	23	_	۲2 ت ت				
DR 1979	3 KE61	M	2	45141	072700	310	647.5		35.0		•	4.80E-07 ?			!	•						
	_	m	2	142343	872700	930	647.5		35.0		~	2.405-07										
PR 1979		m .	2 :	123	97270	= :	448.6		27.0				13		ř	23	_					
	5 24	w- 1-	2 :		872709		9.8		7.0				M	# I			•	55 55				
-) p	2 5	/2121	2017/0	:	7	3 :	27.0		•	:	•			27	_					
-		·	2 2	1111	F.02/0	3 2	7.70	÷ ;	· ·		-, 0	1.705-07					_	ದ :				
		м	2	115132	907778	=	3 3	, X			-	1000						Α,				
) KES	m	2	445141	872705	Ê		n	40.0			2,105-07						_				
		\$	2	445147	872653	₩	656.3	0.0	-01		•		•				Ī			•	2	
-		m	2	445147	872653	≓	656.3	1.0	5.0									. بر				2.5
		m		445147	872653	록	\$56.3		÷.								_	ہے ا			15.0	2.9
		M	2	45147	872853	¥	656.3		5.5								_	ہر		, 13	i	i
	EEE	ימ	- 2:	445147	872653	= :	656.3		9.0								_	-4			5.0	4.5
		۰ د	2 :	7	202/0	2 ;	656.5		0.0								_	- -!		_	15.0	\$.
-		~ g	2 2	1	2657.0	₹ \$	3	-	12.0								_	-+·			16.0	5.4
	5	-	2 5	1717	1107/0	2 :	9		o .								_	.		••	24.0	e:
	-	, M		15117	1774.44	2 %	447.0		9 4									ر بہ			9 .	2.9
	KE81	100	: =	145147	872644	12	6137											, ,.		- •	12.0	S:-
		m	2	445147	872644	Z	6 5 99		9									. ب		_	0.5.0	ų.
DR 1973	_	m	2	(45147	872644	翠	\$5.5	_	1.5									4			٥.٠	7
	5	\$	2	45147	872644	꾶	663.9		17.0								_	ب ر ا			6.0	2.9
		e: :	2 :	112117	872644	2	\$63.9	20.0	22.0								_	بب			18.0	2.3
		<u>چ</u> •		45142	872649	오 :	662.1	0.0	0								_	=		•••	21.0	6.1
-	1024	o •	• •	71101	872648	2 1	662.1	0.0	5.0								_	٠,			9.6	2.5
		3 M		7101	817778	2 2	·	0.7	÷ 4	30E-08	س							~	115.0		16.7	
		, M		415162	87248	2 5	1 2 2	• •				•					•			E		•
	KEEL	>		115142	972648	3 2	662.1	• 60	> r								- •				0.41	4.5
DR 1973		m	Ċ	45142	872548	Ŷ	662.1	9	12.0								-	.		÷	9	7.7
		m	-	45142	872648	ij	662.1	15.0	17.0									٠,				
	Š.	m	•	445142	872648	2	662.1	8	22.0					-			_	ہبر			0.8	2.2
		g: '	- ≘:	145139	972653	2	526.8	• •	6.5								Ī	-		• • •	25.0	0.3
		w ,	2 :	445139	872653	₽ ;	656.8	0	5.0								_	ہبر			18.0	0. 4
	_	וניי	- -	112139	872653	≘ :	656.8	5.0	4.0								_	بب		_	5.6	£.5
24 14/5	1 KE	~ ı	e :	145139	872653	₽ !	656.8	÷	0.9								_	,,,			15.0	£, 5
_	_	~	2	45134	72653	2	656.8	9.0	9.0								_			_	9.9	4.5

Appendix 3 - HYDSOSEOLOGIC AND ENGIREEPING D	2	OHI AN	16EQ. 06	1C AND	Appendix 3 - HYDSOGEOLOGIC AND ENGINEERING BATA FOR DOOR COUNTY BALEFIEL		TA FOR	9004	COUNTY	BALEFILL	_															
+ IDENTIL	<u>~</u>										+	+ HYDRAULIC			£5 +	+ BRAINSIZE PERCENTAGES	+ HYDGALL C + GRAINSTIE PERCENTAGES + ENGINEERING PROPERTIES +		*	+ ENGINEERING PROPERTIES	6 PROPER	TIES				٠
•		Litho									#	* COMBUCTIVITY			٠	Matri	(I Hatrix	X Matrix	*							•
•		strat.						Ser.	Sass	le Sappi	+				+	N.S.	sand silt clay +	Ü	+	E S	Ħ	ž				•
+ County	_	unit	Hzt.	Site			Brag.	Brng, Elev. to	8	hotto	+	¥ q	#	Fld K Net	5 + Bu	1k Z (2.0 t	to (0.0625	ء ع	•	Soi.i	Percent	Unit Ht.	SPT Koist	Liquid .	Plastic.	3
+ (code) Year (code) (code) No.	Year	(rode)	(code)	ě	ij		2	10. (ft)	€	(ft) (ft) + (cn/s) code	+	(5/8)	8 00	(ca/5) cod	e + >2	.0mm 0.0625	(ca/s) code + 22.0mm 0.0625mm) 0.002mm] ((0.002mm) + Class. P200 (prfl (N) cont.(1) limit index (1sfl +	1200.002	÷	Class.	828	(pr.f)	(10 cont. (2) limit index (tsf) +	2) linit	index	(tsf) +
DR 1973 KEG1 J 10 445139 87265	1933	KE61	n	2	445139		=	656	60 60	M7 656.8 8.0 10.0	-						3 N7 656.8 8,0 10.0 18.0 4.3			ದ			18.0	0		Ş
ä	1973	KEG3		3	445139		*	656.8	.8 10.0	0 12.6	_									ದ			35	٠		4.2
æ	52	DR 1973 KE61	m	2	445140	872644	£	670.B	9	0 2.6	_												<u>e</u>	٥		2.9
*	1973	KEGI	m	2	445140		2	670.	8 2,	3.6	_												22.			
X	1933	EB3	**	2	445140		앞	8.079	بر ده	9.4	_									₩.			13.0	9		
2	1973	TES)	M	9	445140		2	670.	70.8 4.	9.9	_									ದ			20.0	0		5.5

SPT Moist, Liquid Plastic. UC + (M) coot.(2) limit index (t6f) + 2.2 ***** Bult Dry Percent Unit Ht. 9 9200 (pcf) + Matrix I Matrix I Matrix I + EMSIMEERING PROPERTIES
+ sand silt clay + Unitied Bulk Dry
+ Bulk I (2.0 to (0.0225 to + Soil Percent Unit Mt + 72.0ss 0.0525as) 0.002as) + Elass one Fld K Neth (ca/s) code + HYBRAULIC + CONDUCTIVITY tab K (ca/s) Sample Sample + top bottom + t 640.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 658.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 659.0 Brig. 865315 865315 865317 865317 865317 86539 86539 86539 86539 86539 865319 865319 865319 865319 865319 865305 865304 865317 865317 865317 865317 865308 865308 665314 665314 665313 665313 865313 865317 865314 452310 452309 452312 452313 452319 452319 452319 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 452309 45 tithe-strat. unit Nat. + County + (code) Year

Appendix 3 - HYROBEOLOBIC AND ENSINEERING DATA FOR DOOR COUNTY - TONN OF MASHINGTON STIE

•	•	id Plastic. UC +	t index (tsf) +		51 31	42 25			42 25				11 17		30 16			3 2					45 29		46 30			-						
		SPI Moist. Liquid Plastic. 8C	(M) cont. (I) limit	11	1	82			ĸ	69	002		φ.		55	SS		33	15	25			8	ĸ	≅	z								
æ	Unit		(pcf)								•••												5	5	6	108								
PROPERT	Bult	_	P200	₹	96	83			25	23	∓		2		89	55		Ş	8	S														
+ ENGINEERING PROPERTIES	Unified B		Class. P	ದ	ä	ರ	ದ	ದ	ರ	뺉	보	虻	겁	ದ	ದ	귤	멅	ದ	ದ	**	뽀	ದ	ದ	¥	겁	æ.	겁	뺲	ರ	75-XX	ರ	至-5	ಶ	ð
1983 +		- X	ជ ÷																		_													
Kateur I	Ç,		(0,002ma)	#	3	**			\$	₽	22		22		ŝ	2		\$	=	25				φ.		- a								
ES atrix I	5114	(0.0625 to		ភ	*	×			33	28	\$		#		83	\$		s	×	3				83		\$								
E PERCENTASES Hatrix I Matrix I	pars	.0 to 60	625au) ('n	~	=			12	ន	×		=		2	ş		=	=	8				ф.		4								
+ SRAINSIZE PERCENTASES + Matrix I Matri		+ Bulk 1 (2.0 to	+)2.0mm 0.0625mm 0.002mm) ((0.002mm)		۰	2			=	5	33		2		2	×		97	2	25				•	٠	٥								
		Reth					~	~				j					^				-	~					_	r.	1		_		^	•
		FId K	(ca/s) code				2.92E-07	8.43E-26				9.04E-07					4. 35E-05				1.77E-06	5.316-07				٠	4.3£6-0	3.516-06	8.84E-07	2.618-05	2.55£-07	3.016-0	7.498-06	74. 74. 6
١		Seth	ě											~									™	بم چو	6.4									
HYDRALE IC CONDUCTIVITY			(5/8)											2.06-08									4.005-08	7.006-06	1.86.43	1.066-05								
* +	. •	bottos +	÷ :	3.5	16.0	36.0	0.01	40.0	16.0	36.0	40.0	S.0	3.5	24.0	29.0	45.5	8.0	9::	26.0	40.5	40,4	0.0	21.5	38.0	16.0	5:1	3.5	8	31.0	51.2	31.7	19.5	31.3	
	Saple Saple	top D	₹	2.0	5.5	34.5			34.5	34.5	39.5	37.0	2.0	22.5	24.5	44.5	38.0	9.5	24.5	39.5	27.4	5.0	19.5	36.0	14.5	39.52	0	4.5	9.0	45.0	0.0	43.5	9.	
	Surf. S		£	818.4						81B.4	918.4		820.3		820.3	820.3					817.5	816.4			819.5	819.5	822.3	922.0	917.7	818.0	819.1	818.5	819.4	4
	Š	Brng. El.	<u>۔</u> چ	Ē	Z	Ž	#174 #174	2	E	1842	1117	18 2		產	18A3	뎚	2	ž	ž	Ī	ž	ANA A			316	B16	£	3 5	=	2	SAR	1 0	2	
		46	tong.	83158	83158	83158	93158	383158	83151	83151	83151	883151	83128	83158	83158	83158	83158	83151	183151	883151	383151	883141	383146	883201	83128	883128	83141	883141	883138	883138	883158	883128	883201	407344
			Ė	i i		434923						434524 (434932	
		Site	Q	21	=	=	24	=	2	ဌ	2	21	=	엄	2	¥	¤	¤	2	읔	2	2	2	21	2	2	2	2	23	22	£	2	2	:
		ž	(oge)	m	m	**	m	~	n	M	m	-	M	m	M	m	m	M	> >	m	m	m	m	6	m	17	~ >	ħ	m		m	ĸ	m	٠
itho-	strat.	unit	(code)					Ä				3							KEK	3	E.C	KEXI	ij	3	_				EX		Œ		æ	2
_		- -	(code) Year (code)(code)		-		-																	1981								_	_	
DERTITY		County	Code	π	4	껕	ď	#	₫	=	ᄄ	귣	⊏	≖	Ξ.	ヸ	⊏	٣	ば	₹.	₫	ᄄ	깚	Œ	₫	æ	7	ď	ď	≖	롰	Œ	딦	•

SPI Moist, Liquid Plastic. UC (N) cont.(2) limit index (tsf) ሯ Unified Bulk Ory Soil Percent Unit Mt. S Class. P200 (pcf) * ENGINEERING PROPERTIES 甲烷乙烷 计载 中外战略军轮杆路线转位统势引手体 经线路位 农松 22 28 GRAINSIZE PERCENTAGES Fld K Neth (ca/s) code 1.992-04 5.69E-05 3.43E-03 3.20E-05 1.93E-05 1.56E-04 2.53E-03 1.41E-03 7.31E-06 2.95E-04 3.02E-04 Lab K Heth (ca/s) code + HYDRAULIC + CONDUCTIVITY Appendix 3 - Hydroseclobic and engineering dria for green lake coatiy - comiy langfill 7.60E-05 2.50E-06 2.00E-05 Sample Sample + top bottom + it (ft) (ft) + (864.3 866.8 866.8 844.3 844.3 844.3 844.3 844.3 844.3 845.7 817.2 817.8 817.8 817.8 817.8 817.8 817.8 817.9 817.9 Ser. 885499 1792
885499 1792
885499 1792
8855499 1793
8855499 1793
8855499 1793
885549 1793
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1893
8855413 1 Ħ. Litho-strat. unit Nat. Site r (code) (code) No. + County u + (code) Year (

+ Unified Bulk Bry
+ Soil Percent Unit Wt. SPT Moist. Liquid Plastic. UC +
+ Class. P200 (pcf) (N) cont.(Z) limit inder (1sf) + 71 12 13 15 2 2 Ξ 2 2 ***** * 222 z z약 2 2 2 2 23 .3 化ルの 計画 やり 交替 打打 取品 打 自 引 射 ドル 印 に 吹き 5 次分 52 137.1 + ENSINEERINS PROPERTIES + **22** 23 22 Z 3 2 28 28 ವವದ ರರವರದ ದವದ ವವರ ರವದ ದವರ ರಹ ಕು ಹ ದರ ರಹ ಹಿ ದರ್ಶಾ<u>ಜ</u>ರಕ್ಕಿ ರತ್ತದವರಹಿದರ ೫೬ ರ ಕ + sand silt clay + Bulk % (2.0 to (0.0625 to + 72.0m 0.0625m) (0.002m) Hatrix 2 Matrix 2 Matrix 2 88 **第** 13 **₹**5 2 8== 22 8 ಫಜಿ ភ + GRAINSIZE PERCENTAGES 2 2 2 20 **я** ^ 2 0 Fld K Neth (ca/s) code 1.106-07 4.22E-04 3.79E-04 1.24E-06 3.00E-04 2.52E-08 7.205-07 8, 326-05 6.125-07 e Sample +
bottos + Lab K Meth
(ft) + (ca/s) code + HYDRAIL IC + CONDUCTIVITY 1.50E-06 3 4.00E-08 1.106-08 65.0 75.0 88.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 90.0 Sample S top b (ft) (744.7 b.0
744.7 b.0
744.7 b.5
744.7 b.5
744.7 b.5
744.7 53.6
744.7 53.6
744.7 53.6
744.1 53.5
744.1 53.5
744.1 53.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6
744.1 54.6 £ 5. 1430
11430
11430
11430
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431
11431 Brng. 86. 880243 880243 880243 880243 880243 880243 880234 880234 880234 880237 880219 880219 880219 880219 880244 880214 880214 880219 880219 880239 880234 880224 880224 880224 880224 880224 880224 880224 8 (2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2000)
(2 ž unit Mat. Site (code)(code) No. + County sear (+ IDENTITY

ASPENDÍX 3 - HYDROSEOLOGIC AND ENGINEERINS DATA FOR KENOSHA COUNTY - PHEASANT RUM LANDFILL

÷

÷.

SPT Moist, Liquid Plastic, UC + (W) cont.(I) limit index (tsf) + 2.5 1.5 3.6 £ 5 3.0 2 2 2 22 2 2 \$ 23 27.0 28882222 ****** 2222 8288 13.4 = 22 = = 22 22 ರವರೆದದರರದದರರದದ ೫ ವ ಔ ೩ ೫ % ರವಧರದದ ಜ ೫ ೫ ಜ ಕ $\begin{array}{c} \mathtt{d} \, \mathtt{$ + sanó silt ciay Fid K Neth + Bulk I (2.0 to (0.0425 to {ca/s} code + 72.0se 0.0425se) 0.002ne) ((0.002me) # # ₹ 8 # ∓ **7** 3 2 2 12 ŧ æ % SRAINSIZE PERCENTAGES 3 t 35 2.55E-07 1.70E-04 1.01E-07 1.02E-02 9.23E-08 1.53E-07 3.49E-06 4.22E-07 2.11E-06 7.40E-07 1.20E-07 3.80E-07 4.20E-07 5.50E-07 1.54E-07 3.39E-05 1.27E-04 Heth Code * CONDUCTIVITY 2.00E-08 1.10E-05 6.306-08 + HYDRAULIC 4.20E-08 Lab X (ce/s) Samile + bottom + i 88.5 113.5 113.5 15.5 15.5 123.5 88.5 731.2 731.2 731.2 731.2 731.2 731.2 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 731.4 73 Brog. 6 88440
88410
88410
88410
88410
88410
88410
88410
88410
88410
88410
88410
88410
88410
88410
88410
88410
88410
88410
88410
88410
88410
88410
88410
88410 880245 880245 880245 Long. 880247 880247 BB0247 BB0247 B80247 880239 880247 B80220 880239 880239 880239 880239 880239 880239 680230 680230 880225 680225 680225 880247 880247 \$80239 423333 423333 423333 423336 42334 42334 42335 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 4233 4233 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 42333 4233 unit Hat. Site (code)(code) No. + County u + (rode) Year (**DENTITY**

Approdix 3 - Hydkóbeolóbic and Ehrineering data for kenosha coraty - parasant run landfill

SPI Moist. Liquid Plastic. DC + (M) cont. (X) limit index (tsf) + 8 % ≈ z 5 + HYDRARIC + GRAINSIZE PERCENTAGES + EMBIREBRING PROFERTIES
+ COMDUCINITY + SALTY X MATTY X HATTY X HA ದ ದ 88 = 2.205-07 3,255-06 3,605-03 5,70€-06 2, 406-07 1, 335-06 5,606-07 733.4 733.8 733.8 732.8 732.8 701.1 701.1 702.8 703.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 723.3 Surf. Brng. Elev. Long. no. (ft) 42356 880242
42350 880742
42350 880740
473520 880240
473520 880237
47351 880213
47351 880213
47351 880213
47351 880213
47351 880213
47351 880213
47351 880213
47351 880213
47351 880213
47351 880213
47351 880213
47351 880213
47351 880213
47351 880213
47351 880213
47351 880213
47351 880213
47351 880213
47350 880218
47351 880213
47350 880213
47350 880213
47350 880213 : Lithn-+ Strat. + County unit Mat. Site + {code} Year (code) Ko. + IDENTITY

Appendix 3 - Hydroseologic and engineering data for xenosha county - Pheasant rum Landfill

SPI Moist. Liquid Plastic. UC + (M) cort.(Z) limit index (tsf) + 2.0 3.7 3.0 2.0 25.00 4:15.00 E.S. 25.00 E.S. 25. n 15.0 14.0 14.0 17.0 17.0 24.0 13.0 14.0 14.0 14.0 14.0 14.0 15.0 15.0 3 A Z 85228238 Unified Bulk Dry Soil Percent Unit Ht, S Class. P200 (pcf) (ENGINEERING PROPERTIES ರದರವರರದರರದವರದರವರದವರ್ಧಧರ್ಣ ಕ್ರಿಕ್ಕಿಸ್ ಕ್ರಿಸ್ ಕ್ರಿಕ್ಕಿಸ್ ಕ್ರಿಸ್ ಕ್ರಿಕ್ಕಿಸ್ ಕ್ರಿಕ್ಕಿಸ್ ಕ್ರಿಕ್ಕಿಸ್ ಕ್ರಿಕ್ಕಿಸ್ ಕ್ರಿಕ್ಕಿಸ್ ಕ್ರಿಕ್ಕ್ ಕ್ರಿಕ್ಕಿಸ್ ಕ್ರಿಕ್ಕಿಸ್ ಕ್ರಿಕ್ಕಿಸ್ ಕ್ರಿಸ್ ಕ್ 23 돌 F16 K 1 Lab K Heth (ca/s) code + HYDRAULIC + CONDUCTIVITY 7 % T Sample Sample + top bottom + i 96.6 102.0 102.0 116.5 121.5 121.5 121.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 131.5 1 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40.0 784.9
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3
789.3 MANAGE COMMENS £rng. ₽0. MASS OF SERVICE SERVIC 87355 87355 87355 87355 87355 87355 87355 87355 87355 87355 87355 87355 87355 87355 873454 873456 873456 873456 873456 873456 873456 873456 873456 873456 873456 873456 873456 873456 873456 873456 H7827 t Lithostrat.
Comty unit Nat. Site
+ (code) Year (code) Koo. + IDENTITY

Appendíx 3 - Hydrogeologic and encineerins data for kebaunee county langfill

SPT Moist, Liquid Plastic. EC + (N) copt.(2) limit index (tsf) + 8 8 7 9 8 7 8 8 8 8 8 8 8 222222 3.5 4.5 2 2 2 20元 æ 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 13.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 12.0 5.0 5.0 5.0 5.0 ងន = + Unified Bulk Bry + Soil Percent Unit Mt. + Class. P200 (pcf) 127.0 117.8 121.6 120.5 108.0 * ENGINEERING PROPERTIES 23 2 28828228282 Natrix X Hatrix Z Hatrix X + + sand silt clar + Bulk I (2.0 to (0.0625 to + 22.0ee 0.0625ee) 0.002ee) ((0.002ee) * * * * * * * **\$** \$ 2 4 2 * GRAINSIZE PERCENTAGES 2288228222 2 2 Fld K Neth (ce/s) code 6.00E-07 bottos + Lab X Meth (ft) + (ca/s) code + HYDRALLIC + CONDUCTIVITY 2.10£-08 2.70E-08 2.80E-08 1.10E-08 3,706-07 2.40E-07 3,605-08 2€ 744.8
744.8
744.8
744.8
744.8
744.8
744.8
744.8
744.8
744.8
744.8
744.8
744.8
744.8
744.8
744.8
744.8
744.8
744.8
744.8
744.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8
748.8 Bev. 873515 MAS 873516 MAS 873515 MAS 873515 MAS 873515 MAS 873515 MAS 873515 MAS 873516 MAS 873515 MAS Brag. no. 873504 873504 873504 873504 873504 873504 873504 873504 873504 873505 Legi 44.822 44.822 44.822 44.822 44.822 44.822 44.823 44.823 44.823 44.823 44.823 44.823 44.823 44.823 44.823 44.823 44.823 44.823 44.823 44.823 44.823 44.823 44.823 44.823 442827 442827 442827 442827 442827 442827 442827 442827 442827 442827 442827 442827 442827 442827 442827 442827 442823 442823 442823 142827 442823 <u>:</u> Site 8 strat. + County unit Nat. Si + (code) Year (code) (code) No ž ž KET.

Appendix 3 - Hydrosequebic and ensineering data for Kemalnee County Landfill

+ \$PAINSIE PERCENTAGES + ENGINEERING PROPERTIES + Hatrix I Matrix I Matrix I Hatrix I Hatrix I + sand sill cray + Ubified Bulk Dry + tax 1 Cato to Cars to + 50ii Percent Unit Bi. SF7 Boist. Liquid Plastic. UC + (texts) code + 72.0ss 0.0425as) ((0.002as) + Class, P200 (pcf) (M) cont.(I) limit index (isf) + :: :: 12.0 15.0 13.0 119.3 127.9 126.3 115.0 124.3 123.0 115.5 115.4 128.7 # ದ ರ ಜ ದ ರ ದ ಹ ದ ದ ದ ದ ದ ದ ದ ದ % 2225 经货品的现代 + HYDRALE IC + CREDUCTIVITY Sacin Sapie + to button tab K Meth F (ft) (ft) + (cs/s) code (3,506-08 Appendix 3 - HYDROSECKOSIC AND ENGINEERING DATA FOR KENAUNEE CORNTY LANDFILL 781.0 781.9 784.9 785.1 785.1 785.1 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 Brng. Elev. no. (ft) 873506 873506 873505 873507 873507 873508 873510 873510 873510 873510 873595 873505 873505 873505 873511 873511 873504 873506 873506 873506 873506 442824 442828 442828 442828 442828 442828 442828 442828 442828 442828 442828 442828 442828 442828 442828 442828 442828 442828 442828 442828 442828 442828 442828 442828 unit Mat. Site (tode)(code) No. Ĭež. + IBENTITY

<u>~</u> 2.8

2 2

+ thistised Bulk Dry + Soil Percent Unit Mt. SPT Moist. Liquid Plastic. UC + + Elass. P200 (pcf) (M) cont.(E) limit index (tsf) + 2 % 2 % 9.1 11.8 9.3 11.9 10.7 55.0 21.0 25.0 26.0 19.0 118.9 121.3 130.3 122.2 125.4 28. 132.1 ≈ ≈ 222282 ***** 고 55 년 로 고 55 년 로 고 55 년 로 ದ **ಕ** ರ DOCUMENT 23 = = * * Appendie 3 - Hydrögeologic and enginkering data for hantongc courty including lenerger, papposed hantongc equity, and ribsevien sites 3,00E-05 3,60E-06 3.606-05 Neth code + HYDRALL IC + CONDUCTIVITY 1.25£-07 2.65£-05 Sapie + bottom + Lab K (ft) + (cm/6) 4.61E-07 2.21E-07 1.586-05 45450 45450 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 4550 Sample S top (ft) 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 881.1 881.1 881.1 881.1 881.0 881.0 881.0 881.0 991.3 991.3 991.3 991.3 991.3 991.3 991.3 Sert. Brag. 1 CS1 (CS2) (CS2) (CS2) (CS3) (C 874944 875048 875048 875048 875049 875047 875047 875041 875041 875041 875041 875041 875041 875041 875041 875041 875041 875012 875012 875012 874999 875010 875010 875010 875010 875010 875010 875010 875010 874999 874999 874999 874999 874999 Long. 441099 441099 441099 441099 441099 441099 441030 441030 441030 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 441031 unit Mat. Site (code)(code) Mo. + County u + (code) Year (

+ Unified Bulk Dry + Soil Percent Unit Mr. Syl Maist. Liquid Phast + Class. Proo (pcf) (W) cont.(1) limit inde Cl. 10 125.9 12.2 26 SN-SC 25 25.0 12.4 28 SN-SC 25 25.0 12.4 19 SN-SC 25 25.0 12.4 12.4 11 SN-SC 25 25.0 12.4 12 SN-SC 25 25.0 12 SN-	5 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
# Unified Bulk Dry # Soil Percent Unit Mr. # Class. P200 (pcf) C C 3 30 C 7 10 125.9 SW-50. 73 S	
# Unified Bulk Dry # Soil Percent Unit Mr. # Class. P200 (pcf) C C 3 30 C 7 10 125.9 SW-50. 73 S	** ******
# Unified Bulk Dry # Soil Percent Unit Mr. # Class. P200 (pcf) C C 3 30 C 7 10 125.9 SW-50. 73 S	13.7 10.8 10.8 12.0 10.4 10.1
1863 1863 1863 1863 1863 1863 1863 1863	25.0
1863 1863 1863 1863 1863 1863 1863 1863	138.5
1863 1863 1863 1863 1863 1863 1863 1863	:
	ರದದರದಣ್ಣದದ% 8 ಹ ಹೆಚ
2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	
20 C C C C C C C C C C C C C C C C C C C	22 22 23
CHEF SITES SEES Batrix 1 Matrix 2 10.0625 to 0.002as1 ((0.002as) 51 25 52 29 53 29 54 25 55 29 54 47 57 47 58 49 59 49 59 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50 49 50	25 4 25 4 25
AND RIDGEVIEW SITE Natrix 1 Batrix 1 Sand Silt (2.0 to 10.0625	**********
CCOUNTY, AND RIDGEVIE + SCAINSITE FREEHINGES + Bair 1 7.0 to 10.0 + 72.0ac 0.0625aa) 0.0 13 20 20 20 20 20 20 20 20 20 20 20 20 20	* F E E E E E E E E
0.000 C	
Fig. Fig. Mail Tonic County Mail Pace Exercises, Proprose Mail Pace Mail Pac	
829 A B B B B B B B B B B B B B B B B B B	-
4,725-08 4,725-08 4,725-08 6,855-08 8,855-08 8,635-08 7,476-08	4.285-07
25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0	20.0 20.0 31.0 23.0 35.0 36.0 36.0
C COUNTY (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140) 1 (140)	26.55 3 2.55 5 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
MITIDAGE ttp://www.mitidage.com/ ttp://www.mitidage.c	894.8 1 905.6 195.6 898.9 1 898.9 210.6 3
Surt. Bring Eller.	1883 6 1883 6 1884 9 1884 9 1884 9 1884 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 1885 9 18
BY 1346 1847 1846 1847 1846 1847 1846 1847 1847 1847 1847 1847 1847 1847 1847	7452 74946 75010 75010 75007 75007 75007 75001

20	*****

\$ 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	
DENTITY Code Very Code	KEVA KEVA KEVA KE KE KE KE KE

Ropend	2	MUMBER	1 3190	AND ENGIN.	ERING D	12 E	MAKE A	302		DING LENGER	(SEB., PS	FOPEGET S - SYTHOGERE AND ERGINERANG DATA FOR MANITONIC COUNTY INCLUDING LENGERGER, PROPOSED MANITONIC COUNTY, AND RINGEVIEW SITES	ESC COUNTY,	AND RIDGE	VIEW SITES									
DENTITY		;							-	P HYDRALL IC			+ SEATING 1	GRAINSIZE PERCENTAGES	æ		+ ENGINEER	ENGINEERING PROPERTIES	1165					
	_	: # - #							•	+ CONDUCTIVITY	/11X		-	Natrix I Hatrix I	fatrix 1	Matrix 1								
		strat.	1				Ş.	Sapie						gues	si)t	413y	+ Unified	E	Ž					
(code) Year	Year	icode) (code)	t. Site de) No.	; : :	. Long.	 		\$ €	bottom +	1 Lab K 1 (cs/s)	Ket Code	Fld K Meth (ca/s) code	+ Bulk 1 + >2.0ss 0	_	(0.0625 to 0.002ms) ((0.002mm)	0.002mm)	t Soil	-	Percent Unit Wt. P200 (act)	SPI Moist. Liquid Plastic. UC	t. Liqu	id Plast	Plastic. UC	-
至	1983	KEVA	3 28	3 44103		i	!	0	1						9		1		-			•		. ;
至	8	KEWA	~	14103			3 870.6						• =	* =	<u> </u>	3	# E	2 ;		22.0	15.2			
폿	1983	3	2	44103									2 5	ខម			2	3 3	133.3		7.1			
Ë	1983	S		14104			8 905.1	7.5					2 5	8 8	2	ź	7 7	2 5	=				:	
₹	1983	KEN	3 16	44104			_						2 5	3 5	2 :	₹ 2	5 i	: د	•	43.0	9:5	≂:	= :	
ĕ	1983	3	; ≈ , m	14104						4.95E-08	-		3 €	3 6	ž	2 5	# S	=		•		2 2	≘ :	
差		噩	3 14	14104			9 910.4	4 24.5					2	: P	3 4	: :	3 2	≩ 2				e:	.	
委		KEVÀ	×	411042	2 875005	8	•		5.6.5	1,515-07	-			; =	2 25	ន	ೆ ದ	* 88	128.7		9 2	3 %		
₹		KEVA	3	5 44104.			_			3.946-08	. <u>.</u> .		7	B	#	9	æ	-	2	: =		3 6		_
ž	1983	3	n	44104				4 19.5				-	25	25		:	25-15	A		0.00		2	2	
ž	28	3	≈	× #10£		£	-						ĸ	S			34	5			2	2	2	
쯮	1983	KEVA	≃ m	¥ #10#			•			1.876-08			Ĺ	38	#	*		• • •	128.9			. ×	: =	
至	1881	KEYA	≃	44104			2 904.5						X	×		ŀ	- E	3		:		2	2	
季	8	KEVA	~			284							==	2	=	45	. =	: 64		=		ž		
Ē	1983	KEVA	2				•			2.926-08	_		^	22	*	8	-		8	. K	· ·	: :		٠.
Ž	188	š	= n			0 893	-						\$	i i		i	35			•				
₹.	1983	5	n H				-						Ş	B			39-15		~	200.0	•			
2	£	KEVA	≍																•	-		s	2	
Ž	ž.	KE'S	3 16				+:03 +:03 -			5.566-08	_		00	2	4	23	: ਹ	3	120.4			3 8	: 5	
Ž	1983	KEW	≃ +										ñ	*3	:	i	2 第			•			•	
Ž	86	(E/U)	≈					9 17.0					B	2			8	123						
Ž	1983	KEYA	r n	44104									**	78	8	74		3			•	5	2	
풒	188	KEVA	~	4410H			915.9						8	77	6	=	5					3 5	5 5	
垄	1881	KEYA	۳ ۳										90	23	=	2	2	. =				2 2	2 =	
柔	1963	KE	35			5 TP13							•	2	9	K	ಚ	3				: 10	: 12	
æ	1983	KENA	≓ m	44102									12	35	4	2	. Z	: 2				: :	: ::	
ž		3	2	5 #101.			-						8	ĸ	8	12	5	\$: 10	1 15	
菱		KEVA	i m	\$ 41 01			5 903.8						•	23	*	2	a	2						
菜		KEVA	3 15	44101									9	8	*	7	ء ا د	<u> </u>			-		9	
준		\$	= m	\$ 44103				12.0	0 13.0				· 23	; #3	: 4	; =	; z	: #	•		•	3 5	2 2	
쥺		KEYA	3 16	10114									W [*]	* *	2	: :	\$ 2	3 5					: 5	
ž		KEVA	~	44101			7 908.3						1 447	1 7	: #	: 7	1 2	: *					2 5	
Ē		3	31	3 44105									167	: 8	3 2	. p	3 2	2 5			•			
ž		KEVA	-	\$ 44101									^	8		; ?	1 2				•		. :	
歪		KEVA	2	14103										1 =	: 4	3 7	3 2	2 5			•		٠:	
差		쎂	=	441033		8 IP19	986.6	9.0	0.6					: 3	?	4	3 5	2 \$			•		<u>.</u>	
ž	1983	뽀	* 15	5 441034			_						- =	3 8			i i	<u>}</u>						
ž	1883	KEVA	31	44101		1P20		8 11.0	0.21				; *	: 23	5	25	: ਰ :	2 2						

SPI Noist. Liquid Plastic, UC + (N) cont, (I) light index (tsf) + ~ E E C E C E ~ 22 2 22 2 2 222222 : Unified Bulk Dry + Soil Percent Unit Nt. Sl + Class, P200 (pcf) U + ENSINEERING PROPERTIES 252324224242424242222 ರರದರದರದ ಈ ರಜ್ಞಾನ ಹಿವರ ನರಹಿರದ ದ ಜಿ. ಹ ಹ + Matrix I Matrix I + sand silt clay : Fid K Meth + Bulk I (2.0 to (0.0625 to + (te/s) code + 72.0m 0.0625m) 0.002mal + 17 \$ # Z # 2 2轮4路轮移时路路 ₽; ROPENTIX 3 - HUDROSEDLUGIE AND ENGINEERING BATA FOR NANTIDADE, COLNIY INCLUDING LENEERGER. PROPUSED MANTIONOC COLNIY, AND RIBGEVIEW SITES \$ \$ けされなななななけ 4 12 **++++** + GRAINSTIE PERCENTAGES Sample Sample + top K Heth (ft) (ft) + (cm/s) code + HYDRAULIC + CONDUCTIVITY 919.8 896.7 888.8 915.9 901 901 874.7 882 882 882 897.1 708.3 906.5 906.5 913.2 913.2 913.2 Surf. Brng. Elev. Long. no. (#t) 874951 1720 874945 1721 874946 1722 874945 1722 874945 1723 874945 1723 874945 1723 874942 1723 874944 1731 874944 1731 874944 1731 875004 176 875004 176 875007 177 875007 177 875007 177 875007 177 875007 177 875007 177 441014 87945 141014 87496 141008 87495 141008 87495 141008 87495 141008 87495 141003 87495 141003 87594 14100 875004 14104 875007 14104 875007 14104 875007 441013 41044 ij strat. + County unit Mat. Site + (code) Year (code) (code) No. 75 ES * IDENTITY

Mat. Site Page	+ IDENIITY +	lithe-	Ł								+ HYDRAULIC	31		1895	GRAINSIZE PERCENTAGES	TAGES	•	ENGINEERING PROPERTIES	NG PROPER	TIES				
March Marc		ŧ	ندو					S.		e Saspie	• +			• •	Matrix X	Matrix X	Hatriz I +	lbition.	à	45				
18 16 17 151479 880579 186 7727 150, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20.5 15, 20	onty ode) Ye		e) frod				Brng.	₩.	_	bottoe (ft)	+ Lab K (58/s)		Fld K Reti		% (2.0 to	_	\$ (a.600.0)	Soii	Percent Pond	libit ign		foist. L	iquid Pl	etic. 1
1	1			-	15,180	- 1	-	1	,	1	-	•				•						7 (31 -) 80		noex 1
19 12 13 13 13 13 13 13 13				: :	15,1400													ದ	ş	116.1	22	15.9	* 2	=
100 1 1 1 1 1 1 1 1	•		۳ د د	: :	16,100								:					ದ	23	126.7	8	12.5	æ	=
1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141 1411-141	•			:: 									96-96	~				ರ						
1991	٠.		٠.	≘ :	421495			•					1.44E-05	,				ವ						
1991			2	=	\$1 \$4								2.05E-06	~			٠	a						
1891			, W	3 13	421489										73			3	×	8		~		
1981			ш	-	\$1			۵.	23.5				•					i	;			;		
1981 RE 3 17 451479 860579 813 815, 615, 615, 617, 817, 817, 817, 817, 817, 818, 817, 815, 815, 815, 815, 815, 817, 817, 817, 817, 817, 817, 817, 817			ш	3 27	451489				10.0					-				b	=		3 ;	7 0		
1981 15 17 451479 880579 1814 785.5 45.0 51.0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 451,0 1.1816-05 7 33 4 4 1.1816-05 7 33 4 4 1.1816-05 7 33 4 4 1.1816-05 7 33 4 4 1.1816-05 7 33 4 4 1.1816-05 7 33 4 4 1.1816-05 7 33 4 4 1.1816-05 7 33 4 4 1.1816-05 7 33 4 4 1.1816-05 7 33 4 4 1.1816-05 7 33 4 4 1.1816-05 7 33 4 4 1.1816-05 7 33 4 4 1.1816-05 7 33 4 4 1.1816-05 7 33 4 4 1.1816-05 7 33 4 4 1.1816-05 7 33 4 4 1.1816-05 7 33 4 4 1.1816-05 7 33 4 4 4 4 4 4 4 4			بىر	3	451499				15.0									\$ 2	3 \$		7 5	. ·		
1881 18 18 18 18 18 18			نفا	11	451499			•		-				•				3	¥		7	•		
1981 1881 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882 1882	_			: :	45120							٠	3,200-00					SC. Rock						
195 185 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195 195				::	2								1.816-05	_				SC, Rock						
1981 15 3 14 514199 8805599 11418 80057 55.46 70.11 1.996=-05 7 1.996=-05 7 1.996=-05 7 1.996 115.01 1.906=-05 7 1.996 115.01 1.996 115.01 1.996 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.01 115.	٦.			: :	45164										7 33			랖	5	119.0		13.0		
1951 KE 5 17 451459 800579 M148 ROA7 65.6 70.1 4.18E-65 7 8 8 8 8 9 9 1 1 1 1 1 1 1 1	•			: د	42143								1.906-05	~				뽀						
1981 KE 11 741479 880579 815 15.0 16.5 15.0 16.5 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19.			M.	2	421499				_				1,185-05	-				9						
1941 KE			14	2	4514%			_	15.0						500			5	=		2			
1981 If					451499			_	£5.0						8			8	. "	101	2 5			
1981 KE 5 17 451479 806259 KI44 80236 M14 80239 M14 M14			į.	====	451495				0.03						!			; 8 ;	•		2 5			
PMS KE St 17 451479 805559 K246 827.6 91.0 94.5 5.13E-04 7 91.0 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 91.5 9				2	451499				35,0						11			3 2	ě	111 7	÷ ş	,		
1943 KE 54 17 451479 800559 K24A 80254 K24A 80255 K24A 10.0 11.5 1945 KE 5 17 451479 800559 K24B 80254 K24A 80255 W27 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5			rī S	11	451499		_						3, 906 - 06		:			: 2	8		3	7.7		
1961 KE			in The		451499								1 1X-01					3 3						
1981 KE 5 17 451479 806559 824 32,0 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5 40,5			إيرا		451499										63			2 2	•		193			
1981 KE 1 151449 880559 Du27 10.0 11.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5		25	ш	5 13	451499													* 3	• 5		2 8			
1981 KE 5 17 451449 880539 DAZ2 70.0 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5		£			451499				10.0						ة ة د			2 2	6		3 2			
1911 KE 1 151419 880539 823 70.0 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70.5 70		83 K	w	2	451499				9						2 5			, ,	٠;		₹ ;			
1981 KE		*		6	451499			-ـــــ	76.0						9			2 8	τ,		= {			
1961 KE 3 17 451449 880559 835 805.8 8.5 10.0 0 16 16 17 17 17 17 17 17		81 X	Ш	1 17	451499				28									5 8	7		≘ :): ::		
1981 KE 3 751479 880539 83.5 83.5 17.0 18 0.1 84 0.1 19 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 17 <td></td> <td></td> <td>, w</td> <td>3 17</td> <td>451499</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>``</td> <td></td> <td></td> <td>ኧ ፡</td> <td>7 8</td> <td></td> <td>æ;</td> <td></td> <td></td> <td></td>			, w	3 17	451499										``			ኧ ፡	7 8		æ;			
1981 KE 1 43149 800399 810 52 54 DNR JE 3 73149 800399 818 50.7 173.6 134.1 173.6 134.1 173.6 134.1 173.6 134.1 173.6 134.1 173.6 134.1 173.6 134.1 173.6 134.1 173.6 134.1 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6 173.6<			141	21	451469				_						2 5			d :	≅					
DRM IE 3 17 451479 800359 NA 18 86.7, 127.6, 134.1 1.36E-65 7 1961 KE 3 17 451479 880359 NA 18 86.7, 127.6, 134.1 2.96E-05 7 5C 26 1961 KE 3 17 451479 880356 NS 80.5, 0.27.5, 28.5 3.40 3.7 5C 26 1961 KE 3 17 451479 880356 NS 80.5, 0.40, 0.40, 0.40 1.0 3.7 5C 26 1961 KE 3 17 451419 880356 NS 80.5, 0.40, 0.40, 0.40, 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40			سو	=	567157										2			ದ :	7					
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,				: :	25.460		•								2 -			55	23					
10	_			2 -	75.150		_		7.75				1.385.05	~				X						
1998 KE 5 17 431429 8805346 83 8054,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 354,0 35				::	100000				123.6				2, 965-05					쓞						
1761 K. J. 17 451429 880536 B. 8054,0 35.0 36.0 17 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72 72		2 2		: :	47.0									_	 K		,	S	*		7			
1981 KE 99 17 451429 880535 B 8 805.0 40.0 41.0 1 16 E1 94 1981 KE 4 17 451419 880532 B 8 805.2 5.0 6.0 100 SP 7 1981 KE 4 17 451419 880532 B 8 805.2 B 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8		¥	. بد	~ ~	421425										3 23			4	72		8			
1981 KE 4 17 451411 880532 B4 823.0 5.0 6.0 0 100 5.9 7 100 100 5.9 7 100 100 100 100 100 100 100 100 100 1		 	ф		451429			•							16			2	7		3			
1981 KE 3 17 451415 880542 BS 804.6 15.0 16.0 46 76 5F-5H 16.0 18.0 10.0 10.0 10.0 10.0 10.0 10.0 10		æ		-	451411										2			2	; '		: =			
1981 KE 4 17 451414 680532 84 812.4 5.0 6.0 0 0 100 SP-51 16 17414 880532 84 812.4 5.0 6.0 0 100 SP-51 17 17 15144 880532 84 812.4 10.0 11.0 0 100 100 SP-51 17 17 15144 880532 84 812.4 10.0 11.0 0 100 100 SP-51 17 17 15144 880532 84 812.4 10.0 11.0 0 100 100 SP-51 17 17 17 17 17 17 17 17 17 17 17 17 17		<u> </u>		1	451415									•				s č	٠:		= ;			
1961 KE 4 17 451444 880532 84 812.4 10.0 11.0 0 100 5P 5		18 X	, Lu	71	451414													EC. 46	2		Ş			
198			ر.	1	11111				_									i i	•		a			
			, 14	: :	10.000													4	٠.		:			

	 + GRAINSIZE PERCENTAGES	Batrix 2 Matrix I Batrix 1	series the base
	 + 68AIN	•	4
THE COOKIN	 + HYBRAULIC	+ COMBUCTIVITY	Cust Canta Camin A
RODEROIX S - MIDROSELLUSIC AND ENGINEEKING URIG FUN RANDUCE		Litho-	Set 24
* x tou-addy	 + IDEKIITY	•	•

				ı																	
•		¥	(484)																		
		astic.	limit index (tsf)	•	**	ន		=	Ξ		•	2		00	00		'n	•	•	۲.	4
		P Sing	=	2	S	57		=	Ħ		æ	7		ĸ	73		2	Ħ	£	2	7
		ž	Æ æ																		
		Mois	cont. (2)	<u> </u>																	
			*																		
	ć	hit	(pcf)																		
	alk	rcent 1	P200	29	2	8	7	85	ŝ	#	43	3	5	-9	2	7	S	3	29	25	7
				ದ	ದ	Ξ	¥5	ಚ	ş	芫	ಕ	ᆸ	55	ದ	ದ	S	#	#	무건	#	- F
			Elass.														ä	ä	占	Ċ	Ž
*	*	•	÷					22		•	13										
Š	Ċ₹		(ca/s) code +)2.0ss 0.0625ssi 0.002ss] ((0.002ss) +																		
M X		25 to	, [88]					\$		×	×										
1	Š	60.09	8.0															_	_		
Ž	bes	0	625883	7	5	~	3	5	3	3	S	8	22	×	×	æ	\$	=	ŝ	7	
*		1 4	Des 0.0	~	۲.	0	7	٥	, - ,	•	۰	-0	'n	•	~	m	~	٥	 .	m	<
	+	+ Bu}	+ >2.																		
		Ę	ğ																		
		F16 X	[S/#3]										•								
<u></u>		Het:	a Code																		
+ COMBOC: 18113		¥	{\$/																		
5	+	<u>-</u>	+																		
	Sample	bottos	(ft) (ft) + (cm/s)	10.0	25.0	5.0	10.0	15.0	5.0	8	20.0	15.0	25.0	20.0	10.0	25.0	10.0	15.0	15.0	9.0	ş
	Saaple	ş	£5																		
			€	916.7	316.7	836.4	8.4	836.4	864.0	864.0	860.5	860.5	860.5	868.7	870.2	B70.2	9.138	€.	833.7	832.7	5
	Š		ë.	26	æ	22	22	罂	£	8	2	2	88	B 12	Ħ	Ē	3	B 16	B 17	8 18	9
		Ä	Leng.	892842	2842	2846	2846	2846	2851	2851	2854	2854	785 785	2825	2858	12858	2858	2846	2846	ž	200
			7	434710 89																	
				₹	₹	\$															
		Sit	e) #0.	5 29	5	S 29	5 5	2											2 2		
ě	<u>:</u> :	unit Mat.	le) tcod	藏	-··	3	燕	黄											3		
=	Stri	ti en	¥ (to	_																	
		2	ode) Year	6761 0															61 Q		
		ŝ	8	, ac	Σ:	**	Ē	•	×	×	=	**	=	-	¥.	#7	=	=;	*	~	*

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR RACINE COUNTY - (MEPCB) CALEBONIA SITE

+ IDEXIII											HYDRAUL I				+ GRAINS	IZE PERCEN	TAGES		+	ENSINEERI	NS PROPE	RTIES			
•		Litho-								+	CONDUCTI	VITY	-		•			Matrix I							
+		strat,						Surs.	Saani	e Sample +					+	sand	silt	clay		Unified	Retk	Drv			
+ County		unit					Braç.	Elev.	top	bottos +	Lab K	Heth	Fld K	Reth	+ Bulk I	(2.0 to	(0.0625 to	· · · · ·	+	Soiì	Percent	Hait Mt.	SPT Koist.	Liquid Plastic. UC	
+ (code)	Year	(code)	(code)	No.	Lat.	Long.	no.	(ft)	(ft)	-{ft} +	(ce/s)	code	(ca/s)	code	+ >2.0aa	0.0625ea)	0.002am)	((0.002mm)	ŧ	Elass.	P200	(brd)	(N) cont. (2	limit index (tsf)	
																						-p		· ••••• • • • • • • • • • • • • • • • •	
	1977		3			875028		705.8							0	32	58	10			74		4	1.0)
	1977		3		42503.			705.6							8	11	64	25			91		23	4.5	í
	1977		3		125031			705.8							0	11	64	25			91		14	4.5	i
	1977 1977		3		425031 425031			705.6							0	11		30			92		15	4.0	,
	1977		3		425031			705.6							0	10					93		14	3.5	i
	1977			20	425031			705.6							0	8		27			94		16		
	1977		5		425031			705.6							13	٧.					15		11		
	1977			20	425031			705.6	40.0						3	11		21			88		19	4.5	i
	1977			20	125025			711.8							0	15					90		46		
	1977			20	425025										Đ	14		24			89		3	1.8	į
	1977			20		875033		711.8							0	13		23			91		22	4.5	i
	1977		_	20		875033		711.8							0	10	-	25			92		25	4.5	
	1977		3			875033		711.8							Q.	8		30			94		18	4.5	i
	1977		5		125025			711.8							0	4		35			97		11	2.5	
	1977		3		425025			711.8							9		92				100		20	2.8	
	1977	-		20	425025			741.6							14	26	57	17			64		11	2.5	
	1977			20	425025			711.8							0	9					92		15	1.8	
	1977		99			875023			1.5						0	10	73	17			92		14	1.5	•
	1977			20	425024				5.0						2	19		30			82		3	1.5	Į.
	1977			20	425024				10.0						!	13		23			89		12	3.0	
	1977			20	425024				15.0						:	9		23			92		21	4.5	
	1977			20		875023			20.0						3	8		23			91		18	4.5	
	1977			20	425024				25.0						0	3	_	. 8			98		15	2.5	
	1977			20	425024				30.0							3		35			97		14	3.5	
	1977			20		875023	£3		35.0						7	10		35			91		13	3.0	
	1977			20	425024				40.0						3	H	60	29			98		15	4.0	
	1977			20	425020				1.5						0	15	-	21			84		10	2.0	r
Ra	1977	0C		20	425020				5.0						12	20 32	65 57	15 11			82		3		
Ra	1977	BC		20	425020		EA		10.0						16	32 26	40	14			63		14	2.0	
	1977			26	425020				15.0						0	4		47			54		15	2.0	
Ra	1977	38		20	425020				20.0						, v	ì	49	50			96		11	3.0	
Ra	1977	Œ		20	425020				25.0						,	3		50			99 99		14 12	3.5	
Ra	1977	90	5		425020				30.0						۸ .	2		45			99		12 P	3.0	
Ra	1977	OC.	5	20	425020	875047	C4		35.0						, ,	3		52			77 98		-	2.0	
Ra.	1977	30	5	20	425020	875047	C4		40.0						Å	2		50			99		11 9	1.8	
Řà.	1977	30	3	20	425019	875032			1.5							17	-				85		7	2.8 2.0	
Ra	1977	ĐC	3	20	425017	875032	C5		5.0						2	10	64	26			90		18		
Ra	1977	90	5	20	425619	875032			10.0						16	58		6			37		18	4.5	
Ra	1977	DC	5	20	425019	875032			15.0						25	83	16	·			15		19		
Ra	1977	OC	5	20	425019	B75032	C5		20.0						10	78		2			22		11		
Ra	1977	OC.	5	20	425019	875032	C5		25.0						13	72	23				26		13		
Ra	1977	9€	3	20	425019	875032	£5		30.0						0	10	79	11			95		20	4.5	:
89	1977	DC	3	20	425019	875032	€5		35.0						Ó	"		44			96		11	3.0	
Ra	1977	ÐC	3	20	425019	875032	€5	703.5	40.0						2	ė	29	31			94		15	3.3	
84	1977	38	99	20	425018	875041		494.0							ā	15	65	20			89		2	313	
																		**			97		•		

Noist. Liquid Plastic. UC coat.(1) Limit index (1sf) 5, ≆ Bulk Bry Percent Unit Ht. P200 (pcfl ENSINEERING PROPERTIES Unified Soil Class. + sand silt clay Fld K Meth + Bulk I (2.0 to (0.0425 to (ce/s) code + 72.0ms 0.0425ms) (0.002ms) + GRAINSIZE PERCENTAGES Keth Code + CONDUCTIVITY *** HYDRAUL 1C Lab X (ca/s) Sasple Sasple + top bottos + L (ft) (ft) + (696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 696.0 Brng. 875041 875041 875041 875041 875041 875041 875041 875024 875024 875025 875035 875035 875035 875035 875035 875035 875035 875043 875043 875043 875043 875043 875043 875043 875043 875043 875043 875043 875043 875043 (25016 | 125016 | 125016 | 125016 | 125016 | 125016 | 125016 | 125016 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125017 | 125 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) 0.0 (1917) County u (code) Year

Appendix 3 - HYDROSECOLOBIC AND ENGINEERING ONTA FOR RACINE COUNTY - (WEPCO) CALEBONIA SITE

Moist, Liquid Plastic, UC cont.(1) limit index (1sf) 2.3 ¥; 44 2442222 442448 - 1224 222 022020 202200 2024 ٠<u>٠</u> 5.5 12225 经经分别单的现象处 经分价的连续 计引擎引引化论设计算 的变化吸引性的现在分词自然和 + Unified Bult Bry + Suil Percent Unit Ht. + Class, P200 (prf) ENGINEERING PROPERTIES ವರದರಡ್ಡೆ ವರದದವಡದ ನಿಭರರರ ರವಣೆ ನಿರದದ ದನ್ನೆ ದರವದ ಪರರ ನೆ Matrix & Matrix & Matrix & + + sand silt ciay + Bulk I (2.0 to (0.0625 to + 22.0ss 0.0625es) 0.002es) (<0.002es) り はなな 的っぱ 日 故 な なん な GRAINSIZE PERCENTAGES 8 8 3 4 7 2 5 7 7 7 8 8 Reth code Fld K (ca/s) Aporadix 3 - HVDROGEOLOGIC AND ENGINEERING DATA FOR RACINE COUNTY - (NEPCO) CALEDONIA SITE + HYDRAULIC + CONDUCTIVITY (ce/s) Saspie + bottos + L Sample top 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 713.3 688.3 688.3 688.3 688.3 688.3 688.3 688.3 689.4 699.6 699.6 699.6 ##. ##. Brng. E 815099 815099 815099 815099 815099 815099 815099 815099 815050 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 815052 81 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 80027 strat. unit Nat. Site (code)(code) No. Year + County + (code))

Appendix 3 - HYDROSEOLOGIC AND ENGINEERING DATA FOR RACINE COUNTY - (WEPCO) CALEDONIA SITE

+ IDENTI +) Y	14	tho-								HYDRAULII				IZE PERCEN				en bineeri	NG PROPE	RTIES			
•			rat.					Our é	C	e Sample :	CONDUCTION	1114		+		Hatrix I								
· County			it Mat.	Site	,		Bros	Eley.	top			W.41	F3.4 P W.41	+	5308	silt	ctay		Unified		Dry			
•			ode) (code			Long.				fill .	: LOD K	neta	Fid K Meth (cm/s) code	+ Bulk 2	12.0 to	(0.0625 to) **** ***	+	Soil	Percent	Unit Vt.		st. Liquid Plasti	
											. 168/3/		/LE/3/ COGE	72.088	0.0013481	0.00288)	((V.UUZea)	• •	Crass.	P200	(pcf)	(N) cont	.(2) limit index	(tsf)
		30 O	•		425028			?	45.0	47.0				0					ML	90				
		10 0	-			875037			50.0	51.5				i					ML	89		27		2.0
	198			20		875017		-	4.0					2					a	77		27		
	198		-		425014				9.0					•		ν			SH	41		26		
	198 198					875017			9.5	*				٥					α	96		34		
	198		-			875017 875017			14.0					0					CL	97				3.5
			-			875017			19.0		4 635 4			0					α	95				4.5
						875017			24.0 29.0		1.87E-08	•		9					NL	82				3.4
	198					875017			4.0					9					SM	41		12		
Ra			-		425014				9.0										CL.	91		42		4.5
			-		425014				14.0		1.286-08			0					SH	41		28		
Ra	198	_	-	-		875017			19.0		1.100-00								CF	97				4.5
					425014			-	24.0					۸					Œ	98				3.0
Ra	198	30 D			425014				4.0					:					CL	100				4.5
Ra	198	0 0	€ 5		425014				9.0										EL	91		24		
Ra	198	30 Đ	E 3	20	425014	875017			15.0					ň					ML Cl	71 99		17		
Rai	198	0 0	K 3	20	425014				20.0										u U	99 98				4.5
Ra	198	30 B	C 3	20	425014	875017	BC3	5	25.0					ň					a	70 96		22		3.0
Ra	198	10 B	C 5	20	425014	875017	BE3	5	30.0										CL	99		42		2.4
Ra	198	10 D)C 5	20	425014	875017	BE3	5	35.0					٥					. CL	99				3.3 4.5
Ra	198	io e	£C 5	20	425014	875017	BC3	3	45.0		1.97E-08	i		ŏ					SH	33				4.5
	198			20	125014	875017	BC3	\$	50.0	51.5				Ó					GL.	100				4.5
Ra			_	-	125007	875031	BA4	ŀ	4.0	5.5				2					EL	86		20		4.5
Ra	198	-			425007	875031		i	9.0	10.5				2					CL.	82		26		3.5
					4250 07	875031		ł	14.0	16.0				\$					EL	94				4.2
Ra		_	-		125007	875031			19.0	21.0				. 0					CL	96				3.5
		_	-		425007	875031			24.0		1.47E-08	ĵ		0					CL	98				3.6
Ra			-		125007	B75031			29.0					Ō					α	99				3.0
		-	-	-	425007	875031			4.0	5.5				į					CŁ	89		32		3.2
		-			425007	875031			9.0					1					CL	94		43		4.5
	198 198		-		425007	875031			14.0	16.0	8.87E-09	į		į					CL	93				3.5
	198		-		425007 425007	B75031			19.0					0					α	96				4.0
Ra	198				425007 425007	875031 875031			24.0					0					CL	99				2.5
			-		425007 425007	875031			5.0	6.5				0					CL	91		39		4.5
Ra		-		-	425007				10.0										SH	56		30		
	198		-		425007	875031			15.0 20.0					10					MT-CT	76		26		4.5
	198		-		425007	875031			25.0					2					CL	B6		24		3.0
	198		-		425007	875031			30.0					1					CL	95		29		2.8
	198	-	-		425007	0 75031			35.0					ų,					CL	100		24		3.0
Ra	198		-		125007	875031			40.0					0					CL	99		36		3.5
Ř≥	198	0 0	E 3		425007	875031			45.0		1.72E-08	i		^					CL	99		34		3.7
Ra	198	0 0			425007	875031	BC4		50.0		***** V	. =		V A					EL.	99		70		2.5
Ra	198	10 O	E 3			875038			4.0										CL CL	97 85		39 15		4.0
Ra	198	0 0	€ 5	20		875038				10.5				۸					SM	54		15		4.5

Appendix 3 - HYDROSEDEOGIC AND ENGINEERING DATA FOR RACINE COUNTY - IMEPCO) CALEDONIA SITE

IDENTII	TY		ho-								HYDRAULIO CONDUCTION			+ GRAINS +	lle Percen Natrix I		Hatrix I		ENG I NEER!	NG PROPE	RTIES			
+		sti	at.					Surf.	Sample	Sample +				+	sand	silt	clay		Unified	Balk	Dry			
County			t Mat.				Brng.	Elev.	top	bottos +	Lab K	Heth	Fid K Heth	+ Bulk I	12.0 to	(0.0625 ti	D	+	Soil	Percent		SPT Mois	. Liquid Plast	ic. DC
			de) (code		Lat,	Long.	ng.		(ft)	(ft) +	(ca/s)	COSE	(ce/s) code	+ >2.044	0.0625aa)	0.002am)	((0.002ea)	+	Class.	P200	(pcf)	(M) cont.	(1) limit inde	ex (tsf)
		80 O		2		875038				16.0				i					α	93	;			4.5
		30 DI	-	2		87503B				21.0				į					EL	92				2.0
Ra		80 D				875038			24.0		2.34E-01	B į		ŧ					CL	93				2.5
		30 Q1 30 Q1		_		875038 875038			29.0					ŧ					CL.	90				2.2
		30 O				875038			4.0 9.0		6 17F A								EL	88				4.5
Ra						875038			14.0		1.67E-01			9					EL	95				2.0
Ra						875038			19.0										EL	93				2.2
		90 DI				875038			24.0										CL	90				2.0
0.0		10 OI		_		875038				4.0									ČŁ.	91 99				2.0
Ra	198	90 DI	: 5	2		875038								Ň	·				CŁ	28		13		3.5
Ra	198	30 DI	5			875038			10.0	11.5				٥					H2 H2	13		25 29		
R≇	198	80 EN		2		875038			15.0					۸					an CL	100		19		1.5
Ra	198	80 BI	3	2		875038			20.0					ž					દા	92		15		2.0 2.0
Ra	198	80 D	3	2	0 425018	875038	BC5		25.0					ō					a	98		15		2.0
Ra	198	80 DI	3	2	425018	875038	BC5	699,9	30.0					2					EL	97		15		1.0
Ra	195	80 B	: 3	2	0 425018	875038	BC5	699.1	35.0	36.5				ī					EL	91		14		1.0
Ra	198	80 BI	; 3	2	425016	875038	BC5	699.9	40.0	41.5				i					EL	93		21		1.5
Ra	198	80 D	: 5	7	0 425018	875038	BE5	699.9	45.0	47.0	1.76E-0	} !		2					α	85		••		2.2
-		80 QI	-	_		875038		699.9	50.0	51.5				Ţ.					a	92		25		1.5
		80 QI	-			975041		,	4.0	6.0				i					ČL.	BB				4.5
Ra				_		875041			9.0	11.0				2					Cr	90				4.5
	198					875041			14.0		3.98E-0	î		į					CL	94				2.2
Ra						B75041			19.0					ş					CL-NL	90				2.0
	198		-			875041			24.0					į					CŁ	92	:			2.0
	198					875035			1.0					í					CT	91		33		4.5
			-			875035			9.0					į					CL.	89	•	33		4.5
Ra	-					875035			14.0		7.95E-09	ì		2					ÇL	92	:			3.2
Ra Ra						875035			19.0					2					EL	96				4.0
						875035 875023			24.0					į					CL	94				3.5
_		30 · DI				875023			4.0					9					α	58		16		
		30 DI				B75023			9.0					0					ξſ	100		34		4.5
Ra				_					14.0					0					£L.	99				3.0
	198	_				875023			24.0					0					ÇL	99				3.5
R≥				-		875021			4.0					9					CL.	97				4.5
		80 O				875021			9.0					8					CL	86		32		4.5
		30 OI	_			875021			14.0		1.77E-0	,		,					CL.	89		54		4.5
-	198		-			875021			19.0		**************************************	,		3					CL	B9				2.5
Ra						875021			24.0					, , , , , , , , , , , , , , , , , , ,					CL.	90				4.3
Ra	198	80 DI				875022			4.0					2					CL CL	97		71		3.5
Ra	198	10 00				875022			9.0										姐	80		31 39		4.5
Ra	198	80 DI	5	2		875022			14.0		6.58E-0	5							FIL.	76		Φī		3.3
Řa	198	30 DI				875022			19.0		5.42E-08			2					II.	84				4.5
Ra	198	80 (94	3	2		875022			24.0		VI			1					EL.	89		33		2.5
Ra	198	30 01	3	2		875028			4.0					,					EL	88		33 41		4.5

Noist, Liquid Plastic. 1K cont.(2) liait index (tsf) 225233 3.2 2.5 224 4538583 335835382 8 2552538 5 € 222 经设计 HE PERCENTAGES + ENGINEERING PROPERTIES

RATIX I MATIX I + thifted Bulk bry
sand silt clay + thifted Bulk bry
(2.0 to (0.052 to + 50il Percent Unit Mt.
0.0625as) 0.002as) ((0.002as) + Class. P200 (pri) + Bulk X (2.0 to (0.0625 to + 2.0se 0.0625as) 0.002as) ((0.002as) サリサットリアにいいにより おりにたいかんはいいん しけにご にによート じいりし ないだいれいがいいかいにゅうにないかいにはいいないがいにはいいにはいいにないがっている。 GRAINSIZE PERCENTAGES Reth Code Fld K (ca/s) Neth code CONDUCTIVITY (s/es) Sample + bottom + 1 22:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25:00 23:25: Sample top I Sert. \$10.00 pt 10.00 pt 10 Brng. 875028
875028
875028
875028
875028
875028
875028
875029
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030
875030 425010 425014 425014 425018 425018 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 425020 42 Litho-strat. unit Nat. S (code)(code) + County u + (code) Year (

Appendix 3 - HYDSOBERLDGIC AND ENSINEERING DATA FOR RACINE COUNTY - (NEPCO) CALEDONIA SITE

	* · · * * *																
	3. ft																
	Kost, Liqvid Plastic. UC con. (2) libit index (186)	27 :	<u>.</u> •	오	S	12	=										
	Moist. Liquid F cont.(2) limit	8:	z z	23	2	25	25										
	 1.89	0.0	15.0	3.0	0.	٠.	9.0										
į	For the state of t		∴ -		-		_										
1	15. €																
	TES Dry bit Ut. (pcf)																
	MS PROPERTIES Bulk Dry Percent Unit Mt. P200 (pcf)	<u>تة</u> 8	2 2	*	8	\$	Ľ										
	+ ENGINEERING PROPERTIES + Unified Bulk Dr. + Soii Percent Unit + Class. P200 (pc.	ದಃ	ᆲద	ದ	후	ᆸ	ಧ										
	± + + + +																
Ì	M 9	= :	2 5	2	23	25	8										
	Matrix clay ((0.002ma																
1	HBES Matrix X silt (0.0625 to 0.002mm) (35 1	2 23	3	73	22	'n										
	######################################	.	" •		_	•	*										
	+ 68AINSIE PERCENTAGES + 18 :				-		~										
	1 KS 1 7	₩.	4		s	~	~										
	+ + + + + + + + + + + + + + + + + + +																
		,						_			~	~	~	~	~	_	
	Fld K Neth (cm/s) code							- 9K-	1.13E-08	1.655-06	1.946-04	1.885-04	1.01E-06	1.2%-05	2.22E-04	1,576-02	
3116	Feth code																
DAIR TON NACIRE COMMIT - THEYEN'S CALEDONIA SILE	+ HYDRALLIC + CONDUCTIVITY E + n + Lab K Ne + (cm/s) co																
3									_		_		_		_	_	
	Sampl Dotto												80.0				
	Suple Saple + top bottom + (ft) fft] +		5.0 2.0														
TAL CHE	Surf. Elev. (ft)	Ę.	696.5	707	717.5	717.5	705.7	701.1	701.4	733.7	7.4.1	5.683	689	200	669	306.8	
5	Brng.	}	2 2										꾶			¥78	
	Long.	875033	875029 875029	875029	875034	875034	875030	875052	875052	875037	975037	10578	875017	875038	B75 038	875035	
SPENDIX S - NITHINGELLUSIC NAU ENSINCENTAB	Lat.	425010	425014	425020	425025	425025	425030	425018	425018	425028	425028	425014	125011	425016	425016	425012	
2	Site No.	ឧន															
1 P	Kat. code)	м,	3 P	m	m	м	m	ĸ	m	m	М	S	**	M	23	33	
200	Litho- stret. unit Kat. Site (code)(code) No.	88	3 23	음	8	용	유	8	8	용	8	盎	ä	8	8	8	
,	74	86															
nenati	DENTITY Dunty Code) Y		 														
rā.	ಷ ಕರೆ																

SPT Boist. Liquid Plastic. UC + (N) cont.(1) limit index (185) + 5 5 5 おすないひゅせんない ロドロ 井口 けいな : sand silt clay Fld K Meth + Bulk X (2.0 to (0.0625 to (cefs) code + 22.0as 0.0625as) 0.002as) ((0.002as) + GRAINSIZE PERCENTAGES bottos + Lab X Meth
(ft) + (cs/s) code + HYDRAULIC + CONDUCTIVITY 912,9 85.0 792,7 15.0 792,7 15.0 792,7 15.0 792,0 15.0 792,0 15.0 881.8 181.0 881.8 181.0 792,7 15.5 791.1 15.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13.5 791.1 13. 880346 P28
8880340 P29
8880348 P20
880410 P8-AR
880410 P8-AR
880410 P20
880348 P26
880348 P26
880349 P26
880340 P28
880340 P38
880405 P38 Brng. 1 100 M 880340
880340
880340
880340
880340
880353
880353
880353
880353
880353
880353
880353
880353
880353
880353
880353
880353 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 25055 unit Mat. Site (code)(code) No. + County u + (code) Year (

Mapendix J - HYDROBEOLOGIC AND ENGINEERING DATA FOR MILWAUKE COUNTY - NETRO SITE

Moist, Liquid Plastic, UC : cont.(I) limit index (tsf) + 7 2 15.7 2222222 + EMSTACERTING PROPERTIES 8 8 5 **ದವರದದರದರದರದರದದ** ರವರದ ಧರವದ ವದ ಪರಕರದ ಪರವರ ಪರಕರ ದ ದ ವ æ 23 × + SRAINSIZE PERCENTAGES Keth code F16 K (ca/s) 2.09E-06 1.125-07 1.2%-07 1.9%-06 2.0%-06 2.298-07 Sample Sample +
top bottom + Lab K Meth
(ft) (ft) + (cm/s) code + HYDRAUL IC + CONDUCTIVITY 5.105-08 3.605-08 Appendiz 3 - NYDROBEOLOGIC AND ENGINETRING DATA FOR MILKAUKEE COUNTY - NETRO SITE 28.5 28.5 33.5 38.5 103.5 805.0 806.0 806.0 806.0 806.0 806.0 806.0 807.3 807.3 807.3 807.3 807.3 Surt. Elev. (ft) Prng. 890358 1 880358 1 880358 880358 880358 880358 880358 880358 880358 880358 880358 880358 880358 880358 880400 880400 680358 680358 680358 680358 680358 680358 880357 880357 880357 880357 880357 880400 880400 B80400 880400 880400 880400 880400 880400 680400 880358 Long 880357 BB0400 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 625038 62 ij unit Nat. Site r (code)(code) No. + Eounty u + (code) Year (+ IDENTITY

2.0 2.0 2.3 1.5

3.5 3.6 3.6 3.6

4.1 2.5 2.6

27.25.8

2.7

2

3.5 £ 2.8

=

÷ ::

2.5

SPT Moist, Liquid Plastic, UC + (N) coat, (I) limit index (tsf) + \$ 5 23 = 7 16.0 22.0 훒 8 옭 울 Ç Fig K Meth + Bulk I (2.0 to (0.0625 to (ce/s) code + 72.0sm 0.0625m) 0.002mm) ((0.002mm) × # 3 * GRAINSIZE PERCENTAGES 2 3.398-07 Reth Code + HYDRAULIC + CONDUCTIVITY Lab K (ce/s) Sample + bottom + (ft) + 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 993.8 99 £ 5. £ 880348 78498 880348 78498 880348 78498 880348 78498 880348 18498 880348 18498 880348 18498 880348 18498 880348 TM498 880348 TM498 880348 TM498 880348 TM498 Prng. **880348 TM498** 88034g TM49B **BB0348** 1 880348 1 880348 890337 88033 880337 880337 890337 880337 :
 titho trat.
 County onit Nat. Site
 (code) Year (code) Koo. + IDENTITY

16 3.4

2

₽

2.5.5.3

2.0

∞

Apoendix 3 - Hydrogeologic and engineering data for milbainzee county - netro site

SPI Moist, Liquid Plastic, UC + (M) Cont.(1) limit index (tsf) + 2 12 8 19.0 10.0 16.3 **我被告款款款款款款款款** 35.08 17.50 នីង 22 + sand silk clay Fid K Meth + Bulk X (2.0 to (0.0625 to (cm/s) code + >2.0se 0.0625ss) 0.002ss3 ((0.002ss) 3 C ` ; GRAINSIZE PERCENTAGES 1.075-06 Reth Code + CORDUCTIVITY 3.706-08 [ab K (ce/s) Sample + bottom + (ft) + Saple S top b 60.0 63.5 73.5 73.5 83.5 83.5 83.5 811.8 811.8 611.8 611.8 611.8 611.8 611.8 809.4 809.4 809.4 809.4 809.4 809.4 809.4 809.4 809.4 809.4 809.4 809.7 809.7 809.7 Brag. E 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 1853 1 18 425042 880357 425042 880357 425042 880357 425042 880357 425042 880357 425042 880357 425042 880357 425042 880357 425042 880357 425042 880357 425042 880357 425042 880357 425042 880357 425042 880357 425042 880357 425042 880357 880329 880329 880329 880329 880329 880357 B80357 B80357 B80357 425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 (425038 Site Fo unit Mat. S (tode)(code) | + IDENTITY

Apoendix 3 - HYDROGEOLOGIC AND ENGINEBRING DATA FOR MILHAUREE COUNTY - NETRO SITE

SPI Moist. Liquid Plastic. UC (N) coal.(X) limit index (1sf) 2.5.5 2.5 2.7 2.5 2.5 2.5 5 2 = 2 R 33 ないなななない 内特許のなななななに非死なないないないない 2 2 33 7 + Unified Bulk Bry + Soil Percent Unit Mt. + Elass. P200 (pcf) + EMBINEERING PROPERTIES \$ 2 2 ದವರನದಪಡೆದವರದರರದರವರವರದ \mathbf{x}_{i} ದ \mathbf{x} ರ ನ ಕ ದ ದ ರ ವ ದ ವ ದ ವ Natrix & Matrix & Matrix 2 + + sand silt clay + Bulk I (2.0 to (0.0625 to + 22.0se 0.0625ss) 0.002as) ((0.002as) G ∞ 2 ន្ធ ន GRAINSIZE PERCENTAGES -- ×2 Fld K Meth (cs/s) code -bottos + Lab K Meth
(ft) + (cs/s) code + HYDRAUL IC + CONDUCTIVITY Saple for 804.7 63.5 894.7 63.5 894.7 63.5 894.7 63.5 894.7 63.5 894.7 63.5 894.7 63.5 894.7 63.5 894.7 63.5 894.7 83.5 894.7 83.5 894.7 83.5 894.7 83.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 897.2 13.5 Set. Prng. 880337 880337 880337 880337 880337 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 880338 £ong. unit Hat. Site (code)(code) Ho. + County ur

Apornaix 3 - HYDKOBEOLOGIC AND ENGINEERING DATA FOR MILMAUKEE COMMIY - METRO SITE

SPI Maist, Liquid Plastic, UC + (W) cont. (2) Limit index (tsf) + 3.0 1.8 2.0 3.3 3.3 Ξ ĸ ∺ 15.8 19.0 22 # ₹ 8 + Unified Bulk Dry + Soil Percent Unit Mt. + Class. P200 (pcf) 125.88 118.10 + ENGINEERING PROPERTIES 2 53 **ವರವರದವರದರರದ ಪ್ರಪ**ರ್ಕಕ + 6KAINSIZE PERCENTAGES

H Matrix Z Matrix Z H + sand silt ciay Fld K Meth + Bulk X (2.0 to (0.0625 to (ca/s) code + 72.0se 0.0625ss) 0.002ss) ((0.002ss) 器 3 3 × 23 1.00E-07 Sapie Sapie +
top bottos + Lab K Neth
(ft) (ft) + (ce/s) code + HYDRAULIC + CONDUCTIVITY 783.5 783.5 783.5 783.5 783.6 789.6 789.6 789.6 789.6 789.6 789.6 7789.6 7789.6 7789.6 7789.6 7789.6 7789.6 7789.6 7789.6 800.8 800.8 800.8 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800.4 800. Surt. Brng. Elev. Long. no. (ft) 880499 885 880499 885 880499 885 880499 885 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 886 880499 8101 880499 8101 880439 8101 880439 8101 880439 8104 880439 8104 880439 8104 880439 8104 880439 8104 880439 8104 880439 8106 880439 8106 880439 8106 880439 8106 880439 8106 880439 8106 880439 8106 880439 8106 425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
425199 880499
42 + Strat. + County unit Nat. Site + (code) Year (code) Koo. + IDENTITY

Appendix 3 - Hydroseca, dbic and ensineering data for allumanee County - Netro Site

	* + *	# 1		۲.	2.5	្ន	9.		2.0	0.2	2.0	<u>:</u>								
		rtic. L		•		**				. 7	. 7	-	22	œ	2					
		SPI Moist. Liquid Plastic, UC + (%) cont.(1) limit index (15f) +										z	s	82	23					
												•								
		Koist.	19.8	16.2	16.2	19.5	12.1	15.3	15.6	21.3	2.8	17.6								
		£ €																		
	RIES	Unit III. (pcf)																		
	NS PROPE	Percent P200											æ	9	,					
	ENSINEERING PROFERTIES	Soil Class.																		
	+++	+ +																		
	Ratrix	(0.902																		
	IE PERCENTAGES Natrix I Matrix I Matrix I Fand Silt Fand	Fig K Neth + Bulk I (2.0 to (0.0525 to + Soil Percet Unit Ht. (cars) code + 72.0ms 0.052ms) (.0.02ms) + Class. P200 (pcf)																		
	+ GRAINSIZE PERCENTAGES F Natrix I Matr	2.0 to fi 0625as)																		
	GRAINSI ZE	Bulk X (
	* + *															7	~	~	~	
		* (š														\$	ş	Ş	ş	
																3.4.	¥.9	¥.	1.01E-06	
	IE VITY	Reth Code														99	-			
SITE	+ HYDRAUL IC + CONDUCTIVITY	bottos + Lab K (#t! + (cs/s)														. SS. ₹	2.406-08			
E E	+ + +																æ.	46.4	30.0	
UKTY	3	top botton	_	۰		٥	٠	٥	•	۰	۰		۰	۰	٥					
	å	₹									98.0		4	9	Š,	o;	zi.	85	8	
DATA FOR MILWADKEE COUNTY - METRO SITE	, i	Brag. Elev. no. (ff.)	,		822.7							122.7								
¥ 86		Breg.	910	B308	838	910 8	8108	3	808	89	8	80	108	88	8	1808	8 56	268	P1081	
		Long	880337	880346	880346	880346	880346	880346	980346	880346	880346 \$108	880346	880346	880346	880346	880346	880346	880346	880346	
EXE		i i	425049	425112	425112	425112	125112	425112	12312	425112	22112	425112	425112	425112	425112	425112	425112	425112	425117	
2		Site No.	22	7	77	77	≂	≂	≈	≂	7	≂	7	≂	~	z	≂	7	≈	
ECK 06		Kat. (code)	\$	m	m	m	m	~	-	m	•	\$	m	m	m	m	n	*>	-	
HADSON	itho-	nit rode)	8	용	8	용	쓤	8	ឌ	ខ	8	8	జ	윰	ខ	쓤	굨	용	ន	
	·	Year	1 7 85																	
kosendix 3 - HYDXIGEIK.OBIC AND ENGINEERINS	DENTITY	County anit Mat. Site (rode) Year (rode)(code) No.	Œ	댶	Œ	Ŧ	¥	포	₽	궆	꺌	¥	Œ	Ħ	Ŧ	Z	≘	Z	쓮	

+ County with Net. Site	+ HYDRAUE IC		8	GRAINSIZE PERDENTAGES	ENTAGES		+ EMBINEER	+ ENGINEERING PROPERTIES	IES				
Strict. Strait Shape Strict. Stri	+ CONDUCTIVITY		+	Matri	Natrix I Matrix I	I Matrix I	+						
Hear (code) (code) Mo. Lat. Long. no. (ft) (ft) (ft) + 1918 1983 KE 5 22 445151 880728 B1 704.2 55.00 24.50 1983 KE 5 22 445151 880728 B1 704.2 55.00 24.50 1983 KE 5 22 445141 880723 B1 704.2 55.00 24.50 1983 KE 5 22 445141 880723 B2 688.9 35.00 77.00 1983 KE 1 2 44514 880723 B2 688.9 35.00 77.00 1983 KE 1 2 44514 880723 B2 688.9 35.00 77.00 1985 KE 1 3 2 44514 880725 B3 724.1 65.00 47.00 1985 KE 1 3 2 44514 880725 B3 724.1 65.00 47.00 1985 KE 1 3 2 44514 880725 B3 725.1 15.00 14.00 1985 KE 1 2 44514 880725 B4 724.5 0.00 1985 KE 1 2 44514 88072 B4 724.4 55.00 52.00 1985 KE 2 2 44514 88072 B4 724.4 55.00 52.00 1985 KE 2 2 44514 88072 B4 724.5 5.00 52.00 1985 KE 3 2 44514 88072 B4 724.5 5.00 52.00 1985 KE 4 2 44514 88072 B4 724.5 5.00 52.00 1985 KE 5 2 44515 88073 B5 702.4 55.00 52.00 1985 KE 5 2 44515 88073 B9 702.4 55.00 52.00 1985 KE 5 2 44515 88072 B9 702.4 52.00 12.50 1985 KE 5 2 44515 88072 B9 702.4 52.00 12.50 1985 KE 5 2 44518 88072 B9 702.4 52.00 12.50 1985 KE 5 2 44518 88072 B9 702.4 52.00 12.50 1985 KE 5 2 44518 88072 B9 702.4 52.00 12.50 1985 KE 5 2 44518 88072 B9 702.4 52.00 12.50 1985 KE 5 2 44518 88072 B9 702.4 52.00 12.50 1985 KE 5 2 44518 88072 B9 702.4 52.00 12.50 1985 KE 5 2 44518 88072 B9 702.4 52.00 12.50 1985 KE 5 2 44518 88072 B9 702.4 52.00 12.50 1985 KE 5 2 44518 88072 B9 702.4 52.00 12.50 1985 KE 5 2 44518 88072 B9 702.4 52.00 12.50 1985 KE 5 2 44518 88072 B9 702.4 52.00 12.50 1985 KE 5 2 44518 88072 B9 702.4 52.00 12.50 1985 KE 4 2 44518 88072 B9 702.4 52.00 12.50 1985 KE 4 2 44518 88072 B9 702.4 52.00 12.50 1985 KE 4 2 44518 88072 B9 702.4 52.00 12.50 1985 KE 7 2 44518 88072 B9 702.4 52.00 12.50 1985 KE 7 2 44518 88072 B9 702.4 52.00 12.50 1985 KE 7 2 44518 88072 B9 702.4 52.00 12.50 1985 KE 7 2 44518 88072 B9 702.4 52.00 12.50 1985 KE 7 2 44518 88072 B9 702.4 52.00 12.50 1985 KE 7 2 44518 88072 B9 702.4 52.00 12.50 1985 KE 7 2 44518 88072 B9 702.4 52.00 12.50 100.00 11.00 100.00 11.00 100.00 11.00 100.00 12.50 100.00 12.50 100.00 12.50 100.00 12.50 100.00 12.50 100.00 12.50 100.00 12			+			clay	+ Unified		ž				
Control No. Lat. Long. Inc. (ft)	bottos +	Fld K Keth		+ Bulk 1 (2.0 to	o 10,0625 to	\$	+ Soi J	Percent Unit Ht.		SPT Moist.		Liquid Plastic. UC	
1983 KE 5 22 445151 880928 BI 704,2 25.00 26.50 1985 KE 5 22 445151 880928 BI 704,2 25.00 4.59 1985 KE 5 22 445141 880923 BI 804,2 25.00 4.59 1985 KE 5 22 445141 880923 BI 804,2 25.00 5.50 6.59 1985 KE 5 22 44514 880923 BI 706,1 20,0 21,0 1985 KE 1 22 44514 880925 BI 706,1 20,0 21,0 1985 KE 1 2 44514 880925 BI 706,1 30,0 17.00 1985 KE 1 2 44514 880925 BI 706,1 30,0 17.00 1985 KE 1 2 44514 880925 BI 706,1 30,0 17.00 1985 KE 1 2 44514 880925 BI 706,1 30,0 17.00 1985 KE 1 2 44514 880925 BI 706,1 30,0 17.00 1985 KE 1 2 44514 880925 BI 706,1 40,0 41,10 1985 KE 1 2 44514 880925 BI 706,1 40,0 41,10 1985 KE 2 44514 880925 BI 706,1 40,0 41,10 1985 KE 2 44514 880925 BI 706,1 40,0 41,10 1985 KE 2 44514 880925 BI 706,1 40,0 41,10 1985 KE 3 2 44514 880925 BI 706,1 40,0 41,10 1985 KE 4 2 44514 880925 BI 706,1 40,0 41,10 1985 KE 5 2 44518 880925 BI 706,1 40,0 41,10 1985 KE 5 2 44518 880925 BI 706,1 40,0 41,50 1985 KE 5 2 44518 880925 BI 706,1 40,0 41,50 1985 KE 5 2 44518 880925 BI 706,1 40,0 41,50 1985 KE 5 2 44518 880925 BI 706,1 45,0 16,0 11,0 1985 KE 5 2 44518 880925 BI 706,1 45,0 16,0 11,0 1985 KE 5 2 44518 880925 BI 706,1 45,0 16,0 11,0 11,0 1985 KE 5 2 44518 880927 BI 706,1 70,0 11,0 11,0 1985 KE 5 2 44518 880927 BI 706,1 70,0 11,0 11,0 1985 KE 5 2 44518 880927 BI 706,1 70,0 11,0 11,0 1985 KE 5 2 44518 880927 BI 706,1 70,0 11,0 11,0 1985 KE 5 2 44518 880927 BI 706,1 70,0 11,0 11,0 11,0 1985 KE 5 2 44518 880927 BI 706,1 70,0 11,0 11,0 11,0 11,0 11,0 11,0 11	÷ (35)	(ca/s) code		+ >2.0sa 0.0625as}		0.002mm (<0.002mm)	+ Class.	P200	(\$24)	(N) cont. (X) limit		index ((Lsf)
1983 K. 5 22 445151 880728 81 706.2 73.40 27.40 1985 K. 5 22 445151 880728 814 706.2 73.40 27.40 1985 K. 5 22 445141 880723 82 489.9 73.00 21.50 1985 K. 5 22 445141 880723 82 489.9 73.00 21.50 1985 K. 5 22 445141 880723 83 76.11 30.00 21.50 1985 K. 1 2 445141 880725 83 726.1 30.00 21.50 1985 K. 1 2 445141 880725 83 726.1 30.00 21.50 1985 K. 1 2 445141 880725 83 726.1 30.00 21.50 1985 K. 1 2 445141 880725 83 725.1 15.50 19.50 1985 K. 1 2 445141 880725 83 725.1 15.50 19.50 1985 K. 1 2 445141 880725 83 725.1 15.50 19.50 1985 K. 1 2 445141 880725 83 725.1 15.50 19.50 1985 K. 2 445141 880725 84 72.4 25.00 21.50 1985 K. 2 44514 880732 84 72.4 25.00 21.50 1985 K. 2 44514 880732 84 72.4 25.00 21.50 1985 K. 2 44514 880732 84 72.4 25.00 21.50 1985 K. 3 2 44514 880732 85 72.4 25.00 21.50 1985 K. 4 2 44514 880732 84 72.4 25.00 21.50 1985 K. 4 2 44514 880732 84 72.4 25.00 21.50 1985 K. 4 2 44514 880732 84 72.4 25.00 21.50 1985 K. 5 2 44515 880723 89 70.4 25.00 21.50 1985 K. 5 2 44515 880723 89 70.4 25.00 21.50 1985 K. 5 2 44515 880723 89 70.4 25.00 21.50 1985 K. 5 2 44518 880723 89 70.4 25.00 21.50 1985 K. 5 2 44518 880723 89 70.4 25.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.0	į			0.00	5.00 92.00	3.00		8		25			•
1985 KE 5 22 445151 880972 B1 706.2 5.00 6.50 1983 KE 5 22 44514 880972 B2 6869 75.00 77.00 1983 KE 5 22 44514 880972 B2 6869 75.00 77.00 1983 KE 5 22 44514 880972 B3 726.1 75.00 77.00 1983 KE 5 22 44514 880972 B3 726.1 15.00 47.00 1983 KE 5 22 44514 880972 B3 725.1 15.00 47.00 1983 KE 4 22 44514 880972 B3 755.1 15.00 47.00 1983 KE 4 22 44514 880972 B4 755.0 40.00 1983 KE 5 22 44514 880972 B4 755.0 40.00 1983 KE 5 22 44514 880973 B4 755.0 40.00 1983 KE 7 2 44514 880973 B4 755.0 60.00 1983 KE 7 2 44514 880973 B4 752.4 50.00 1983 KE 7 2 44514 880973 B5 742.4 55.00 1983 KE 7 2 44514 880973 B9 742.4 55.00 1983 KE 7 2 44514 880973 B9 742.4 55.00 1983 KE 7 2 44514 880973 B9 746.1 55.00 1984 KE 9 22 44515 880973 B9 746.1 55.00 1985 KE 5 22 44515 880973 B9 740.1 55.00 1985 KE 5 22 44516 880973 B9 700.4 65.00 1985 KE 5 22 44516 880973 B9 700.4 65.00 1985 KE 5 22 44518 880973 B9 700.4 65.00 1985 KE 5 22 44518 880973 B9 700.4 65.00 1985 KE 5 22 44518 880972 B9 700.4 65.00 1985 KE 5 22 44518 880972 B9 700.4 65.00 1985 KE 5 22 44518 880972 B9 700.4 65.00 1985 KE 5 22 44518 880972 B9 700.7 65.00 1985 KE 7 22 44514 880972 B9 700.7 65.00 1985 KE 7 2 44514 880972 B9 700.7 65.00 1985 KE 7 2 44514 880972 B9 700.7 65.00 1985 KE 7 2 44514 880972 B9 700.7 65.00 1985 KE 7 2 44514 880972 B9 700.7 65.00 1985 KE 7 2 44514 880972 B9 700.7 65.00 1985 KE 7 2 44514 880972 B9 700.7 65.00 1000 700 700 700.7 700.7 1000 700 700	-	1.005-05	_				2			; -			
1983 KE 5 22 445147 880973 B2 688.9 35.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00		1		60						٥			
1983 KE 4 22 44514 889273 R2 48519 Z2.00 21.50 1983 KE 4 22 44514 889273 R3 785.1 S.50 21.00 1983 KE 1 3 22 44514 889275 R3 725.1 S.50 21.50 1985 KEN 3 22 44514 889275 R3 725.1 S.50 19.50 1985 KEN 3 22 44514 889272 R3 725.1 S.50 19.50 1985 KE 4 22 44514 889272 R3 725.1 S.50 19.50 1983 KE 5 22 44514 889273 R3 725.1 S.50 19.50 1983 KE 5 22 44514 889732 R4 734.4 S.50 0.00 1983 KE 5 22 44514 889732 R4 734.4 S.50 0.00 1983 KE 5 22 44514 889732 R4 734.4 S.50 0.00 1983 KE 5 22 44514 889732 R3 725.1 S.50 19.50 1983 KE 7 2 44514 889732 R3 725.1 S.50 15.50 1983 KE 7 2 44518 889732 R3 725.4 S.50 0.00 1983 KE 7 2 44518 88973 R3 725.4 S.50 0.00 1985 KE 7 2 44518 88973 R3 725.4 S.50 0.00 1985 KE 7 2 44518 88973 R3 725.4 S.50 0.00 1985 KE 7 2 44518 88973 R3 725.4 S.50 0.00 1985 KE 7 2 44518 88973 R3 725.4 S.50 0.00 1985 KE 7 2 44518 88973 R3 725.4 S.50 0.00 1985 KE 7 2 44518 88973 R3 725.7 S.00 1.50 1985 KE 7 2 44518 88973 R3 725.7 S.00 1.50 1985 KE 7 2 44518 88973 R3 700.4 S.50 0.00 1985 KE 7 2 44518 88973 R3 700.4 S.50 0.00 1985 KE 7 2 44518 88973 R3 700.4 S.50 0.00 1985 KE 7 2 44518 88973 R3 700.4 S.50 0.00 1985 KE 7 2 44518 88973 R3 700.4 S.50 0.00 1985 KE 7 2 44518 88973 R3 700.4 S.50 0.00 1985 KE 7 2 44518 88973 R3 700.4 S.50 0.00 1985 KE 7 2 44518 88973 R3 700.4 S.50 0.00 1985 KE 7 2 44518 88973 R3 700.4 S.50 0.00 1985 KE 7 2 44518 88973 R3 700.4 S.50 0.00 1985 KE 7 2 44518 88973 R3 700.4 S.50 0.00 1985 KE 7 2 44518 88973 R3 700.4 S.50 0.00 1985 KE 7 2 44518 88973 R3 700.4 S.50 0.00 1985 KE 7 2 44518 88973 R3 700.4 S.50 0.00 1985 KE 7 2 44518 88973 R3 700.4 S.50 0.00 1985 KE 9 2 44518 88973 R3 700.4 S.50 0.00 1985 KE 9 2 44518 88973 R3 700.4 S.50 0.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10	-		_	8			8 2	5 2					
1983 KE 1 22 44514 88975 RA 275.1 15.0 21.00 21.00 1895 KE 1 22 44514 88975 RA 275.1 15.0 17.0 22.00 11.90 1995 KE 1 2 24514 88975 RA 275.1 15.0 17.0 17.0 1895 KE 1 3 22 44514 88975 RA 275.1 15.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17		5 AAC-04		3			5 5			2,0			
1983 KEI 3 22 445142 880755 B1 778.1 20.00 22.00 1985 KEI 3 22 445142 880755 B1 778.1 20.00 22.00 1985 KEI 3 22 445142 880755 B1 778.1 55.0 47.00 47.00 1985 KE 4 22 445142 880752 B1 725.1 115.00 41.50 1985 KE 4 22 44514 880752 B1 735.0 40.00 41.50 1985 KE 4 22 44514 880752 B4 735.0 40.00 41.50 1985 KE 4 22 44514 880752 B4 735.0 40.00 41.50 1983 KE 5 22 44518 880753 B5 722.4 55.0 26.00 1983 KE 5 22 44518 880753 B5 722.4 55.0 26.00 1985 KE 5 22 44518 880753 B5 722.5 30.0 0.00 1985 KE 5 22 44518 880753 B9 748.1 15.00 16.50 1985 KE 5 22 44518 880752 B9 700.4 65.00 12.50 1985 KE 5 22 44518 880752 B9 700.4 65.00 16.50 1985 KE 5 22 44518 880752 B9 700.4 65.00 16.50 1985 KE 5 22 44518 880752 B9 700.4 65.00 16.50 1985 KE 5 22 44518 880752 B9 700.4 65.00 16.50 1985 KE 5 22 44518 880752 B9 700.4 65.00 16.50 1985 KE 5 22 44518 880752 B9 700.4 65.00 16.50 1985 KE 5 22 44518 880752 B9 700.4 65.00 16.50 1985 KE 5 22 44518 880752 B9 700.4 65.00 16.50 1985 KE 5 22 44518 880752 B9 700.4 65.00 16.50 1985 KE 5 22 44518 880752 B1 691.7 35.00 16.50 1985 KE 5 22 44518 880752 B1 691.7 35.00 16.50 1985 KE 5 22 44518 880752 B1 691.7 35.00 16.50 1985 KE 5 22 44518 880752 B1 691.7 35.00 16.50 1985 KE 5 22 44518 880752 B1 691.7 35.00 16.50 1985 KE 5 22 44518 880752 B1 691.7 35.00 16.50 16.50 1985 KE 5 22 44518 880752 B1 691.7 35.00 16.50 1985 KE 5 22 44518 880752 B1 691.7 35.00 16.50 16.50 1985 KE 5 22 44518 880752 B1 691.7 35.00 16.50 16.50 1985 KE 5 22 44518 880752 B1 691.7 35.00 16.50 16.50 1985 KE 5 22 44518 880752 B1 691.7 35.00 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50 16.50		5								31			
1985 KEI 5 22 445142 880975 B3 775.1 15.50 47.00 47.00 1985 KEI 3 22 445142 880975 B3 775.1 15.50 19.50 19.50 1985 KEI 3 22 445142 880975 B3 775.1 15.50 19.50 19.50 1985 KE 4 22 44514 880972 B4 734.9 42.80 42.10 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.50 19.5			•	20 20						2	72		4
1985 KERI 3 22 445147 880975 83 755.1 15.50 14.50 1985 KERI 3 22 445147 880975 84 755.1 15.50 14.50 1985 KE 4 22 445147 880972 84 755.1 15.50 14.50 1985 KE 4 22 445147 880972 84 73.4.4.20 04.10 1983 KE 5 22 445154 880973 84 72.50 55.00 1983 KE 5 22 445154 880973 85 74.2.4 35.00 25.00 1983 KE 4 22 445154 880973 86 72.2.50 25.00 1983 KE 4 22 445154 880973 86 72.2.50 25.00 1983 KE 4 22 445154 880973 86 72.2.45 72.00 25.00 1983 KE			-		3.00 67.00	31.00	ಕ ಪ	8		•		9	•
1985 KEN 3 22 445142 880925 B3 725.1 17.00 14.00 14.50 1985 KE 4 22 445147 880922 B49 735.4 17.00 14.00 14.50 1985 KE 4 22 44514 880922 B49 735.4 2.00 41.50 1985 KE 5 22 44514 880925 B49 734.5 4.50 57.00 1983 KE 5 22 44515 880925 B5 712.4 55.00 57.00 1983 KE 5 22 44515 880925 B5 712.4 55.00 57.00 1985 KE 4 22 44515 880925 B5 712.4 55.00 25.00 1985 KE 4 22 44515 880928 B9 742.4 55.00 55.00 1985 KE 5 22 44515 880928 B9 742.4 55.00 6.50 1985 KE 5 22 44515 880928 B9 742.4 55.00 6.50 1985 KE 5 22 44515 880925 B9 700.4 55.00 6.50 1985 KE 5 22 44516 880925 B9 700.4 55.00 6.50 1985 KE 5 22 44518 880925 B9 700.4 55.00 6.50 1985 KE 5 22 44518 880925 B9 700.4 55.00 6.50 1985 KE 5 22 44518 880929 B10 15.00 15.00 15.00 1985 KE 5 22 44518 880929 B10 15.00 15.00 15.00 1985 KE 5 22 44518 880929 B10 15.00 15.00 15.00 1985 KE 5 22 44518 880929 B10 15.00 15.00 15.00 1985 KE 5 22 44518 880929 B10 15.00 15.00 15.00 1985 KE 5 22 44518 880929 B10 15.00 15.00 15.00 1985 KE 5 22 44518 880929 B10 15.00 15.00 15.00 1985 KE 5 22 44518 880929 B10 15.00 15.00 15.00 1985 KE 5 22 44518 880929 B10 15.00 10.00 11.00 1985 KE 4 22 44518 880929 B12 690.3 40.00 1985 KE 4 22 44518 880929 B12 690.3 40.00 1985 KE 4 22 44518 880929 B12 690.3 40.00 1985 KE 5 22 44518 880929 B12 690.3 40.00 1985 KE 5 22 44518 880929 B12 690.3 40.00 1985 KE 7 2 44518 880929 B12 690.3 40.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00	9.50	3.005-03	,										
1983 KE 4 22 44314 880972 B4 735,0 40,00 41,50 1985 KE 4 22 44314 880972 B4 735,0 40,00 41,50 1983 KE 4 22 44314 880972 B4 735,0 40,00 41,50 1983 KE 5 22 44318 880973 B5 724,5 5,0 25,0 10 1983 KE 5 22 44318 880973 B5 724,5 5,0 25,0 1983 KE 4 22 44318 880973 B5 724,5 5,0 25,0 1983 KE 4 22 44318 880973 B9 748,1 55,0 15,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18,50 18			-	9.00 38	38.00 38.00	23.00	T T	13			5.6.0	2	
1985 KE 4 22 445147 889972 849 734;9 47.80 49.10 1985 KE 4 22 445148 889972 B4 734;9 47.80 80.00 1983 KE 5 2 445154 889735 B5 742,4 55.00 55.00 1983 KE 5 2 445154 889735 B5 742,4 55.00 55.00 1983 KE 4 22 445154 889734 B6 872,4 37.00 45.50 1983 KE 4 22 445154 889734 B6 872,4 37.00 45.50 1983 KE 4 22 445154 889737 B7 74.30 46.50 1983 KE 4 22 445154 889737 B7 14.30 46.50 1983 KE 4 22 445154 889737 B7 14.30 14	41.S		'				23			#		i	
1985 KE 4 22 44514 880532 BIC 734,6 73,50 60.00 1983 KE 5 22 445154 880552 BIC 734,6 75,50 60.00 1983 KE 5 22 445154 880552 BS 742,4 25,00 25,00 1983 KE 4 22 445154 880525 BS 742,4 55,00 25,50 1983 KE 4 22 445154 880524 BL 672,6 72,00 21,50 1985 KE 4 22 445154 880528 BT 748,1 15,00 60,00 1985 KE 5 22 445154 880528 BT 748,1 15,00 60,00 1985 KE 5 22 445152 880525 BF 700,4 75,00 65,50 1985 KE 5 24 445154 880525 BF 700,4 75,00 75,50 1985 KE 5 24 445154 880525 BF 700,4 75,00 75,50 1985 KE 5 22 445154 880527 BF 700,4 75,00 41,50 1985 KE 5 22 445154 880527 BF 700,4 75,00 41,50 1985 KE 5 22 445154 880527 BF 700,4 75,00 41,50 1985 KE 5 22 445154 880527 BF 70,0,4 75,00 41,50 1985 KE 5 22 445154 880527 BF 70,0,4 75,00 41,50 1985 KE 5 22 445154 880527 BF 70,0,4 75,00 41,50 1985 KE 4 22 44514 880527 BF 70,0,4 75,00 41,50 1985 KE 4 22 44514 880527 BF 70,0,4 75,00 41,50 1985 KE 4 22 44514 880527 BF 70,0,4 75,00 41,50 1985 KE 4 22 44514 880527 BF 70,0,4 75,00 41,50 1985 KE 4 22 44514 880527 BF 70,0,7 75,0 75,0,0 1985 KE 5 22 24514 880527 BF 70,0,7 75,0 75,0,0 1985 KE 5 22 24514 880527 BF 70,0,7 75,0 75,0,0 1985 KE 5 22 24514 880527 BF 70,0,7 75,0 75,0,0 1985 KE 5 22 24514 880527 BF 70,0,7 75,0 75,0,0 1985 KE 5 22 24514 880527 BF 70,0,7 75,0 75,0,0 1985 KE 5 22 24514 880527 BF 70,0,7 75,0 75,0 1985 KE 5 22 24514 880527 BF 70,0,7 75,0 75,0 1985 KE 75 75 75 75 75,0 1985 KE 75 75 75 75 75 75 75 7		1.405-03	-				27			;			
1983 K. 5 22 445154 880755 B5 712,4 55,00 57,00 1983 K. 5 22 445154 880755 B5 712,4 55,00 52,00 1983 K. 5 22 445154 880757 B5 712,4 75,00 12,50 1983 K. 4 22 44515 880757 B6 632,6 34,00 1983 K. 4 22 44515 880727 B1 718,1 15,00 1983 K. 5 22 44515 880727 B1 718,1 15,00 1983 K. 5 22 44515 880727 B1 718,1 15,00 1983 K. 5 22 44515 880727 B1 700,4 25,00 1985 K. 5 22 44516 880727 B1 700,4 55,00 1985 K. 5 22 44516 880727 B10 15,00 15,00 1985 K. 5 22 44516 880727 1985 K. 5 22 44516 10,00 11,00 10,00 11,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 10,00 12,00 1		1.605-03	_				24						
1983 KE 3 2 445154 860953 BSA 742.4 25.00 26.00 1983 KE 4 22 445151 860973 BSA 742.4 53.00 35.50 1983 KE 4 22 445151 860978 B) 742.5 43.00 46.00 1983 KE 4 22 445154 860978 B) 748.1 15.00 16.50 1985 KE 4 22 445149 860972 B) 748.1 15.00 16.50 1983 KE 5 22 445152 860972 B) 700.4 65.00 65.50 1983 KE 5 22 445152 860972 B) 700.4 65.00 65.50 1983 KE 5 22 445162 860972 B) 700.4 65.00 65.50 1985 KE 5 22 445148 860972 B) 10.00 11.00 1985 KE 5								8					
1983 K 5 22 445154 880935 BSA 742.4 35.00 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50 35.50				2.00 19	19.00 45.00	25.82	ರ			83	23.0	19.0	
1983 KE 4 22 445151 889924 B6 672.4 70.0 21.50 21.50 1983 KE 4 22 445154 889924 B6 672.4 70.0 46.00 1983 KE 3 22 445154 889928 B7 748.1 15.00 16.50 1985 KE 3 22 445154 889928 B7 748.1 15.00 16.50 1985 KE 3 2 445152 889928 B9 700.4 15.00 16.50 1983 KE 9 2 445152 889928 B9 700.4 15.90 19.90 1985 KE 4 2 445182 889929 B9 5.00 45.50 1985 KE 5 2 445182 889929 B9 10.00 11.00 1985 KE 5 2 445148 889929 B9 10.00 41.50 11.00 1985 K										×			
1983 KE 4 245151 889924 Bb 69226 34,00 40.00 1983 KE 4 22 445154 889938 B) 748,115.00 18.50 1985 KE 4 22 445194 889721 BS 690.137,30 44.30 1983 KE 5 22 445192 889725 BS 700.4 55.00 26.50 1985 KE 5 22 445182 889725 BS 700.4 55.00 46.50 1985 KE 5 22 44518 889729 BIO 5.00 45.50 1985 KE 5 22 44518 889729 BIO 5.00 45.50 1985 KE 5 22 44518 889729 BIO 15.00 11.00 1985 KE 5 22 44518 889724 BII 691.7 35.00 45.00 1985				9.0						£			
1983 KE 4 22 445154 880938 B7 748.1 15.00 16.50 16.50 1983 KE 3 22 445154 880938 B7 748.1 25.00 26.50 1983 KE 5 22 445154 880925 B7 748.1 25.00 26.50 1983 KE 5 22 445154 880925 B7 700.4 55.00 26.50 1983 KE 99 22 445152 880925 B9 700.4 55.00 26.50 1983 KE 99 22 445152 880925 B9 700.4 55.00 26.50 1985 KE 5 22 445148 880929 B10 10.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.		9.50E-02	г.										
1982 K 3 245154 880938 B7 748.1 25.0 26.50 1985 K 4 22 445124 880928 B7 74.30 44.30 1983 K 99 22 445122 880925 B9 700.4 65.00 25.5 1983 K 99 22 44512 880925 B9 700.4 65.00 26.55 1983 K 99 22 44518 880929 B10 15.00 14.50 18.50 1985 K 5 22 44518 880929 B10 15.00 11.50 16.50 1985 K 5 22 44518 880929 B10 15.00 14.50 16.50 1985 K 5 22 44518 880929 B11 641.7 3.00 41.50 1985 K 5 22 44518 880929 B11 641.7 3.50 <td></td> <td></td> <td>4</td> <td>90.00</td> <td></td> <td></td> <td>24 24</td> <td></td> <td></td> <td>*</td> <td></td> <td></td> <td></td>			4	90.00			24 24			*			
1985 KE 4 22 445149 889924 88 689.1 37.30 44.30 1983 KE 5 22 445152 889925 B9 700.4 45.00 26.59 1983 KE 99 22 445152 889925 B9 700.4 45.00 26.59 1983 KE 99 22 445152 889925 B9 700.4 45.00 6.53 1985 KE 9 22 445182 889929 B10 5.00 6.59 1985 KE 5 22 445148 889929 B10 15.00 11.00 11.00 11.90 KE 5 22 445148 889929 B10 15.00 15.00 15.50 1985 KE 5 22 445150 889924 B11 641.7 40.00 41.59 1985 KE 4 22 445148 889929 B12 640.3 40.00 41.59 1985 KE 4 22 445148 889929 B12 640.3 40.00 41.59 1985 KE 4 22 445148 889920 B12 690.3 31.10 38.10 1985 KE 4 22 445148 889920 B12 690.3 31.10 38.10 1980 B1 20.5 40.3 40.00 41.50 1985 KE 4 22 445148 889920 B12 690.3 31.10 38.10 1980 B1 20.5 40.5 40.5 40.5 40.5 40.5 40.5 40.5 4					32.00 51.00	17.00		69		83	27.0	15.0	
1983 KE 5 22 445152 880925 B9 700.4.25.00 26.50 1983 KE 99 22 445152 880925 B9 700.4.45.00 66.50 1983 KE 99 22 445152 880925 B9 700.4.75.00 74.50 1983 KE 1 22 445148 880929 B10 10.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.		2.90E-04	_				¥3-83	_					
1983 Kf 99 22 445182 889525 89 700.4 65.00 66.50 1983 Kf 99 22 445182 889525 89 700.4 65.00 65.50 1985 Kf 5 22 445182 889529 810 5.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15				0.00				≅.				-	ď
1983 K 99 22 445152 880725 89 700.4 73.40 79.50 1985 K 4 22 44518 880729 810 5.00 6.50 1985 K 5 22 44518 880929 810 15.00 16.50 1985 K 5 22 44518 880924 811 681.7 35.9 40.00 1995 K 4 22 445148 880924 811 681.7 35.9 40.00 1985 K 4 22 445148 880924 812 69.3 40.00 41.50 1985 K 4 22 445148 880924 812 69.0 3 1.10 30.10 1985 K 4 22 445148 880924 812 69.0 3 1.10 30.10 1985 K 4 22 445148 880924 817 50.0 3 1.10 30.00					9.35	00 40.00		%		25	2	16.1	2
1985 KF 4 22 445148 890729 B10 5.00 6.50 1985 KF 5 22 445148 890729 B10 10.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50 11.50		6. BOE -04	Ŀ				¥.0					•	0
1985 KE 3 22 445148 869279 810 10.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00			_		8		ds-25	-9		83			
1985 KE \$ 22 445148 880929 B10 15.00 16.50 16.50 1985 KE \$ 22 445148 880924 B11 691.7 35.50 40.00 1985 KE \$ 22 445150 880924 B11 691.7 35.50 40.00 1985 KE \$ 12 445148 880924 B12 690.3 40.00 11.50 1985 KE \$ 1 22 445148 880924 B12 690.3 31.10 39.10 1985 KE \$ 1 22 445148 880920 B12 590.3 31.10 38.10 19.10 1985 KE \$ 22 445148 880950 B12 745.2 25.50 30.00 1985 KE \$ 22 445148 880950 B12 745.2 25.50 30.00 1985 KE \$ 32 445148 880950 B12 745.2 25.50 30.00 1985 KE \$ 32 445148 880950 B12 745.2 25.50 30.00 1985 KE \$ 32 445148 880950 B12 745.2 25.50 30.00 1985 KE \$ 32 445148 880950 B12 745.2 25.50 30.00 1985 KE \$ 32 445148 880950 B12 745.2 25.50 30.00 1985 KE \$ 32 445148 880950 B12 745.2 25.50 30.00 1985 KE \$ 32 445148 880950 B12 745.2 25.50 30.00 1985 KE \$ 32 445148 880950 B12 745.2 20.00 1985 KE \$ 32 445148 880950 B12 745.2 20.00 1985 KE \$ 32 445148 880950 B12 745.2 20.00 1985 KE \$ 32 445148 880950 B12 745.2 20.00 1985 KE \$ 32 445148 880950 B12 745.2 20.00 1985 KE \$ 32 445148 880950 B12 745.2 20.00 1985 KE \$ 32 445148 880950 B12 745.2 20.00 1985 KE \$ 32 445148 880950 B12 745.2 20.00 1985 KE \$ 32 445148 880950 B12 745.2 20.00 1985 KE \$ 32 445148 880950 B12 745.2 20.00 1985 KE \$ 32 445148 880950 B12 745.2 20.00 1985 KE \$ 32 445148 880950 B12 745.2 20.00 1985 KE \$ 32 445148 880950 B12 745.2 20.00 1985 KE \$ 32 445148 880950 B12 745.2 20.00 1985 KE \$ 32 445148 880950 B12 745.2 20.00 1985 KE \$ 32 445148 880950 B12 745.2 20.00 1985 KE \$ 32 445148 B1000 B12 745.2 20.00 1985 KE \$ 32 445148 B1000 B12 745148 B1000 B	_		_	10.00		19.00		÷		2			
1985 KE 5 22 445150 880724 B11 681.7 40.00 1965 KE 5 22 445150 880724 B12 681.7 35.50 1965 KE 4 22 445148 880724 B12 680.3 31.10 1985 KE 4 22 445148 880724 B12 680.3 31.10 1995 KE 4 22 445148 880724 B12 680.3 31.10 1995 KE 7 22 445148 880757 B12 1997 XF. 50 1995 KE 7 22 445148 880757 B12 1997 XF. 50 1995 KE 7 22 445148 880757 B12 1997 XF. 50 1995 KE 7 22 445148 880757 B12 1997 XF. 50 1995 KE 7 20 1995 KE					3,60 67.00		≓	\$					
1965 KE 5 22 445150 850724 811 691.7 33.50 1985 KE 4 22 445148 880724 812 690.3 40.00 1985 KE 4 22 445148 880724 812 690.3 31.10 1985 KE 4 22 445148 880724 812 690.3 31.10 1985 KF 4 22 445148 880724 813 749.7 28.50 1065 KF 7 29 44514 800037 814 749.7 28.50				-	98.00		75			ñ			
1995 KE 4 22 445149 889724 B12 690.3 40.00 1985 KE 4 22 445148 889724 B12 690.3 31.10 1985 KE 4 22 445148 889724 B12 831 749.7 28.50 1095 KF 4 22 445148 88974 B13 749.7 28.50 1095 KF 7 23 44514 80003T B13 749.7 28.50		4.705-04	^										
1985 KE 4 22 445148 880924 B12 690.3 31.10 1985 KE 4 22 445148 880940 B13 749.7 28.50 1986 VE 1 22 445148 880940 B13 749.7 28.50				29.00 99	99.00		'n	~		88			
1985 KE 4 22 445148 880940 813 749,7 28,50		1.30E-03	P.				ಜ	_					
1000 NE T SO AFRICE BONDE BULL TAN SOL			•		8		AS-AS	-		≃			
OC. C. J. OF T. STUTE GOTTON OF THE C. S.				4.00	26.00 38.00	00 35.00		ĸ		23	32.7	19,3 4.5	۳:

Appendix 3 - HYDROSEOLOGIC AND ENSINEERING DATA FOR OCONTO COUNTY LANDFILL

						• •									*****												
+ IDENTI	ITY										+ HYBRAULIC				+ GRAINS	IIE PERCEN	TASES		+	ENSINEERI	NG PROPE	RTIES					
+		Litho-									CONDUCTIV	ΙΥΥ			+	Matrix I	Matrix 1	Matrix Z	ŧ								
+		strat.						Surf.	Sample	Saaple	+				+	Sand	silt	ctay	+	Unified	Bulk	Bry					+
+ County	,	unit !	iat.	Site			Breg.	Elev.	top	botton	tab K	Heth	Fld K	Heth	+ Bulk I	(2.0 to	10.0625 to	0	÷	Soil	Percent	Unit Wt.	SPT	Hoist.	Liquid	Plasti	c. DE +
+ (code)	Year	(cose) ((sbo)	No.	Lat.	Long.	no.	(ft)	œ	(ft)	(ce/s)	Code	tca/s)	code	+ >2.0mm	0.0625aa)	0.002mm)	((0.002ee)	ŧ	Class.	P200	(pcf)	(10)	cost. (%)	lieit	index	itsf) +
or	198	KE.	3	23c	445016	POALLE	81	722 4	10.0	11.0			*****		28		***********			32	36		46				
00	198		99	23c	445014			714.5		16.0					40					SH	39		16				
90			"	23c	445024	880606		704.1		11.5										90	31		28				
nc nc	178		7	23c		BB0504	86			6.0					20					er er	30		32				
DC			3	23c	445012		88			6.0					£1					70	65		15				
30	198		ž	23c		880611	88			6.0	4.00E-08	51			-						00						
DC.			99	23c	445024			,		40.0	8.000 00					1		•		SP-SM	á						
90			3	23c	445016				9.5	11.0					18					CL	73		65				
20			3	23c	445012			720.6		4.0	6.00E-08	53			•••					SE							
36	198		99	23c	445012				35.0	41.0	*****	-	1.31E-04	8	ı					SP			84				
30			3	23ε	445016					2.0	2.00E-05	53								SC			4				
90	198		3	23ε	445016					4.0			8.7		i					CL	55		i				
30			3	23c		880525					1.008-07	53															
90			5	23ε	445016					16.0	******	•••								CL	68		62				
90			99	23c	445026					40.0					ī	,				SP							
30	198	KEK)	3	23b	444113				2.0	7.0					Š	34	51	15	i	EL	66				31	. 1	4
00			3	235	444114				16.0						- 4	25		26		CL	78				39		23
OC.			3	23b	444331	B81024			9.0						7	16	44			CL	78				33	i 1	9
DC			3	235	444110			ı	3.0							2				Q.	81				4:	2 7	? \$
BN	198	KEKI	3	232	443921	880902	B1		8.0						73	27		33	Ţ	CL	73				44	, ,	17
BN	198	4 KEKI	3	23≥	443921	B80907	82	!	3.0	9.0					78	3	3 4:	26	5	CL	76)			3:	\$ f	19

SPT Maist, Liquid Plastic, UC + (K) Cont.(1) limit index (tsf) + 2 2 \Box ≳ = 计特货银行 2222 S € 5 29.9 18.0 28 61.8 23 표 욹 Unified Bulk Dry Soil Percent Unit Mt. S Class. P200 (pcf) t 11.5 119.8 61.1 133.1 ENGINEERING PROPERTIES ವರವದವದವದ ಧರ್ಮ ರ a.P., a.e. ದ ವ ಕ ಕ ರ ವ ವ ವ ವ ವ ಭ ವ ಸ ವ ವ ವ ವ ವ ವ ವ ವ ವ DOC-ONLTE DOLOKITE CH SH-SC CL.SH-SC DEDROCK Natrix 2 Natrix 2 Natrix 1 sand silt clay 20 Fld K Neth + Bulk I (2.0 to (0.0875 to (0.0875) code + 72.0mm 0.0825mm) 0.0825mm) ((0.092mm) 祖の公の私 ន == 2 2 2 12 22 24 25 24 25 24 25 9 2 3,5 + GRAINSIZE PERCENTAGES 22 6.93E-07 5.506-07 1.256-05 2.85£-05 1.00£-05 5. BHE-07 3,345-06 Neth Code -+ HYDRAULIC + Conductivity Sample Sample + top bottom + Lab K R (ft) (ft) + (cm/s) : 3.28E-08 2.795-09 3.592-09 4.285-08 8.805-09 730.8 731.5 731.5 733.3 733.4 734.2 734.2 734.2 734.1 737.1 737.1 737.1 737.1 737.1 737.1 737.1 737.1 887035 DM3018 B 887035 P015 B 887035 P015 B 88703 P015 B 88703 P015 B 887018 B 87018 882003 MW218B 882003 MW218B 882035 8219 882025 8220 882015 B221 Prag. Long. + County unit Nat. Site + (rode) Year (code) (code) No. 1982 KER1 1982 KER1 1982 KER1 1982 KER1 1982 KEN1 IDENTITY

2.6 5.0

Appendix 3 - Hydroseologic and engineering data for outsgame county, outsbame county landeill

SPI Moist, Liquid Plastic, UC (M) cont.(2) limit index (fsf) 222575288883325252 8 E = = = 22.9 21.0 24.4 24.9 17.1 24.0 18.0 **= 22 = =** Bulk Bry Percent Unit M1. S P200 (pcf) ((pcf) 104.7 GRAINSITE PERCENTAGES + ENGINEERING PROFERILES
Matrix I Matrix I Matrix I + 2 2 2 2 2 4 4 2 2 2 Unified Soii | Dass. + Bulk I (2.0 to (0.0625 to + 20.0ss 0.0625ss) 0.002ss) ((0.002ss) ¥ 9 6 I **42522222222444444444** ************************ 222222 = **#** # # # # # # Fld K Neth (ce/s) code 2.3第七8 5.24E-05 4.14E-05 2.16E-07 3.33E-06 7.406-06 3.206-06 Sample Sample +
top bottox + Lab K Meth
(#t) (#t) + (ta/s) code 4.30E-08 + HYDRAILIC + CONDUCTIVITY 2.90£-08 1 · 80-306-1 1,70E-08 1,30E-08 2.706-07 1.70E-07 3.30£-08 7.905-08 1.10E-08 1.50E-08 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25 5.3 40.6 20.0 20.0 20.0 \$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\frac{1}{2}\$\$\fra 713.9 713.9 713.1 713.1 711.5 711.5 711.5 719.3 719.3 718.1 £ 5. Bras. Lost. 41172 41173 41173 41173 41173 41173 41173 41173 41173 41173 41173 41173 41173 41173 41173 41173 41173 41173 41173 41173 41173 41173 41173 41173 41173 41173 41173 strat. unit Mat. Site (code) (code) No. 313 3513 + County ut + (code) Year in

Rodendia 3 - Hydrobeclogic and engineering data for cutagrate county, outagrate county largetle

5 2 5 5 5

2.7

SPI Moist, Liquid Plastic, UC + (E) cont. (2) limit index (18f) + 28.0 16.9 5.0 5.0 15.0 18.0 15.0 15.0 15.0 **\$** \$ + Unified Bulk Dry + Soil Percent Unit Ht. + Class. P200 (pcf) 128.0 115.0 114.0 11.0 112.0 112.0 + ENGINEERINS PROPERTIES 2 2 ತರವರಕ್ಕಿಸಿ 55 ತ Hatrix X Hatrix X Hatrix X + sand silt clay + Fid K Neth + Bulk I (2.0 to (0.0625 to (re/s) code + >2.0se 0.0625es) 0.002se) ((0.002se) =2222 \$ ☆ + SRAINSIZE PERCENTAGES DNR 3.93E-07 1.05E-05 1.78E-06 3.13E-06 1.00E-05 2,046-08
2,916-06
1,586-06
1,586-06
1,586-07
3,186-05
1,986-07
1,986-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,586-07
1,5 Reth Code + HYDRALE IC + CONDUCTIVITY Sample Sample +
top bottom + Lab K
(ft) (ft) + (cm/s) 22.0 22.0 42.0 42.0 45.0 45.0 26.0 21.6 16.2 15.0 28.0 15.0 15.0 737.77 737.77 737.77 737.74 737.74 737.74 737.74 737.74 737.74 737.74 737.74 737.74 737.74 737.74 737.74 737.74 737.74 737.74 737.74 737.74 737.74 Surt. Brng. Elev. 20. (#1) B 44.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (1974) 1.0 (197 882042 882050 882199 882199 882199 882199 882103 882163 882060 882060 882060 882051 882042 882107 882107 882104 882104 882104 882104 882104 882107 882044 882044 882050 882199 882199 882199 882199 882194 8822047 Site Bo. strat. unit Nat. Si (code)(code) N + County u + (rode) Year (

2

Appendix 3 - Hybrobeologic and Engineering data for Outramile Comity, Outramie County Landfill

DEKTITY										+	+ HYDRAULIC			+ GRAINS	GRAINSIZE PERCENTAGES	NTABES		7	* ENGINEERING PROPERTIES	IS PROPERT	231				
	Lith									Š	+ CONSUCTIVITY				Hatrix	Matrix I Batrix 2 Hatrix 1	Y Matri								
	stra	strat.					Surf.		Sample Sample +	+ 47					gues	silt	£33y	+	Unified	쭚	à				
· County	mit	Hat.	ž.	*		Pro.	Brng, Elev.	\$	bott	+ 80	å X de	Neth Fld	K Keth	+ Bulk I	12.0 to	10.0625	۽	*	Soil	Percent U	nit IR.	SPT No.	st. Ligu	SPT Moist, Liquid Plastic, UC	2
+ (code) Year (code) (code) No.	ear (cod	e) (codi	F. ₩0.			Losq. no.	€		eft) eft)	(tt) + (co/s)	93 (8/8)	code (ca.	15) code	+ >2.0as	0.062588	(ca/s) code + 22.0as 0.0625as) 0.002as) ((0.002as) +	(0.00)	+ (48)	Class.	Class. P200 (pcf)	(Jzt)	(N) ton	12 (2)	(W) cost. (2) limit index (tsf	£
	1974 KEM		× ×	1	PF 882199	ì	88 738	9.5	9,	0						3.0 8.0			墇		0.601		3.0		2
2	974 KENS	144	3 24	1 44173		3	13.	737.3 25						٥	ř	8	60	16	ದ	\$			25.0		?
			3	4417	_	16 B1	133			٥									ದ		112.0	•	5.0		-
_		-	3.22	1 44173		18 93	133				7.486-07								ದ						
	974 KA	 	⊼ 2	44173										•	~			29	7	ĸ					
	974 KI	 	2	_	S 882046		333	37.3 40		۰				•	2	- 22	~	-	ರ	ž					
	1975 KI		2	_	28 682050		3	ř		•									₽ d		97.5		32,0		2.3
		 W	2 2		_		£	ž			28 P								걸						
	975 XE	щ	₹ 5	_	28 682042	12 344	3	×			4.53E-09								ದ		110.0		9.0		÷
	×		22	_	38 882050		¥	≈											겁		111.0	.,	23.0		2
_	1975 KEE1	_	3 24	_	\$8 BB2050	55 88 88		*			80-369								ದ						
_	979 KENI	-	≈	441721	21 882107	27 B134			25.0 27.0		1.536-07	m		m	=	•	ı,	25	ಕ	2					
_	1979 KI	щ	≈ •	417	26 882107	07 B15A		736.6 40		۰				•	=		\$	¥	ಕ್ಕ ದ	8			40.0		23
8	1970 M		7	121171	F15000 F1	44													•						

+ Unified Bulk Bry
+ Soil Percent Unit N: SPT Moist. Liquid Plastic. UC +
+ Class. P200 (pcf) (W) cont.(1) limit index (tsf) + 2 28828282828282828282828 19.9 14.0 17.0 17.0 14.0 14.0 26.0 26.0 24.0 17.0 18.0 18.0 121.3 121.3 114.0 116.5 116.7 123.0 117.7 116.1 116.1 113.7 120.7 111.1 118.4 122.7 11.7.7 + ENGINEERING PROPERTIES ಧರಧಧರ**ವ**ರದ ಕ ಕಕ ひひとひひむむななななひひひひむせぎ ひひとせん かんだん Matrix I Matrix I Matrix I + + sand silt tiay Fld X Neth + Bulk 1 (2.0 to (0.0425 to (ca/5) code + >2.0sa 0.0425es) 0.002as) (<0.002as) £ 23 = けんになけけなおびのなにははなれ **₩** -2 + GRAINSIZE PERCENTAGES 2 4 APPEDDÍX 3 - HYDROBEOLDGIC AND ENGINEERING DATA FOR OTRAKEE COLNIY. THELUDING ANDERSON, DIDJER, AND HEPCO PARPOSED SITES 9 488422222425 6.905-05 1, 706-05 7,505-06 5.208-06 1.906-07 1.506-07 6.306-07 bottom + Lab K Meth (ft) + (ca/s) code + CONDUCTIVITY 1.10E-07 3,206-08 2.505-08 + NYDRAULIC 724.4 778.5 778.5 777.3 777.3 777.5 777.5 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 774.0 Surt. Brng. Elev. no. (ft) 919 919 919 920 920 920 921 921 921 921 42151 875477 422151 875477 42253 875121 42253 875121 42250 875121 42250 875121 42250 875121 42250 875121 42250 875121 42250 875121 42250 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 87512 42251 8 + County unit Mat. Site + (rode) Year (rode) (code) No. + IDENTITY

Ç

SPT Moist, Liquid Plastic, UC + (M) cont.(1) limit index (1sf) + 43222775 2.0 32.5.4.5.5 : <u>:</u> 7 33 27.6 222 4 1 2 2 2 2 4 ***** + Unified Bulk Bry + Soil Percent Unit Ut. + Elass. P200 (pcf) 164.5 117.6 125.1 122.0 119.1 + ENGINEERING PROPERTIES 8 3 22222 2 ಶ ರಹದದವವರದ ದರದ 8 + 6RAINSIIE PERCENTAGES + Matrix I Matrix I + 1 + sand silt Clav Fld K Neth + Bulk X 12.0 to 60.0525 to (ce/s) code + >2.0se 0.0625as) (0.002as) 33 # # # 2 3,005-06 Sample Sample + top K Heth (ft) (ft) + (cm/s) code ** + HYDRAIR.IC + CONDUCTIVITY 2,005-08 3 Approdix 3 - HYBROSECLOGIC AND ENGINECRING DATA FOR RACINE COLARY - LAND RECLANATION SITE 5 00F-08 6.30E-06 4.20E-08 1.10E-04 1,666-69 705.8 705.8 705.8 705.8 705.8 705.5 705.5 705.5 705.8 705.8 705.8 705.8 705.8 705.8 705.8 705.8 705.8 Surt. Braq. Elev. Long. no. (ft) 875132 875132 875132 875132 875132 875132 875132 875132 875132 875132 875132 875132 875133 875133 875133 875133 875133 875133 875133 875133 875133 875133 875133 875130 875130 875130 975130 975130 875130 875130 875130 975153 875153 875153 875153 875153 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 14,170 titho
strat.

+ County unit Nat. 5

+ (code) Year (code) inde) ik RR 1975
RR 1975
RR 1975
RR 1976
RR 197 + IDENTITY

SPT Moist. Liquid Plastic. UC + (N) cont.(2) liait index (tsf) + X 2222 + Unified Bulk Bry + Soil Percent Unit Wt. + Class, P200 (pcf) 122.5 126.5 120.0 180.6 19.3 ટુ ≢ = ದ ರ ದ ದ ದ ದ ದ ನ ನ ರ ನ ರ ನ ರ ರಕರದದಹದಹದಕ್ಕೆ ಹೆದವನ್ನೆ ಹೆ ದ ದಹಿನಿ # ದ ದ # ರ ಧ ವ ದ ದ 53-55 54-55 Ct, 78, 53 ರ ವ ಈ ಹ ರ ರ ಈ ರ ರ + sand silt clay + Bulk I (2.0 to (0.0525 to +)2.0se 0.0525as) 0.002es) (<0.002es) z 25 22 -£ 33 5 + GRATHSTTE PERCENTAGES Ξ, Fld K Neth (cs/s) code ~ ~ 1.00£-06 6.00£-07 2.60E-05 1.00E-05 1,005-05 8,005-07 3,006-03 2.005-06 £ 50 + Hydrau.ic + Conductivity 2.005-08 3.005-08 2.06.48 bottos + Lab K (ft) + (ca/s) 685.6 685.6 685.6 685.6 685.6 685.6 685.6 685.6 685.6 Suri. Brng. Elev. Long. no. (ft) 875132 875132 875132 875132 875132 875154 875154 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 1473 4 14 + County unit Mat. + (code) Year (code) (code) + 1DENTITY

Apoendix 3 - HYDROGEOLOGIC AND ENGINEERINS DATA FOR PACINE COUNTY - LAND RECLANATION SITE

+ Unified Bulk Bry + Soil Percent Unit IR: SPT Moist, Liquid Plastic, UC + + Class. P200 (pcf) (N) cont.(2) liait index (tas) + 22.1 13.0 16.3 + Matrix I Matrix I Matrix I + EMENMERRING PROPERTIES
+ sand silt clay + Unified Bult Dry
+ Bulk I (7.0 to (0.025 to + Sail Percent Unit Mi
+ 72.04s 0.06254si 0.0024si ((0.0024s) + Class. Powe z 28 12 ¥ ĸ 23 **...** \approx 2 Fld K Neth 1.005-07 Heth Code 5,008-68 3 + HYDRAUR.IC + CONDUCTIVITY 7,005-07 3,005-08 E Sample +
Dottom + Lab K
(ft) + (ca/s) 9,10E-08 4,60E-08 3,705-08 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 653.8 Surf. Brng. Elev. no. 1ft) B75150 875545 14.22 14.22 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 14.23 + County unit Nat. + (code) Year (code) (code)

Appendix 3 - HUROSECLOGIC AND ENSINEERING DATA FOR RACINE COUNTY - LAND RECLANATION SITE

SPF Boist. Liquid Plastic. UC + (8) cont. (1) lisit index (18f) + 2.5 3.5 222 2.5 3.5 3.5 5.5 2.2 20 2 2 2222 + Unified Bulk Dry + Soil Percent Unit Mt. + Class, P200 (pcf) | Motrix I Matrix I Matrix | HostikERING PROPERTIES | + Sand Silt Clay + Unified Bult Dry | Fld K Meth + Bult I (2.0 to (0.0625 to + Soil Percent Unit Mitcafs) code + 72.0sm 0.0625ms) ((0.002sm) + Class, Ponn | Hostik Mitcafs) 8 ರಹನ್ನರದ ಆನ್.ರವರ <u>ಈ</u> ಸೆ.ಸ. ರಧರ ರಹ್ಯದರದ ಹಪ್ಪಕ್ಷನ್ನ ಹಿಕ್-ಹಿಕ್-ಹಿಕ್-ಹಿಕ್-ಹಿಕ್-5.756-06 3.89£-05 Sample Sample +
top bottom + Lab K Neth
(Ht) (Ht) + (tm/s) code + HYBRAUR, IC + CONDUCTIVITY Appendix 3 - HYBROGEOLOBIC AND ENBINEERING DATA FOR RACINE COLATY - LAND RECLANATION SITE Ξ.5 Surt. Brag. Elev. no. (ft) 875170 864 875170 824 875170 824 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875170 854 875153 B4N 875153 B4N 875155 B4N 875155 B4N 875155 B4N 875155 B4N 875155 B4N-1 Long 875145 875145 44.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64.233
64 unit Hat. (code) (code) + County u RA 1984
RA 1985
RA 1988

SPT Most. Liquid Plastic, UC : (N) cont.(2) limit index ((st) + 2.5 2.6 4.5 4.5 2.2 2.2 3.0 3.5 2 5 9 22 + Unified Bulk Dry + Sail Percent Unit Mt. + Class, 9200 (pcf) Harry I Hatry Hatrix I + EMBINEEGING PROPERTIES Sand silt S ದ ಕ್ಷ ಸ್ಥ 祖 祖 祖 祖 祖 Fld K Beth + Bulk X (2.0 to (0.0625 to (ca/s) code + 22.0m 9.0625ms) 0.002ms) ((0.002ms) ĸ S ĸ \$ ş **BRAINSITE PERCENTAGES** Sample Sample +
top buttom + Lab X Meth
(ft) (ft) : (re/s) code + KYBRAULIC + CONDUCTIVITY 699.8 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 685.5 Elev. 24.7 (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19.2) (19. Brag. no. unit Hat. (code)(code) + County u * IDENTITY

Appendix 3 - HYBKOGEOLOGIC AND ENGINEERING DATA FOR RACINE COLNTY - LAND RECLANATION SITE

2

æ

SPT Moist. Liquid Plastic. UC (H) cont.(Z) limit index (tsf) 2224222222 38 27 ********* + Unified Bult Dry + Spii Percent Unit Nr. + Class, P200 (pcf) * ENGINEERING PROPERTIES ç Matrix I Matrix I Matrix I + + sand silt riay
Fid K Meth + Sulk % (2.0 to (0.0625 to (cefs) code + 22.0ee 0.0625as) 0.002as) ((0.002as) 2 క్ష + GRAINSTIE PERCENTAGES ₽ 2 e Sample +
bottom + Lab K Neth
(ft) + (cm/s) code + HYDRAULIC + CONDUCTIVITY Appendix 3 - Hydköseclöble and Engineering data for racine county - Land reclaration site 2.705-09 B. 20E-08 20.5 9°,0 Sample Staple S 555 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 565 0 56 690.5 690.5 690.5 690.5 690.5 690.5 690.5 690.5 690.5 690.5 675.0 675.0 675.0 675.0 675.0 670.5 670.5 670.5 670.5 670.5 670.5 670.5 670.5 670.5 670.5 670.5 670.5 690.5 690.5 690.5 690.5 690.5 590.5 Surt. Brng. Elev. no. (ft) 875137 875137 875137 875137 875137 875137 875137 875137 875137 875137 875137 875137 875137 875137 875137 875137 875137 875137 875137 875137 875137 875137 875137 424235 424235 424235 424235 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 424236 42 + County unit Hat. + (code) Year (code) (code) + IBENTITY

2 0

7

7.7

2.7

z

8

1.6 3.6 3.6

Ħ

ĸ

0.

2

7 7 7 7

ĸ

ŝ

n

SPI Moist. Liquid Plastic. UC + (M) cont.(I) Limit index (1st) + sot plastic B æ 9 ន 5 Unified Bulk Dry Spii Percent Unit Mt. S Elass. P200 (ptf) + ENSINEERING PROPERTIES + GRAINSIZE PENCENTAGES
HATTIX I MATTIX I to sand silt clay Fld K deth + Bulk % (2.0 to (0.0625 to (cefs) code + 22.0ss 0.0625as) (0.002as) (0.002as) 28 ŝ 2 F K ŝ Saple Samie + top X Neth (ft) (ft) + (ce/s) code + HYDRAULIE + EDIDUCTIVITY Aporadix 3 - Hydrogerlogic and engineering data for racine colanty - Layd reclaration site 8 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25 698.3 698.3 698.3 698.3 Surf. Prog. Elev. no. CEU 86.7 Sept. 19. S 675132 675132 675132 675132 675132 875132 675132 875132 875132 875132 875132 875132 975132 975132 975132 975132 975132 875136 875136 875136 875136 : Litho+ strat.
+ County unit Nat. !
+ (code) Year (code) fcode) + IDENTITY

252222

3.5

+	+ -	+						
	± ;	3		2.5	2.5	2.5	2.5	2.5
	Plastic	, ngex						
) design	ij						
	11	8						
	. F.	3	\$	4	13	ä	#	11
-	±.	<u> </u>						
4	at Unit	Š	83					
128	Perce	8						
Unities	 S	13.55	E	ದ	구	<u>ದ</u>	겁	ద
+ + ~	• :	•						
atr.	4	4200.00						
* 2 #	13. 13.	S (88)	72					
natr Es	60.03	6.6						
atrix ,	2.0 to	06250						
	14.1	0.	~					
• •	*	*						
	7 E	3						
	£16	3						
¥114	Heth	8						
BRIDE	Lab K	3/8						
- + - #a	tos t	-						
Je San	to S	Ĕ	٥.	0.	٥.	φ.	0	ة.
Š	8	≝	2 70	.2 75	.2	.2	2 30	1.2 95.0
Sw.t.	Elev.	2		-				
	Brag.	•						598 05
		Š						
	3	Ė	424233	424233	424233	424233	424233	424233
	Site	9	8	22	23	38	æ	8
	Mat.	(Lode)	8	\$	m	m	m	\$
strat,	unit	E G	ෂ	쓤	絽	용	æ	8
	,	125		-		-		
	County	ğ i	æ	\$	ž	æ	æ	æ
	Surf. Saple Suble + sand silt Clay	Suri. Saple Saple + sand silt clav Site Brng. Elev. top bottos + Lab K Neth Fld K Neth + Sult I (2.0 to (0.0425 to	Surf. Sample Sample + Ludwoollyziii + Site Bran. Elev. top bettom + Lab.K. Meth + Hd K. Meth + No. Lat. Lung. no. (ft) (ft) + (cm/s) code (cm/s) tode +	Surf. Sample Sample + Commodifying + Asing silt crisy Fand Silt Clay Clay Fand Silt Clay Clay	Surf. Sapie Samile + Composition + Surf. Sapirat Amelian America to Beng. Elev. top bettons + Lab K Meth Fld K Meth + Bulk I (2.0 to (0.0425 to no. (ft) (ft) + (cn/s) code (cn/s) code +)2.0es 0.0625ms) 0.0025ms) ((0.0025ms) 889 709.2 70.0 0 2 21 72 6	Surf. Sample Sample + Commodifying + Sample Sample America F. America F. Sample Sample Commodifying the Sample Sample Sample F. Sample Sample Common	Surf. Sample Sample - Ludwoolijiii	Surf. Sample Sample + Cumpotifying + Sample sample + Sample Sample + Sample Sample + Sampl

Maist. Liquid Plastic. UC + cont. (2) liait index (tsf) + 3 :3 28888278 <u>353</u>82282828 8822825825822222228888 + Unified Bulk Dry + Soil Percent Unit Mt. + Class, P260 (ptf) 107.8 126.9 104.5 110.2 106.9 · ENGINEERING PROPERTIES Hatrix & Katrix & Matrix & : + Sulk I (2.0 to (0.0625 to + 20.0se 0.0625sm) (0.002m) ((0.002m) ĸ GRAINSIZE PERCENTAGES ***** 3222222223222 = m - 12 m 23 25 Fld K Neth (ca/s) code Neth Code + HYDRAUR. IC + COMBUCTIVITY 2.13E-03 2.16E-03 4.62E-03 8.576-05 2.306-06 1.236-02 8.296-03 7.826-03 2.276-03 1.40E-02 1.06E-03 2.87E-05 1.08E-04 1.70E-04 1.77E-05 7.97E-03 3.01E-03 2.83E-03 9.62E-04 1.75E-04 1.75E-04 4.94E-04 B.84E-05 Lab K (ca/s) 6.55E-06 1.08E-07 1.99E-04 6.25E-05 Sample + bottom + 1 (ft) + 894313 88803 894313 88803 894313 88804 894313 88804 894313 88804 894313 88804 894314 88804 894314 88801 894314 88801 894314 88801 894314 88801 Brag. 894311 D 894313 D 894313 D 894313 D 894313 D 694398 1 894308 1 894308 1 694308 1 894308 1 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 45124 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 451224 45124 451224 451224 451224 451224 451224 451224 451224 451224 4512 unit Mat. Site (code)(code) No. County (code) Year

Appendix 3 - HYDROGEOLOSIC AND ENGINEERING OATA FOR SAUX COUNTY, BASF SITE

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR SAUK COUNTY, BAAP SITE

+ IDENTII	ſΥ				******					+	HYDRAU TO				041503 ±	11F PERFE	TAGES Hatrix X milt			ruerus per	KC DOOD						
+		Litho-								,	CONDUCTIO	111			+ ounted	Mateix 9	Mateix Y	Hatrix I clay (CO 00700)	* 1	CHOIMEEKI	NO PRUPE	KIIES					+
+		strat.						Surf.	Sagole	Sample +	DD:0000111	***			,	Harrit T	. 211124 ·	SALEST &	•	thi fina	b.14	B					+
+ County		unit	Nat.	Site			Brag.	Elev.	top	bottom +	Lab K	Neih	Flax	Keth	+ Roll 7	42.0 44	10 0135 4	CIAY	•	Cail	Bulk	Dry	***	W-7-1			4
+ (code)	Year	(code) ((code	No.	Łat.	Long.	ND.	(ft)	(ft)	(ft) +	(ce/s)	4b03	icais)	rode	+ 32 And	0 04254e1	0.0023 10	((0.002aa)	•	2013	POON	DRIT MI,	521	M015t.	Liqui	Plastic	. DC +
********															. /4444		V. VVZ447	((0,0)28)		LIA33.							
SK	1982	HO	4	29	432229	894313	DBM02	918.2	103.5	105.0	3.39E-03	3			,	- 00	1			SP							
SK	1982	HO	4	29	432229	894313	DBM02		128.5		3.18E-03	3			•					SP	•	116.1 107.1	143				
5).	1982	HÔ	4	29	432244	894306	ELB01		6.0		1.38E-04	3			59	no.	1			BW-6M		127.4	10				
SK	1982	HD	4	29	432244	894306	ELB01		8.5		4.27E-04	3			47	89				SP-SH		115.3	18				
SX.	1982	110	5	29	432244	894366	ELB01		13.5		1.10E-06	3			· ·	38	ı			JA JA		125.0	20				
	1982	Ю			432244	894306	ELB01	899.2	19.5	20.0	1.16E-05	3								10	•	118.3	20				
	1982	ю	4	29	432244	894306	ELBOI	899.2	23.5	25.0					0	94				SP-SM	9		16				
	1982	HĐ	4	29	432244	894306	ELBOS	899.2	28.5	30.0					3	90				SS	14		27				
	1982	ю	99		432247				6.0	7.5	4.61E-05	3								SP-SH	•••	134,7	15				
	1982	HO	99		432247	894302	EL802	902.8	8.5	10.0	8.21E-05	- 3								SP-SH		129.3	21				
	1982	HS	+	29	432247				13.5	15.0	2.31E-04	3			40	93				SP-SM	7	129.7	28				
	1982	揃		29	432247	894302	EL802	902.8	18.5	20.0	2.41E-04	3			0	97				SP-SM	á		13				
	1982	HO	4	29	432247	894302	EL802	902.8	23.5	25.0	1.01E-03	3			28	96	ı			SP	5		26				
	1982	HO	5		432247	894302	ELB02	902.8	28.5	30.0	3.39E-06	3			. 0	43				14	61		27				
	1982	HO	4	29	432240	894303	ELB03	910.4	6.0	7.5	8.69E-04	3			3	96				SP-SM	6		41				
	1982	Ю	4.	29	432240	894303	ELB03	910.4	8.5	10.0	2.55E-04					•••				SP-SH		119.6	40				
	1982	桕	4	29	432240	894303	EL803	910.4	13.5	15.0					59	B0				6P-6N	8		80				
	1982	HÛ	4	29	432240	894303	ELB03	910.4	18.5	20.0	5.4BE-03	3			8	100				SP-SH	6		14				
	1982	HO	4	29	432240	894303	ELB03	910.4	23.5	25.0	9.40E-03				19	98				5P	ă		32				
	1982	HO	4	29	432240	894303	EL803	910.4	28.5	30.0	2.53E-03				0	99				SH	18		27				
SX	1982	HO	4	29	432240	894303	ELB03	910.4	48.5	50.0					Ŏ	91				SM	19		17				
	1782	HO	6	29	432237	894300	EL804	905.6	5.0	7.0	B. &1E-08	3				•••				CL	• • • • • • • • • • • • • • • • • • • •	109.7	• • • • • • • • • • • • • • • • • • • •				1.4
SK	1982	HĐ	4	29	432237	894300	ELB04	906.6	8.5	10.0	1.18E-04	3			51	76				SH	15	121.6	15				1.7
SK	1982	HO	4	29	432237	894300	EL804	905.6	13.5	15.0					49	77				EN-EN	8		39				
	1982	Ю	4	29	432237	894300	ELB04	906.6	23.5	25.0					0	59				SH	49		20				
	1982	HO	4	29	432237	894300	EL BOA	906.6	28.5	30.0	7.97E-03	3			2	97				SP		114.1	17				
	1982	HO	99	29	432237				48.5	50.0	1.55E-05	3			_					SH	•	115.3	26				
SK	1982	HO	3	29	432234	894258	EL905	919.6	13.5	15.0					43	79				SH	13		58				
	1982	Ю	4	29	432234	B9425B	ELBOS	919.6	18.5	20.0					0	93				SP-SH	12		24				
	1982	Ю		29	432234	894258	EL805	919.6	28.5	30.0	3.65E-03	3			0	100				SP-SH		98.4	26				
	1982	HD	4	29	432234				48.5	50.0	6.61E-03	3			Ġ	100				SP	5		12				
	1982	Ю	•	-	432235				9.5	10.0	5.52E-05	3			54	80				6P-6H	10		19				
	1982	ю		29	432235				13.5	15.0	1.63E-03	3			0	99				SP-SM		107.7	14				
	19B2	HO		29	432235	894250	ELB06	922.7	18.5	20.0	1.40E-03	3								SP-SN	•	106.2	17				
	1982	HO		29	432235				23.5	25.0					0	88				SM	23		29				
	1982	HO		29	432235				28.5	30.0	4.18E-03	3								SH		107.8	25				
	1982	НÔ		29		894250			48.5	50.0	1.3BE-03	3			. 0	97				SP	4	106.1	30				
	1982	Ю	99					A 902.8		7.5	1.37E-05	3			33 59 00 19 00 00 22 43 00 00 54 00 00 10 10 10 10 10 10 10 10 10 10 10	86				SH		121.8	30				
	1982	Ю		29				A 902.8			1.22E-04	3			66	85				6P-6M	6		18				
	1982	HO	99					A 902.8			1.08E-05	3									•	123.9	32				
	1982	HO	99		432241	894307	ELNOI	4 902.8	18.5	20.0	B.71E-06	3			10	86				SM	17	129.4	18				
	1982	HO	99					A 902.9			8.03E-05	3			1	88				SM		117.3	31				
	1982		99					A 902.B			3.86E-05	3								SH		120.1	25				
	1982	HQ		29	432241	894307	ELN01	A 902.8	78.5	80.0					2!	96				SP-SH	Å	101.4	188				
	1982	HO	4	29	432241	894307	ELN01	A 902.8	103.5	105.0	9.06E-01	3			0	99				SP-SH	11		77				
SX	1982	HO	4	29	432237	894252	ELN02	A 912.1	13.5	15.0	1.77E-05	3			5i	Bå				SP-SM		126.6	25				

Appendix 3 - HYDROSEDLOSIC AND ENGINEERING DATA FOR SAUK COUNTY, BAAP SITE

+ IDENTII :		ithe-									HYDRAULIC			+ BRAINS	IZE PERCEN					ING PROPE	RTIES					
t		itrat.						c	C		COMPUCTIV	111		+	Batrix I	Matrix I										
• County		nit Hat					D	Class	258018	S PERCIE 4				+	Sand	silt				Bulk						
	_	(code) (cod		i	2		Brng.	EIEY.	top	pottos +	Lab K	Heth	Fld K Heth	+ Bulk %	(2.0 to	(0.0825 to	•	+	Soil	Percent	Unit Wt.	SPT	Koist.	Liquid I	Plastic	U€
						LDDG.	no.	(32)	{† t }	(96)	(ca/s)	code	(ca/s) code	+ >2.0sa	0.0625es)	0.002mm)	1/0 000-		*1	POAA	1	f lat	199	11.74	4 - 4 -	44 65
27	1287	HU	•	21	432237	E94252	ELHO2	A 912.	18.5	20.0				72	61				Ka	12		46				
	1982	HC	4	29	432237	894252	ELNO26	912.1	23.5	25.0				60	65				6N	41		38				
	1982		4	29	432237	894252	ELM62/	912.1	53.5	55.0	1.86E-03	3		0	100				SP		103.5					
	1982		4	29	432237	894252	ELN02	912.1	103.5	105.0	5.60E-04	3		10	97				SP		114.1					
	1982			29	432237	894252	ELNO2	912.	140.5	142.0				2	100				SP			37				
	1982		ė	29	432233	894250	ELNO3A	925.2	2.5	4.5	3.08E-07	3		0	11	65		24	CT.		116.4			42	23	2.3
	1982				432233						2.9BE-05	3							SP-SH		111.6					
	1982		4		432233									50	84				SP-SM	9		44				
	1982		4		432233						1.66E-03	3		0	95				SP-SN	10	110.7	18				
	1982				432233						6.12E-03	3		0	100				SP	4		16				
	1982		4		432233						1.53E-03	- 3			95				SM	12		28				
	1982		4		432233						1.20E-01	3		13	95				SP-SH	9		90				
	1982		ŧ		432233	894250	ELNO36	925.2	78.5	80.0				45	91	- 1			SP-SM	10		200				
	1982		4	29	432233	891250	ELNG34	925.2	103.5	105.0	5.00E-05	3		10	88				SH	12	115.5					
	1982				432233						2.01E-03	3		7	99				SP	4		147				
	1982			29	432235	894308	ELNO4#	921.4	3.0	5.0	1.26E-07	3		0	5	74		21	CL	97				43	20	1.5
	1982		3	29	432235	894308	ELHOTI	921.4	6.0	7.5				á	68				SE	36		5			•••	110
	1982			29	432235	894306	ELN048	921.4	8.5	10.0	4.64E-04								SH		122.4	-				
	1982		4	29	432235	894306	ELN04	921.4	13.5	15.0				51	71				SH	17		74				
	1982		4	29	432235	894306	ELNOSS	921.4	18.5	20.0	1.19E-04	3		59	80				59-SH	9						
	1982		4	29	432235	894306	ELMO4	A 921.4	23.5	25.0	8.89E-05	3		56	80				GP-GN	11		44				
	1982		4	29	432235	894306	ELNO44	921.4	28.5	30.0	1.43E-04	3		44	77				SH	14		34				
	1982		4	29	432235	B94306	ELNO4	921.4	53.5	55.0	3.88E-04	3		57	88				SP-SN			44				
	1982		4	29	432235	894306	ELNOAR	921.4	80.0	81.5	6.43E-03	3		16	99				52	2		50				
	1982		4	29	432235	894306	ELNO4	921.4	103.5	105.0	6.21E-04	3		7	96				SP-SM	,		357				
	1982		4	29	432235	894306	ELH046	921.4	150.5	152.0	8.47E-05	3		0	86				SH	14		78				
	1982	HO	3	29	432058	891456	PBB01	876.8	6.0	7.5	1.98E-04	3							SH		124.8	51				
SK	1982	ĦĐ	3	29	432058	894456	P8801	676.5	8.5	10.0				30	61				SM	29		61				
SX	1982	B0	4	29	432058	894458	PRB01	876.1	13.5	15.0				24	93				SP-SM	8		28				
SX	1982	Ю	4	29	432058	894456	10889	876.8	18.5	20.0	1.428-03	3							5P-SH	٠	110.3	20				
\$K	1982	RO	4	29	432058	894458	PB801	876.8	28.5	30.0	7.61E-04	5		24	96				SP-SM	5	117.5	δ5				
SK	1982	HD	4	29	432058	894456	P8801	876.8	48.5	50.0	4.81E-05	3		12	97				52		112.7	38				
SK	1982	HO	4	29	432102	894501	PBB02	893.9	6.6	7.5		•		29	90				SP-SM	9		16				
SK	1982	HG	4	29	432102	894501	PB902	883.9	8.5	10.0	1.61E-03	3							SP-SM	,	119.9	10				
SK	1982	HO	4	29	432102	894501	PBB02		13.5		**********	•		•	97				SP-SM	7		35				
Sľ	1982	HO	4	29	432102				18.5		1.17E-04	3			"				97-36 SP-98	•	112.0	33 42				
SK	1982	HO	4		432102				23.5		٧١	•		٥	99				SP-SM	7		-				
SK	1982	80	4		432102				28.5		2.838-03	3		,					SP-SH	•	110.4	72 24				
SK	1982	HO	4		432102				48.5			•		56	92				SP-SM	6		24 26				
SK	1982	HQ	4		432057				6.0					42	100					i		20 20				
SX	1982	HG	4		432057				8.5		5.75E-04	3		02	.00				er er	•						
SX	1982	HO	4		432057				13.5		2.15E-04								6₩		120.0	71				
SK	1982	HO	4		432657				18.5		24.500 84	•		11	97				92		119.8	38				
SK	1982				432057				23.5					E2	92				SP	4		39				
SK	1982	HC			432057						2.44E-03	₹		52 25	96				KS H2 G2	5		101				
	1982			29	432057	894501	PREST	677 4	49.5	50.0	2.468-03			29 10	96 97				SP-SM		113.5					
			,			311044			70.3	2070	4.105-03	•		10	7/				SP	4	107.4	32				

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR SAUK COUNTY. BAAP SITE

+ IDENTITY										A UVADALE						*******					•				
†	Litho									+ CONDICE	iu Tutty	Fld K. Her	+ PK91	ISIZE PERCE	NIASES	Materia W		engineer!	ING PROPE	RTIES					+
ŧ	strat.	i					Surt.	Saante	- Samir	+	4.111		:	rairix bos	a natrix a	MATERIX A		0-221-4	b. it.	8					+
+ County	unit	Hat.	Site			Brog.	Elev.	too	bottos	+ lab K	Heth	Fld K Net	h + Rull	7 (2.0 to	10 0125 +		Ţ	Cair	Socara Socara	UFY Haid VA	CDT	Madel			
+ (code) Yea	er (code)																								
SK 198				432056																					
Sr 198			29	432056				0.0						8 6	8			SC	34		19				
SY. 198			29		894454				15.0				7	10 B	,			52-55	8		66				
SK 198			29		894454				25.0	1 TOF-	04 3		•	;/ 5	0						86				
SK 198		4			894454			29.5		*****	** 5			99 0	ı			92 92		115.2					
SK 196	2 HO	4	29		894454			48.5		8.28E-	04 3				9			SP	•	107.3	101				
SK 199	32 HQ	4	29	132018	894457	P8805		6.0		1.86E-	-04 3			8 9	2			SH		132.7	7				
SK 198	?2 H2	4	29	432048	894457	P8805	872.	8.5	10.0		05 3			•	-			SP-SH		116.3	33				
SK L9	32 HO	4	29	132048	894457	P8805	872.	13.5	15.0					55 9	7			SP-SM			105				
SK 198		4		432048	894457	PB805	672. ⁴	23.5	25.0	2.56E-	04 3			•				SP		114.5					
SK 19			29		894457			28.5	30.0					9 9	8			SP.			100				
SK 198			29		894457			48.5	50.0	1.86E-	06 3			0 10				SP-SH	-		83				
SK 19		4			894502			8.5	10.0				!	i 8	4			SP-SH			5B				
SK 196		4			894502			3 13.5	15.0	4.85E-	04 3		3	2 9	3			SH-SH		119.6					
SK 199		4			894502			18.5		4.11E	-05 3							SP		124.4	44				
SK 196			29		894502			3 23.5	25.0	5.06E-	0 5 3			8 9	1			SP	3	111.7	92				
SK 191		•			891502			8 28.5						4 9	9			\$P	3		37				
SX 198		4			894502			48.5		B. 23E-	05 3							SP		110.1	88				
SK 191			29		894599			6.0	7.5	8.835	-04 3							SP-SH		119.3	33				
SK 198			29		894599			13.5						3 9				SP SP	5		44				
SK 191		4			894599			18.5					4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	10 8				SP-SM	10		56				
SK 198 SK 198		4			894599			23.5			99 3		1	8 9				SP-SM	å	114.1	98				
SX 198		i			894599			28.5			-06 3		1	0 9				SP-sh	6	110.1	83				
SX 19			29		894599 894459			48.5		1.408-	03 3		_	j 9				SP			98				
SK 198		4			894459			1.0					7	.5 6	7			SK	28		41				
SK 198		1			B94459			3 4.0	7.5	1.41	04 3				_			SP-SH		123. 9	14				
SK 198		4			894459			9 13.5 7 18.5						8 9				SP-SH	-		20				
SK 191			29		894459				25.0		04 3		4	7 9				SP		122.3	34				
SK 198			29		894459			28.5			04 3 05 3			6 9				SP			63				
SX 19		4			894459			48.5		2.026-	V3 3			5 9				SP			80				
SK 198				432113				3.5		1 975.	05 3			8 ∂≨ 0 8				. SK			65				
SX 191		4			B91505			7 8.5		1.772	V			v 8 24 9				SX		121,4	.,				
SK 191			29		894505				15.0	1 A2E-	-03 j		•	(4)	2			SP-SM			19				
SK 191		4			894505			18.5		*****			,	52 9	7			SN		106.3	15				
SK 198	2 HG	4	29		894505			23.5		A 50F.	04 3		,	74 7	,			SP			20				
SK 19	B2 HG		29		894505			7 28.5		0,072	V1 3		;) a	9			S¥ SP		100.8	20				
SK 196	32 HO	4	29		894505			53.5		4.46F-	05 3				,			SP-S#	3		19				
SK 19	B2 KO	4	29		891505				80.0		-03 3		1	י לו	8			orron SP	•	125.5 112.4					
SK 198	2 HO	4	29		894505			98.5			03 s			0 10				SP		105.8	16				
SK 19	92 HO	. 6	29		894557			3.0			-07 3				•			EH 31		93.4	10		52	27	
SK 198	32 HG	99	29		894557			6.0	7.5		07 3							SC	,	123.8	11		JZ	21	
SK 19		4	29		894557			9 8.5			03 3							SW		116.7	49				
SK 196		4	29	432053	894557	PBH02			25.0		03 3							S¥		111.5	37				
SK 19		4			894557		2 870.	9 28.5	30.0		•			18 9	5			SP-S#			44				
SK 191	32 HG	4	29	432053	894557	PBM02	870.	5 3.5	55.0	1.286	03 3		1	2 9				SP		107.6					
														- '	-				•	47.10	,,,,				

Moist, Liquid Plastic, UC cont.(1) limit index (tsf) 2.0 ÷. 22 % € Unified Bulk Dry Soil Percent Unit Wt. (Class. P200 (pcf) 111.0 108.6 105.4 111.9 101.0 118.9 100.2 105.5 118.0 113.6 + ENSINEERING PROPERTIES + ងភុគុគ្គ សំសំសំ Matrix I Matrix I Matrix I + sand silk ciav + Bulk Z (2.0 to (0.0625 to +)2.0ss 0.0625ss) 0.002ss) (<0.002ss) GRAINSTIE PERCENTAGES 2223 Fld K Neth (ce/s) code (ab K Neth (ca/s) code HYDRAULIC CONDUCTIVITY 1.532-03 3 4.42E-04 1.24E-02 3,58E-03 5,74E-04 1,27E-02 4,39E-07 5.80E-05 5.09E-06 8.26E-03 1.62E-04 6.25E-03 2.98E-03 1.06E-03 1.37E-03 4.71E-03 1.38E-04 1.24E-04 1.24E-04 5.32E-03 3.38E-03 4.556-04 1.97E-04 2.50E-04 3.65E-03 3.30E-03 3.82E-03 6.14E-05 5.48E-04 Sample + bottos + (ft) + Szepie (FE) 800.9 18.5 800.9 18.5 800.9 18.5 800.9 18.5 800.9 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 800.7 18.5 £ 5. 89445 PBNOJA 89445 PBNOJA 89445 PBNOJA 89445 PBNOJA 89445 PBNOJA 89445 PBNOZA 894505 PENO34 (894505 PENO34 (894505 PENO34 (894459 PENO44 (894459 PENO4A (894459 PENO3A (894459 894557 P8802 894457 P8802 894403 P8803 894403 P8803 894403 P8803 894403 P8803 894499 P8804 894499 P8805 10. 10. 432053 432053 432107 432107 432107 432107 432107 432107 43219 43219 43219 43219 43219 43219 43219 43219 432103 43204 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 43201 432 Ē unit Mat. (code) + County u + (code) Year i

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR SAUX COUNTY. BAAP SITE

++++	
55 55 € 85	
istic. Idex	
1	
E E	
Maist. Gat. (1	
5. 3	#8~ B#
ئۇچى س	155.4
eedic at this	22.
+ ENGINEERING PROFESTIES + Unified Bulk Bry + Soil Percent Unit + Soil Percent Unit	
INEENI Ified Dii Dass.	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
+ + + + +	
12 X	
5 g	
rix X silt 3425 to 362m3	
+ 6PAINSIZE PERCENTAGES Balrix Batrix Batrix X - sand silt clay + Bulk [2.0 to (0.0625 to + 22.0as 0.0625as] (0.002es)	E 88 85
Estrax Sand 12.0 to	
N X	F ~ 3
最 基 欠	4 4 8
Keth) code	, , , , ,
+ 650ANSIZE PERCENTAGES + EMBINEERING PROPERTIES + BAILY X + BAILY X + HDIFFE BAIL Bry + SAN SILE Clay + HDIFFE BAIL Bry + SOI (0.0025 to + SOI Percent Unit Wt. SPT Moist, Elquid Plastic, UC + (cs/s) code + 72.0as 0.0625as 0.002as) ((0.002as) + Elass, P200 (pcf) (M) code,(I) limit index (Es) +	1
TY Reth code	
+ HYDRAULIC + COMDUCTIVITY P + F + Lab K Meti + (ce/s) cod	3.14E-04 2.15E-06
	- I
ettos	33.50
+ HYDRALIC + CONDUCTIVITY Saple Saple + top buttos + Lab K Meth it (Et) (Et) + (Ea/2) code	894459 PENGA 873.0 18.5 20.0 894459 PENGA 873.0 23.5 25.0 894458 PENGSA 875.8 13.5 15.0 894458 PENGSA 875.8 73.0
# # # # # # # # # # # # # # # # # # #	875.0 1 875.0 2 875.8 1 875.8 2
Suré. Brna. Elev. no. (41)	2 2 2 2 2 2
Bras.	694459 PBNO4A 694459 PBNO4A 694458 PBNO5A 694458 PBNO5A 694458 PBNO5A
Leag	6945 6945 8945 8945
+ IDENTITY : titho- strat. + County unit Mat. Site Brna. Elev. + (code) Year (code) Ko. Lat. Long. no. (!!)	SK 1982 HD 99 29 42041 694459 FBNO44 873.0 18.5 20.0 3.14F-04 3 17 77 54 25 25 25 25.0 5.14F-04 3 25 25 25 25 25 25 25 25 25 25 25 25 25
	22222
at. S ode) #	\$ 65 Kr == =
Litho- strat. unit Hat. Site (code)(code) No.	동중홍홍
	1982 1982 1982 1982
DENTITY County (code) Y	****
₩ ₽ ₽	,

SPT Noist, Liquid Plastir, UC : (N) cook.(1) limit index (tsf) + 4.5 4.5 3.6 3.6 1.5 3.5 21.0 15.0 17.0 17.0 20.6 23.0 21.0 15.0 17.0 후 앞 8 3 8258448 Unified Bulk Bry Soil Percent Unit Ht. 5 Class. P200 (pcf) (+ ENGINEERING PROFERTIES 25525277225 ्रेट स्टब्स्ट स्टब्स् स्टब्स्ट स्टब्स्ट स्टब्स्ट ಹೆ ಹಿ ಹಿ ಹಿ ಕ್ಷ್ವಿ ಪ್ರಪದವದ ಪದವ ಪ್ರಪ್ ಪ್ರಶಿ 7 + sand silt clay + Bulk I (2.0 to (0.0625 to + >2.0mm 0.0625mm) ((0.002mm) Hatrix E Batrix E Hatrix 2 22222/2222222 . GRAINSIZE PERCENTAGES 8 5 Fld X Neth (cm/s) code 5.90E-04 2.00E-03 9.10E-05 9.00E-05 3.00E-04 4.00E-05 5.60E-05 3.20E-04 1.205-04 7.60E-03 bottom + Lab X Heth (ft) + (cm/s) code + CONSUCTIVITY 4.50E-08 5.00E-07 1. 10E-05 1.70E-06 1.70E-05 3.30E-06 + HYDRAULIC 8 € 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 827.0 Brng. 8 881345 881343 881343 881343 881335 881335 881335 881399 883345 883345 883332 883332 883399 883399 883399 883399 883399 683399 88XE) 883523 883622 444610
444614
444614
444614
444616
444616
444616
444616
444616
444616
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
44617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
444617
44617
444617
444617
444617
444617
444617
444617
444617
444617
4446 444899 444899 444899 Ę strat. unit Mat. Site (code)(code) No. + County u + 10EN111Y

Aporadix 3 - Hybroseologic and ensineering bata for syanang county landfill

÷ + + + + + + + + + + + + + + + + + + +	7 1 15 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Squid Plastic, BC Sait index (tsf) 24.0 8.0 2.3 25.0 13.0	Lisquid Lieit 24.0 25.0	ist. Li rt.rti.li 15.0	2 G		PERTIE at this	Perce Political	+ ENGINEERING PROPERTIES + Unified Bulk Dry + Soil Percent Unit + Class. P200 (pcf	* * * * *	+ GROWINSIZE PERCENTABES + Matrix I Mat	283 24 2 25 25 25 25 25 25 25 25 25 25 25 25 25 2	+ 600.1KS1ZE PERCENTAGES + Natrix X Natr sand sand + Balk X 12,0 to (0.06) + 72.0am 0.0625am 0.00 3 34	E PERCI Sand 12.0 to 1.0625e	RAINSII ulb I 2.0mm	4 + - + +	K Ret	P. 0	+ HTGRANE IC + CDNGCCTIVITY Samie + Lab X Meth (ft) + (tg/s) code 4.5	+ HTDRAUE IC + CONDUCTIVITY + Lab K Ne + Ite/s) co	tttos + + + + + + + + + + + + + + + + + + +	Surf. Sasple Saule no. Elev. top botton no. (ft) (ft) (ft) M13 834.9 2.5 4.5 M18 833.2 1.5 10.0	rf. Sapit ev. top t) (ft) 834.9 2.5 833.2 1.5	Surf. Surf. ho. (ft) M13 834.9 M14 833.2	Brng. bo. N.3.	Lane. 883699 883699	Lat. 444899	S S S		Hat. (rode)	Litho- strat. unit flat. (code)(code) KENI 3	IDENTITY Lithorstate Stat. County unit Mat. (tode) Year (tode) (tode) SM 1985 KEX 3 SM 1985 KEX 3
**	0 2.	æ	24.0	15.0			23		d i	±	_	S	*		en .						<u>بر</u>	•	6	83			14899	-	ន		8 ; n	8 ; n
÷	#	index	ij	it.	(E)	œ.	٠	P20	Class.	+	(0.002es	(Sec.)	0.0	.0625	2.088 (+	93 (S	9	8	(C#/S)	+	₹	£	€	2	Legi	ij		ė	(code) No.	(code) (code) No.	+ (code) Fear (code) No. Lat. Long. no. (ft) (ft) + (ca/s) code + X2.0m 0.0625mi 0.002ml (C0.002mm) + Class. P200 (pcf) (N) cont.(E) Limit index (tef) +
•	3	Plasti	19110	ist.	2	#	at Unit	Perce	Soil	+		St	(0.02	(2.0 tr	11 X	+	X.	문		 ₹	108 +	2	ţ	Elev.	8				Site	Mat. Site	unit Mat. Site	• County unit Mat. Site
•						~	<u> </u>	2	Unified	+	CI	.	· 🗷	Sand		••					ale +	ole Said		ä							strat.	strat.
+										+	Hatrix	Z Z	X Matr	Katríx		•			YI IY	CONDUCT	+										Litho-	Litho-
+							PERTIE	186 P.E	MG INEES	+			OCTABES	E PERC	RAINSIZ	+			2	(rDRAUE	Ŧ											200

+ Unified Bulk Dry
+ Soil Percent Unit Wr. SPT Moist. Liquid Plastic. UC +
+ Class. P200 (pcf) (N) cont.(1) limit index (tsf) + Ç; ;2 2 I I ~ ~ 22 22 225 22 2223 ĸ Batrix I Maters Attrix I + EMGINEERING PROPERTIES 3738675 + saed silt ctav Fld K Meth + Bulk X (2.0 to (0.0625 to (cs/s) code + >2.0se 0.0425ss) 0.002ss] ((0.002ss) 22 22 23 3 2 23 춘 찬 2 4 2 4 \$ 2 2 + GRAINSIZE PERCENTAGES ならい印象に引 いけなけれ \$ E 22 5.305-06 7.60E-04 1.20E-04 3.20E-05 2.90E-05 1.30E-05 1.70E-05 1.20E-05 2.10E-05 1. SQE-07 2,206-06 bottom + Lab K Meth (ft) + (ca/s) code m m m 4.10E-05 3 m m + NYDRACLIC + CONDUCTIVITY 8.27E-08 3.33E-03 3.27E-08 1.36E-07 1.88E-07 3.97E-07 6.22E-08 9.786-06 4.74E-08 1.296-08 Sapie S top b 704.7 7 704.7 7 704.7 7 704.7 7 704.7 7 704.7 7 704.7 7 704.7 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 7 704.0 Suri. Brng. Elev. no. Ift) 974722 81 974716 82 974716 82 974716 82 974711 82 974711 82 974721 86 974721 86 974721 81 974717 81 974717 81 974712 81 974712 81 974712 81 974712 81 974712 81 974712 81 974712 81 974712 81 974712 81 974712 81 974712 81 974712 81 974712 81 974712 81 974712 81 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 82 974712 874706 824 874721 8866 874720 8810 874706 88248 874712 8825 874712 8825 regio 434134 434134 434134 434134 434134 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 434135 + County unit Nat. Site + (code) Year (code) (code) No. ************************ $\mathbf{z} \in \mathbf{z} \in$ ************************

Appendix 3 - HYDROGEOLOGIC GAD ENGINERAINS DATA FOR SHEBOYGAN COUNTY LANDFILL

	_
1	
	8
- 6	
ı	
- 7	۰
•	-
	4
- 4	÷
	ú
	į
	ř
- :	3
	-
- 2	7
:	۷.
	ц
- 6	
- 7	
·	
•	•
:	,
	ć
	•
-	
400	•
40192	•
- 6	·
	·
- 6	·
- 6	
- 6	*
- 6	*
2010	
- 6	
2010	
2010	
2010	
MA PAGENTE	
2010	
MA PAGENTE	
PARK PARKING	
MA PAGENTE	
PARK PARKING	
ATE AND PARTIES	
The Auth Park Inter-	
COLD AND CHARLE	
DI OCTO ANA CACAMPE	
DI OCTO ANA CACAMPE	
DI OCTO ANA CACAMPE	
DI OCTO ANA CAMPINE	
COUNTY AND CHANGE	
DI OCTO ANA CACAMPE	The state of the s
SOCIA SOLD AND PARTIES	
PRODUCED OF IT AND PARTIES	
PRODUCED OF IT AND PARTIES	
SOCIA SOLD AND PARTIES	
PRODUCED OF IT AND PARTIES	STATE OF THE PARTY
PRODUCED OF IT AND PARTIES	STREET, STREET
PRODUCED OF IT AND PARTIES	
- NUMBER ACTS AND PARTIES	
PRODUCED OF IT AND PARTIES	
- NUMBER ACTS AND PARTIES	
- NUMBER ACTS AND PARTIES	
- NUMBER ACTS AND PARTIES	
- NUMBER ACTS AND PARTIES	
ALL T . HATSACTH ACTS AND PASSING	
- NUMBER ACTS AND PARTIES	
ALL T . HATSACTH ACTS AND PASSING	

+ IDENTITY								į	•	HYDRAM IC	ن		+ 68818617	SRAINGIZE SESSENTARES	7550		A CHETUCKOTHE BONGEDTIES	de ponoce	1156	-			
•	tithe-								•	+ CONDUCTIVITY	VIIV			strix 1	Natrix I Matrix I	Batrix I +							• •
	strat.		į				Surf.	Szepie	Sample Sample +						si	clay +	Unified	POR	ř.				• •
+ (code) Year	unit Mat. (code)(code)	ficode)	پر دو	1	 8	9 4	Elev.	g (bottos +	× 5	F	Flor Meth	+ Bulk I		(0.0625 to	+	Soi 3	Percent Unit Mt.	Juit Mt.	SPT Moist.	t. Liqui		¥
			- 1	•		1					181	100 (5/8)	(#80790.0 #80.77 ±		0.0020m) ((0.0020m)	+ (#6700.0)	Class.	230	9	(M) cont. (T) light	(Z) Jieit	10dex	(tsf) +
₫:	S :	- ,	2 :	424549	882459	ä		_	15.3								25.	=					
7 3	§ =	n =			887454	B10	1018.0										55 E	43					
Ne 1979	<u> </u>				2000	i		2 2 2	5				•	:	1	,	جم ج	2					
M 1979	5 #	, м			882505	2			2 9			·	~	= :	3	2	≓ : 건	: N		ខ	2	- -0 1	
We 1979	7E4 i	· •			892459	: :	-		2 4				٠.	2 :	₽:	e :	ස් i	3 ;		13			
Nr 1979	7.	, ,,			507769	i			2 2				•	÷:	3.1	2 :	# : d :	5			-		
1970	3	, 14			002454	710	-	3 5	÷ ;					÷ :	Fi i	2	== == :	\$		5 5	-	9	
1679	163.	, r			121000	2 2	-		e e		•		=	7	2	2	7	5		ន			
## 1979	3	3 M3			982454	8 8			8 8			8.90F-93	=	9	Ŧ	\$	ä	S		:			
Na 1979	Œ	-			882454	25	-		÷		-	4.005-05	•	F	÷	\$	₹ .	3		₽			
Me 1979	₹	m			882454	818		38.5	10.0		-	!	Ξ	\$	9	=	=	5		23			
N 1979	3	m			682454	B139			55.2		~	7,005-05	;	!	:	:	ŧ	;		į			
Nu 1979	≝	m			882454	818			50.0				∞.	÷	\$	13	æ	38		2			
4	š	ş			882511	8 2			65.0								重	3		:			
2	5	-			882513	97			45.0								5	=======================================					
	*	m			882505	23			40.0				-0	\$	37	15	균	133		22		_	
	7Et	P3 1			682505	83			30.0				-	55	ĸ	Ξ	ᆏ	R		: 24			
	S	m			882459	2	_	_	55.0				-	=	25	91	7	6		; 5 5	===		5.5
_	5	-			882459	2	•••		45.0				æ	8	5	•	55	=		=			:
	5	5			882500	22		2.5	35.0				٥	7	99	13	루 강	5		2			
1979	5	z :	# :		882449	23		_	9.6		•	3.006-05											
	5 3	3			882449	2		~	 0.		4 7	5.005-04											
	5 3	2 8			882449	100			e e		7	4.005-03											
	5 3	2 8			14759	829			o .		~	9.00E-4											
	5 Z	2 8			444799	9			'n		•	5.00E-05											
	5 ⊋	<u>-</u>	3 5		667501	9	6.76		9		.~	2.00£-05					i						
4	5 ≧	~ ~			8025A1	2 2							•	:	:	!	5	œ ;					
J	3	. 62			882501	ä		* * * * * * * * * * * * * * * * * * *	9 5				•	⊼	3	13	로 2 다	% :			→ '		
2	š	m	22		682501	2			8.0								3 5	8 ₹			-	6 5	
	3	m	2		882501	2	984.6		35.0									8			• -		
1979 1979	5	m	×		882451	83		33.5	35.0				8	2	19	=	8	2		77	•	•	9.6
_	3 !	\$	- F		882451	830			55.0			,	•	2	25	*		£		2			0
'	2	- 1	S.		887503	8		28.5	20.0				ŝ	20			ds-XS	0-		23			:
	5 :	m,	2		892503	33			25.0				0	-	\$	25	겁	86		٠,	*	35	
	5	M (22		882428	833							-	7	22	50	ರ	\$			7	. CO	
-"	£	· ·	7		892458	3	_		\$ 2.0				15	S	23	7	35	₽					
	*	m :	2		882458	533	_		74.3				9	\$		¥.	ਵ-ਹ	ŝ		•	9.4		
Wr 1979	=	P) 1	2		887428	53	-		72.7			9.005-04											
	5 ;	r) (2		882458	<u> </u>			9.99	1.316-07	n		*	n	ន	11	걸	3	136.3	=		6	
NA 1979	TET.	٠ ،	2		882428	333	_		£.0				2	S	Š	œ.	#	ş		12	11.4 15		5.1
Nx 1979	E C	м 1	32		862458	E33	-		59.7		~	2.00€-04											
4/41 mm	######################################	,	~ ·		882458	ž	-		72.7		_	7.00E-05											
14/41 HI	5 5	· ·	7	00071	8C1783	2		\$.5 .5	20.0				^	7	₽	5	런	3		33	11	~	
1111	2	-	7	_	887.78	3	666		12.0				Š	~			dS-NS	٠		\$			

Moist, Liquid Plastic, UC + cont.(I) limit index (tsf) + 2 2 2 2 2 2 2 2 2 2 17.6 17.7 7.8 9.6 £ 8 22422 & # ± \$2325 E23 8 23 Percent Unit Ht. P200 (pcf) + ENGINEERING PROPERTIES Unified Soil Class. ಕೆ ೪ ೫ ಕೆ ಕೆ ಕೆ ದೆ ೫ ೫ ದೆ
 4

 4

 5

 4

 5

 5

 6

 6

 7

 8

 8

 8

 8

 8

 8

 8

 8

 8

 8

 8

 8

 8

 8

 8

 9

 8

 9

 8

 9

 9

 9

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10

 10
 </t 를 XS 부 부 각 Hatrix I Matrix & Matrix I + + sand silt clav + Bulk % (2.0 to (0.0625 to +)2.0mm 0.0625mm) ((0.002mm) ≌ ≅ 222222222 5 5 23 37 255697 **# 22** 33 42 83 34 82 计次件记录 路路 经转换 **\$** \$ GRAINSTIE PERCENTAGES Fld K Neth (ca/s) code Sacie Samie +
top bottom + Lab K Neth
(ft) (ft) + (cm/s) code + HYDRAULIC + CONDECTIVITY 2.00E-06 1.00E-07 2,105-08 33.5 53.5 8.5 43.5 68.5 28.5 58.5 58.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 50.5 13.5 3.5 18.5 22.0 22.0 26.0 36.0 36.0 22.5 22.0 26.0 51.0 999.3 1003.0 1003.0 1003.0 964.2 964.2 1010.5 1010.5 1010.5 1010.5 1010.5 1010.6 9772.2 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 997.6 Brna. 80. 882450 887450 887450 882150 882150 882450 88246 88246 882452 882452 882452 882452 882450 882452 882452 882510 882510 882501 882501 882456 882456 882456 882456 882456 882599 682511 882501 424554 424555 424555 424555 424557 424557 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 424558 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 42458 4245 (code) (code) No. unit Hat. + County u + (code) Year (1979 1979 1979 1979 1979 1979 1980 1982 1982 1982 1982 1979 1979 1979 1979 1979 1982 1979 1979 1979 1979 1979 + 1DENTITY

Appendix 3 - Hydrobedlosic and engincering data for walkoria county, east troy site

##
Sante top botton top b
カー・カンド はい はい はい はん
84.75

-

ĸ

SPT Moist. Liquid Plastic. UC + (M) coxt.(%) limit index (tsf) + 3 ÷ 36.4 3.4 13.2 23.4 Unified Bulk Dry Soil Percent Unit Mt. S F Class. P200 (pcf) (Hatrix Z Matrix Z Matrix 2 + ENGINEERING PROPERTIES 2-46 Calls 2-4 ***************** ರ ಧ ದ ದ ದ ದ ರ 5 5 5 \$ 55 55 + + + + san6 silt ciav + Bulk I (2.0 to (0.0525 to + 22.0ms 0.0625ms) ((0.002ms) Ξ 2 2 ĸ GRAINSIZE PERCENTAGES Fld K Neth (tn/s) code e Sample +
bottom + Lab K Meth (ft) + (cm/s) code + HYDRAUL IC + CONDUCTIVITY Apoendix 3 - HYROSEOLOGIC AND ENGINEERING BATA MALNORIH COLMIY. GRELDANUS SITE 4.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 1 Sauple S top b 965.0 972.0 968.0 959.0 968.0 Surt. Broq. Elev. no. (ft) 884324 884323 884313 884313 884313 884313 884313 884330 884305 884305 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 884313 88 42396 423913 423913 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423963 423 Litho-strat. unit Nat. Site r (code)(code) No. + (code) Year (+ IDENTIFY + County

+ SANNOIRE PERCENTAGES + ENGINEERING PRZPERTIES + MATRIX Z MATRIX Z + Matrix Z MATRIX Z + Matrix Z ≂ ಜ \approx \$ 7 あせるある。
なはるあることをあることをあることをあることをなる。
なるまた
はなる
は Fig K Meth + Bulk X 12.0 to (0.0625 to (cm/s) tode + 32.0m 0.0625ms) (cm/s) (cm/s) tode 2022220 Sastle Sastle +
top botton + Lab K Meth
(ft) (ft) + (ca/s) code + HYDRAULIC + COMDUCTIVITY Appendix 3 - KYDKOSECLOGIC AND ENGINEERING DATA MALMORIH COUNTY, SREIDANIS SITE £ 5. £. 87.05 - .05 Long. 884318 884319 884319 884339 884309 884306 884306 884306 884313 884399 884399 884399 884399 884399 423903 423904 423904 423904 423904 423904 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 423909 42 + County unit Hat. Site + (code) Year (code) (code) No. + 1DERIJIY

SPI Moist. Liquid Plastic. UC + (N) conl.(1) limit index (15f) + ς: 200252478254002 **** 2422422444444 3 38 2222222 22225555252 + Unified Bulk Dry + Soil Percent Unit Wt. + Class, P200 (pcf) + ENGINEERING PROPERTIES 888888888 STOCKING STOCK STO Appendix 3 - KTDKOBERLOBIC AND ENBINEERING DATA FOR NASHINGTON AND WARKESHA COUNTIES. INCLUES DATA FOR ONCEA HILLS WORTH AND SOUTH AND PREC EDING LANGILLS. **31110704** + Natrix I Natrix I Matrix I Matrix I sand silt tiay Fid K Meth + Bulk I (2.0 to (0.0625 to (0.0026) (0.00269) (0.00269) BRAINSIZE PERCENTAGES 8.64E-04 1.61E-04 1.64E-05 1.18E-05 5.73E-05 2.67E-04 2.65E-04 2.65E-04 2.65E-04 2.65E-04 2.65E-04 2.65E-04 2.65E-04 4.84E-05 7.07E-05 Heth code + BYDRAULIC + CONDUCTIVITY Saspie + bottos + Lab K (ft) + (cs/s) 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 ‡2.+ Sample S top | (ft) ≎.0 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 812.5 812.5 812.5 819.5 819.5 819.5 619.2 819.4 603.1 818.2 804.0 1 774.2 774.2 774.2 775.0 0 1 774.2 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775.0 0 1 775. Surf. Brng. Elev. no. (4t) 889445 B1 889441 Leng. 431138 431138 431138 431133 431133 431133 431133 431133 431134 431134 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 431147 43 unit Nat. Site r (code)(rode) No. **************** + County us + (code) Year (c 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 1983 1 19 + IDENTITY HOUSE STATES STA

2.4.0.4.

3

SPT Moist. Liquid Plastic, UC + (N) cont. (1) limit index (tsf) + 3:3 2 3.3 53 5.e <u>...</u> \simeq 2 ≆ 5 2 × 36 23 恕 K g 33 7.0 0.0.0.0 ~ 220222222 Fld K Meth + Bujk I (2.0 to (0.0625 to + 50il Percent that iff. (cs/5) code + 72.0se 0.0625ss) 0.002ss) ((0.062ss) + Elass, P200 (pcf) + ENGINEERING PROPERTIES 86288888888888888 3 x x 8 8 ರವರವರವರದರವರನ್ನು ಹಿಸಕ ಜನೆ ನಡೆಕರ ಜೈ ಕ್ಲೇಫ್ ಜಿ. ಸಿ. ಜಿ. ಜಿ. ಪ್ರತಿ ಪ್ರಕ್ರಿಸಿಗೆ ಜಿ. ಜಿ. ಜಿ. ROPENDIX 3 - HTDROBERLOSIC AND ENGINEERING DATA FOR WASHINGTON AND WALKESHA COUNTIES. INCLUDES DATA FOR DNESA HILLS NOATH AND SOUTH AND PREC 201NG LANDFILLS. ಶ ದ + GRAINSIZE PERCENTAGES
: Matrix I Matrix I + 1 23 z 8 29 2 S 2 ~ 2 2 4 2 5 NOON MOOO 3.90E-05 3.20E-05 3.30E-05 2.30E-05 1.40E-05 3.60E-04 1.50E-04 1.50E-04 1.50E-04 1.50E-04 2.10E-05 2.70E-05 e Sample +
bottom + Lab K Meth |
{ft} + (cnfs) code + EDNDACTIVITY + HYDRALIC Sample: 25.0 25.0 3.0 3.0 3.0 3.0 65.0 812.0 812.0 817.0 747.0 747.0 747.0 747.0 756.3 756.3 759.9 759.1 779.3 779.1 781.5 Proj. 988 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98110 98 880499 880499 880499 880499 880499 880499 880499 880439 880499 880499 680489 B80499 8804.99 880499 880499 880499 880499 880402 880402 880415 680408 889413 880413 880408 880408 880499 -000 880439 880459 880499 880499 850408 680409 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 43119 431 + strat. + County unit Mat. Site + (code) Year (code) Code) No. + IDENTITY Service Servic

* SFI Koist, Liquid Plantic, UC + (W) Cont. (X) list index (tef) + 25.5 253 ÷ 2 <u>~</u> ± 2 4 2 4 2 α Ľ. ᅔᅎ **# # # 32** 22 15.5 18.3 16.7 Unified Bulk Ory Soil Percent Unit Mt. S Class. P200 (pcf) (+ ENGINEERING PROPERTIES 2 2 2 \$C151488886546556885577588 Popendix 3 - Hydrosfoldbic and engineering data for washington and hankesha counties. Inclues data for onera hills wath and south and prec eding landfills. + Natrix I Matrix I Matrix I + Sand silt clay + Bulk I (2.0 to (0.0425 to + 22.08s 0.0625as) (0.002as) ድ ዮ 🕾 GRAINSIZE PERCENTAGES #eth code Fld K P Reth Code CONDUCTIVITY + BYDRAULIC Lab K (ce/s) Sample + bottom + (ft) : Seaple top Iff) 781.53 784.53 784.53 784.53 784.53 784.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 785.53 78 \$\frac{1}{2}\$ \frac{1}{2}\$ \fra 8 o Long. 880315 880315 880315 880315 880315 680416 880418 880430 880430 880433 880433 880433 880433 880433 880433 \$80315 \$80315 \$80408 \$80413 431140
431130
431130
431131
431131
431139
431139
431139
431139
431139
431139
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
431131
43 ij tithostrat,
+ County unit Mat, Site
+ (tode) Year (code) (code) No. \$ \text{\$\frac{1}{2} \text{\$\frac{1} \text{\$\frac{1}{2} \text{\$\frac{1} \text{\$\frac{1} \text{\$\frac{1}{2} \text{\$\frac{1}{2} \ 1982 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 11983 1 + IDENTITY FERT FROM THE FROM THE FERT FROM THE FERT FROM THE FERT FROM THE FROM THE FERT FROM THE FERT FROM THE FERT FROM THE FERT FROM THE FROM THE FROM THE FERT FROM THE FROM TH

SPI Maist. Liquid Plastic, UC : (M) cont.(1) livit index (tsf) + 222 2228164 22 24 2 222222 2 2 2 E 17.0 17.0 21.0 18.0 18.0 18.0 おもおおおおと ロロコロコロロコ なればない 2 Duified Bulk Dry Soil Percent Unit Mt. (\$ **2** \$ 2 2 3 ರದರದ ಕರದ ಕರದರರ ರಥಣೆ ನಡೆದ ವರದದರರವದ ವರ ಭರಣೆ ನಿಭರದ ಕರದದ ವರಕನ ನಿ Appendix 3 - Hydrobecologic and engineering data for hashington and wancesha counties. Includes data for oneba Hills north and sauth and prec eding landfills. 战器 计联 计 经统行经帐线 28 2 28222±83 40~40-870-8000000 Keth + HYDRRULIC + EDMBUCTIVITY 7.20E-08 1.60E-08 6.10E-08 1.80E-08 4.00E-08 1.00E-07 5.00E-08 3.005-07 7.00£-09 1.00£-08 5.00£-07 2.00£-07 9.00£-09 1.00E-05 2.00E-04 1.006-07 (s/s) (ca/s) Sample + bottom + t 22.00 22.00 23.00 24.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25 Sapie (ft) 800.4 800.4 812.5 812.5 812.5 773.6 775.7 775.7 775.7 805.2 805.2 765.7 761.1 764.6 764.6 764.6 765.0 759.2 759.2 Brng. no. 880.427 880.427 880.436 880.436 880.439 880.439 880.442 880.442 880.443 880.443 880.443 880.443 880.443 880.443 880.443 880.443 880.443 880.449 880.449 880.449 880.449 880.449 880.449 880.449 880.449 880.449 880.449 880.449 880.449 880.449 880.449 880.449 880.449 880.449 880.449 880.449 880.449 880.449 631154 631157 631157 631157 631157 631157 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 631137 63 Site 76. strat. unit Hat, S (rode)(rode) M + County u + (code) Year (Final Reservation of the servation of th

SPI Mcist. Liquid Plastic. UC + (N) cont.(1) limit index (tsf) + 2828282828282 + Unified Bulk Dry + Soil Percent Unit Wt. + Elass, P200 (pcf) + ENGINEERING PROPERTIES Hatrix I Hatrix I Hatrix I + Sand silt clay Fld K Meth + Bulk I (2.0 to (0.0625 to ice/s) code + 72.0es 0.0625es) 0.002es) ((0.002es) * BRAINSTZE PERCENTAGES 2.94E-06 6.89E-04 1.44E-06 1.94E-05 6.24E-05 6.24E-05 6.54E-05 1.64E-06 bottom + Lab K Meth (ft) + (ca/s) code CONDUCTIVITY 6.00E-07 1,00E-05 5,10E-03 4,00E-07 2,80E-08 4.506-05 B. 90E-08 2.80E-09 3.506-08 + HYDRAULIC Sample top (ft) 23.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50 751.0 759.0 759.4 763.4 763.4 760.7 772.0 772.0 757.2 757.2 757.2 757.2 757.2 757.2 757.2 757.2 757.2 757.2 757.2 749,4 749,4 743,8 743,6 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 743,5 880499 R1 880499 R1 880499 R1 880499 R1 880499 R1 880499 R1 880499 R2 880499 R2 880499 R5 88049 R5 88 Brng. 431199 431199 431199 431130 431130 431130 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 431199 : strat. + County unit Mat. Site + (code) Year (code) (code) No. *********************** 1976 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 1977 1 19 + IDENTITY HOUSE HOUSE

Appendix 3 - Nydrobelolosic and engineering data for Washington and Wancesah counties. Includes data for dikea Hills morth and south and paec soing Landfills.

			3	(#8#)										
			Plastic	ınder		۳,		Ξ			_			
			Liquid	sinit	=	EZ.		8		<u>\$</u>	2			
			SPI Moist. Liquid Plastic. UC	(W) cont. (3) Jinit inder itsf)	49 13 9									
				3	\$	61		8	E	ž	120		E	
ERTIES		Ę	t Unit Ht.		_	~	m	~	m	53	Z	99		
P806		Belk	Percent	P208		-0	^	-4		-				
+ ENGINEERING PROPERTIES		Unified	Soil	Class.	ង	*-		ದ	건	걸	루 다	작	4	
	+	*	+	*	٥	٥				=	9	2	٠.	
	Hatrix 1	Ç	_	((0,002a						_		_		
	Matrix 1	silt	0.0625 to	0.00288)	83	19				ន	=	33	22	
PERCENTA	Matrix & Matrix X	Send	12.0 to	062598)	4	×	=	87	23	8	•	\$	7	
- SRAINSIZE PERCENTAGES	_		Belk 1	ica/s) code + >2.6an 6.6625an) 6.002an) ((0,602au) +	41 42 58 0 5£ 37	-	=	≃	∞	-0	ĸ	=	£	
+ '		•	##	+ apq										-
			FIGK											705-04
1	<u>~</u>		計	goo					•=•					
+ HYDRAULIC	+ COMBUCTIVITY		£ab X	(\$/#3)	155 81 999.0 20,0 21.5		3,306-08		3.606-08					
+	•	Sanpie Sanpie +	bottos +	(ft) + (ca/s)	21.5	7.5	5:2	26.5	31.5	1:5	₹5	¥.	9.0	4
		apple	8	Ŧ	20.0	6.0	10.0	5.0	30.0	10.0	40.0	22.0	8.0	8
				#	9.66	971.0	971.0	975.0	946.0	940.0	940.0	905.0	673.9	7 198
		ŝ	Brng. El	± g	æ	B 2	B2	22	ž	22	\$2	2	SE	ŝ
			Æ,	Lose. no.	881155	881158	891158	881139	81128	81131	81131	8B1041	81037	01610
				ij	:							431755 8		
			Site	ۏ		35						#		
			±	ege)	\$	10	w٦	~	m	\$	m	m	~	۳
:	itho-	trat.	unit Kat.	· (code) Year (code) (code) No.	3	3	š	쭢	2	5	쓮	9	앞	9
	1	•	2	Year (1841	1881	1981	1981	1981	188	1981	1981	1881	1001
JPENTITY			· County	(rode)	4K 1981 UN 99 36	4	3	Š	3	≊	鞷	₹	Ş	3

-	b								+ +	+ HYDRALE IC + CONDUCTIVITY			* * +	ERAINSIIE PERCENTASES Matrix I Matr	CENTAGES t 1 Natrix	x I Matrix	ž,	H 51853 +	ENGINEERING PROPERTIES	ROPERTIE	μņ				+
- 7	÷					Surt.		Sample Sample					•	22.3	d sil	t Clay	2	t Lhif	fied Bul). (*				••
	+ #¥.				Ē	19. EI			ottos +	136 X	Neth	Fld K Netl	- + M	k I (2.0	to (0.062	S to		+ Soi	1 Per	ent Uni	1 H. S	SPF Raist, Liquid Plastic, UC	Liquid	lastic. U	••
	ode) (codi					÷.		(#)	ft) +	(C#/S)	code) (c)(s) cod	t + 72.	00.0 0.0625	um) 0.002	(6.0)	(385)	_	iss. P2	33 00	Ę	K) cont. (I)	lisit	index (tst) +	÷
,						!			10.0										ದ			22.0	B	28	
			•						40.0		in.	.41E-05							ដ						
ಕ			•		_				55.9		•	.51E-05	~					팣	*5						
ಕ			•	_	_	-			70.0		M	90-346	_						5						
ಹ									15.0		•	.398-04	_					15° C	25. 25.						
			_	_					26.1		**	- 04E-04						3	1,6X,59,0						
		-							25.55		•	196-04	~			-		F. 19	<u>ج</u>						
			•		_				40.0										ದ			19.0	82	22	
			Ī		_				6.3		-	.43E-06	_						ದ						
			•						45.5		~	106-04							35						
					_				71.3		••	338-05	-						35						
			-						25.0									ಧ	¥			=	=	-	
					~				6.0		^	.04E-05	_					ਹ, ਇ	1-18.5H						
			•						12.0										35	23					
			•		_				22.0									75	겆		30.0	13.0	23	s	
			•						31.0										ದ	_	38.0	9.0	8	Ξ	
									8.0										ᅺ				ដ	٠.	
			•		_				5.0										료	_	98.0	15.0	\$	Z	
				_	~.				25.0										ದ				61	Ĺ	
					_	_			15.0										ರ				2	7	
	(627 Kear (CO) 1982 CO 1982 CO	22 COC 33 COC 35	(code) (c	(code) (c	CCORP.) (code.) (code.	CCGG (CCGG) No. Lat. Long. CC 3 17 430248 880847 CC 34 37 430248 880847 CC 34 37 430248 880847 CC 3 17 430248 880847 CC 3 17 430248 880847 CC 3 17 430249 880858 CC 3 37 430249 880958 CC 3 37 430298 880908 CC 3 87 430298 880908 CC 3 87 430298 880908 CC 3 87 430298 880908	CCG04 (CCG4) No. LAI. Lang. no. ff C 3 37 430248 880847 MISA DCNB 3 37 430248 880847 MISA DCNB 3 37 430258 880847 MISA DCNB 34 37 430245 880849 MISA DC 34 37 430245 880847 MIZA DC 3 37 430249 880858 RIZA DC 3 37 430249 8	CC 5 7 74 24248 888947 MSA B40.6 CC 5 3 77 430248 888947 M19 SSA.0 CC 5 3 77 430248 888947 M19 SSA.0 CC 5 3 77 430245 888947 M21 833.4 CC 5 3 77 430245 888947 M21 833.4 CC 5 3 77 430245 888947 M21 833.4 CC 5 3 77 430249 8889528 M22 B58.7 UM 5 77 430249 8889528 M23 B58.7 CC 5 7 77 430249 8899528 M23 B58.7 CC 5 7 77 430249 8899528 M23 B58.7 CC 5 7 77 430249 8899528 M23 B59.7 CC 5 7 77 430249 8899528 M23 B50.2 CC 5 7 77 430249 8899528 M23 B50.2 CC 5 7 77 430249 8899598 M23 B70.6 CC 5 7 77 430249 8899599 M23 B70.6 CC 5 7 77 430249 88995999 M23 B70.6 CC 5 7 77 430249 8899599 M23 B70.6 CC 5 7 77 430249 8899998 M23 B70.6 CC 5 7 77 430249 8899998 M23 B70.6 CC 5 7 77 470249 8899998 M23 B70.6 CC 5 7 77 470249 88999998 M23 B70.6 CC 5 7 77 470249 M23 B70.6 CC 5 7 7 7 7 470249 M23 B70.6 CC 5 7 7 7 7 470249 M23 B70.6 CC 5 7 7 7 7 470249 M23 B70.6 CC 5 7 7 7 7 470249 M23 B70.6 CC 5 7 7 7 470249 M23 B70.6 CC 5 7 7 7 470249 M2	CCGG (CCGG) MG, Lat. Long, no. (11) (11) CC 3 37 430248 880847 W54 840.6 82.5 CC 3 37 430248 880847 W54 840.6 22.0 CC 3 37 430248 880847 W54 840.1 44.0 CC 34 37 430258 880842 W19 954.0 40.8 CC 34 37 430258 880847 W10 858.4 4.2 CC 35 37 430245 880847 W10 858.4 4.2 CC 3 37 430245 880847 W10 833.4 35.0 CC 3 37 430245 880847 W10 833.4 35.0 CC 3 37 430245 880847 W10 833.4 35.0 CC 3 37 430249 880858 W10 858.2 15.0 CC 3 37 430249 880858 W10 870.2 20.0 CC 3 37 430249 880858 W10 858.2 10.0 CC 3 37 430249 880858 W10 870.2 20.0 CC 3 37 430249 880958 W10 870.2 20.0 CC 3 37 430249 880958 W10 870.6 4.0	CCGG (CCGG) MG, Lat. Long, no. (11) (11) CC 3 37 430248 880847 W54 840.6 82.5 CC 3 37 430248 880847 W54 840.6 22.0 CC 3 37 430248 880847 W54 840.1 44.0 CC 34 37 430258 880842 W19 954.0 40.8 CC 34 37 430258 880847 W10 858.4 4.2 CC 35 37 430245 880847 W10 858.4 4.2 CC 3 37 430245 880847 W10 833.4 35.0 CC 3 37 430245 880847 W10 833.4 35.0 CC 3 37 430245 880847 W10 833.4 35.0 CC 3 37 430249 880858 W10 858.2 15.0 CC 3 37 430249 880858 W10 870.2 20.0 CC 3 37 430249 880858 W10 858.2 10.0 CC 3 37 430249 880858 W10 870.2 20.0 CC 3 37 430249 880958 W10 870.2 20.0 CC 3 37 430249 880958 W10 870.6 4.0	CC 5 17 430248 888647 W54 840.6 8.5 10.0 CC 5 17 430248 888647 W54 840.6 29.0 40.0 CC 8 17 430248 888647 W54 840.6 29.0 40.0 CC 8 17 430248 888647 W54 840.6 29.0 40.0 CC 8 17 430248 888647 W54 840.6 29.0 40.0 CC 84 17 430258 888647 W19 954.0 40.1 70.0 CC 84 17 430248 8886847 W19 954.0 40.1 70.0 CC 85 17 430248 8886847 W19 854.0 40.1 15.0 CC 85 17 430248 8886847 W19 833.4 4.2 26.1 CC 8 17 430248 8886847 W19 833.4 39.5 40.0 CC 8 17 430248 888684 W19 833.4 39.5 40.0 CC 8 17 430249 888685 W19 889.7 15.0 40.0 CC 8 17 430249 888685 W19 889.7 15.0 40.0 CC 8 17 430249 888685 W19 889.7 15.0 40.0 CC 8 17 430249 888685 W19 889.7 15.0 40.0 CC 8 17 430249 888685 W19 889.7 15.0 40.0 CC 8 17 430249 888685 W19 889.7 15.0 40.0 CC 8 17 430249 888681 W19 889.7 15.0 40.0 CC 8 17 430249 888681 W19 889.7 15.0 40.0 CC 8 17 430249 888681 W19 889.7 15.0 40.0 CC 8 17 430249 888681 W19 889.7 15.0 40.0 CC 8 17 430249 888681 W19 889.7 15.0 40.0 CC 8 17 430249 888681 W19 889.7 15.0 40.0 CC 8 17 430249 888681 W19 889.7 15.0 40.0 CC 8 17 430249 888981 W19 889.7 15.0 40.0 CC 8 17 430249 888981 W19 889.7 15.0 40.0 CC 8 17 430249 888981 W19 889.7 15.0 40.0 CC 8 17 430249 888981 W19 889.7 15.0 40.0 CC 8 17 430249 888981 W19 889.7 15.0 40.0 CC 8 17 430249 888981 W19 889.7 15.0 40.0 CC 8 17 430249 888981 W19 889.7 15.0 40.0 CC 8 17 430249 888981 W19 889.7 15.0 40.0 CC 8 17 430249 888981 W19 889.7 15.0 40.0 CC 8 17 430249 888981 W19 889.7 15.0 40.0 CC 8 17 430249 888981 W19 889.7 15.0 40.0 CC 8 17 430249 888981 W19 889.7 15.0 40.0 CC 8 17 430249 888981 W19 889.7 15.0 40.0 CC 8 17 430249 888981 W19 889.7 15.0 40.0 CC 8 17 430249 888981 W19 889.7 15.0 40.0 CC 8 17 430249 888981 W19 889.7 15.0 40.0 CC 8 17 430249 888988 W19 889.7 15.0 40.0 CC 8 17 430249 888988 W19 889.7 15.0 40.0 CC 8 17 430249 888988 W19 889.7 15.0 40.0 CC 8 17 430249 888988 W19 889.7 15.0 40.0 CC 8 17 430249 888988 W19 889.7 15.0 40.0 CC 8 17 430249 888988 W19 889.7 15.0 40.0 CC 8 17 430249 888988 W19 889.7 15.0 40.0 CC 8 17 430249 888988 W19 889.7 15.0 40.0 CC 8 17 430249 888988 W1	CC 3 37 430248 880847 W5A B40.6 8.5 10.0 CC 3 37 430248 880847 W5A B40.6 8.5 10.0 CC 3 37 430248 880847 W5A B40.6 20.0 40.0 CC 3 37 430248 880847 W5A B40.6 20.0 40.0 CC 3 37 430248 880847 W19 554.0 40.8 115.0 CC 34 37 430258 880847 W19 554.0 40.8 115.0 CC 34 37 430258 880847 W19 554.0 40.8 115.0 CC 35 37 43025 880847 W12 833.4 5.0 25.3 CC 3 37 43025 880847 W19 833.4 5.0 25.3 CC 3 37 43025 880847 W22 B75.8 13.0 CC 3 37 43024 880858 W73 835.7 15.0 40.0 CC 3 37 43024 880858 W73 838.7 15.5 25.0 CC 3 37 43024 880858 W73 838.7 15.0 40.0 CC 3 37 43024 880858 W73 83.7 15.0 40.0 CC 3 37 43024 880858 W73 83.7 15.0 40.0 CC 3 37 43024 880858 W73 83.7 15.0 40.0 CC 3 37 43024 880858 W73 83.7 15.0 5.0 CC 3 37 43024 880858 W73 83.7 15.0 5.0 CC 3 37 43024 880858 W73 83.7 15.0 5.0 CC 3 37 43024 880858 W73 83.7 15.0 5.0 CC 3 37 43024 880858 W73 83.7 15.0 5.0 CC 3 37 43024 880858 W73 83.7 15.0 5.0 CC 3 37 43024 880858 W73 83.7 15.0 5.0 CC 3 37 43024 880858 W73 83.7 15.0 5.0 CC 3 37 43024 880858 W73 83.7 15.0 5.0 CC 3 37 43024 880858 W73 83.7 15.0 5.0 CC 3 37 43024 880968 W73 W74.7 15.0	CC 3 37 430248 880847 W5A B40.6 8.5 10.0 CC 3 37 430248 880847 W5A B40.6 8.5 10.0 CC 3 37 430248 880847 W5A B40.6 20.0 40.0 CC 3 37 430248 880847 W5A B40.6 20.0 40.0 CC 3 37 430248 880847 W19 554.0 40.8 115.0 CC 34 37 430258 880847 W19 554.0 40.8 115.0 CC 34 37 430258 880847 W19 554.0 40.8 115.0 CC 35 37 43025 880847 W12 833.4 5.0 25.3 CC 3 37 43025 880847 W19 833.4 5.0 25.3 CC 3 37 43025 880847 W22 B75.8 13.0 CC 3 37 43024 880858 W73 835.7 15.0 40.0 CC 3 37 43024 880858 W73 838.7 15.5 25.0 CC 3 37 43024 880858 W73 838.7 15.0 40.0 CC 3 37 43024 880858 W73 83.7 15.0 40.0 CC 3 37 43024 880858 W73 83.7 15.0 40.0 CC 3 37 43024 880858 W73 83.7 15.0 40.0 CC 3 37 43024 880858 W73 83.7 15.0 5.0 CC 3 37 43024 880858 W73 83.7 15.0 5.0 CC 3 37 43024 880858 W73 83.7 15.0 5.0 CC 3 37 43024 880858 W73 83.7 15.0 5.0 CC 3 37 43024 880858 W73 83.7 15.0 5.0 CC 3 37 43024 880858 W73 83.7 15.0 5.0 CC 3 37 43024 880858 W73 83.7 15.0 5.0 CC 3 37 43024 880858 W73 83.7 15.0 5.0 CC 3 37 43024 880858 W73 83.7 15.0 5.0 CC 3 37 43024 880858 W73 83.7 15.0 5.0 CC 3 37 43024 880968 W73 W74.7 15.0	CCGP (Code) No. Likt. Ling. no. (ft) (ft) (ft) (ft) (ft) (ft) (ft x x x x x x x x x x x x x x x x x x x	CCGP (Code) No. Likt. Ling. no. (ft) (ft) (ft) (ft) (ft) (ft) (ft x x x x x x x x x x x x x x x x x x x	CCGP (Code) No. Likt. Ling. no. (ft) (ft) (ft) (ft) (ft) (ft) (ft x x x x x x x x x x x x x x x x x x x	CCGP (Code) No. Likt. Ling. no. (ft) (ft) (ft) (ft) (ft) (ft) (ft x x x x x x x x x x x x x x x x x x x	CCGP (Code) No. Likt. Ling. no. (ft) (ft) (ft) (ft) (ft) (ft) (ft x x x x x x x x x x x x x x x x x x x	(Code) (C	CC 3 74 (2014) Robert February Code (code) Code (code)	CC 3 74 420248 880847 MSA 64.0 6.31E-05 7 6.31E-06 7 6.31E-06 7 6.31E-06 7 6.31E-06 7 6.31E-06 7 6.31E-06 7 7 6.31E-06 7 7 6.31E-0	CC 3 74 A20248 880847 MS 64.6 8.5 10.0 5.41E-05 7 7.00E-06.2ms 0.00Zasi (0.00Zasi) (0.00Zasi) (0.00Zasi) 4.00Zasi 8.00Zasi 4.00Zasi 8.00Zasi 4.00Zasi 4.00Zasi <th< td=""><td>CC 3 74 (2014) Red (10.00244) Co.00244) Co.002440 Co.0024400 Co.002440 Co.002440 Co.0024</td><td> C C C C C C C C C C</td><td> C C C C C C C C C C</td></th<>	CC 3 74 (2014) Red (10.00244) Co.00244) Co.002440 Co.0024400 Co.002440 Co.002440 Co.0024	C C C C C C C C C C	C C C C C C C C C C

Coccol St. State Sta	E 5	+ IDENTITY	1	·J								7 7	HYDRAILE IC	2		+ 4	SRAINSIZE PERCENTASES	RCENTAS		* ***	+ ENGINEERING PROPERTIES	21KG PYGDF	ERTIES				
Mart			1	ئد د					à		epie S	+ +	11 COOK	=		. +		- 		clay	t Unifi⊵		Pr.y				
1813 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814 1814	Co G	ty e} Yea		Mat e) (rod				-					Lab K (ce/s)	Keth code	F1d K & (ca/s) R		Bulk X (2.6		.0625 to .0028#) (((0.00284)			Percent Unit Mt. P200 (prf)	SPT Hoist. (N) cont.(Z)	SPT Moist. Liquid (N) cont.(Z) limit	Liquid Plastic. UC limit index (ts	ic. BC x (tsf)
150 151 151 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152 152	-	861		_	3,5	3 4426	1 🗆	824		1	1	11.0					+	20	85	15				2		%	=
1981 KE 3 38 44320 88331 18 90.2 3.5 11.0 11.0 11.1 12.0 11.1 12.0 11.1 12.0 11.1 12.0 12.0 11.1 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12	_	90			7	107K	_	37	_			9					4	Ľ.	•	}	8			Ş		;	
	. =	8		, -		7077		2	_			-					= =	: 0	7	=	5 G			; ;		7	=
183 KR1 3 38 44240 885817 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184 184	- 3	-			5 6 5 6	1137		; ;	•			?					: •	8	7	2 ;	3 2			3	4	; ;	: :
1985 KGT 3 38 44250 BESSET 188 OH-1 10.0 1.00E-07 3 5 78 5 14 10.0 1.00E-07 3 18 1.00E-07	*	_			٠ •	•		7			2		1	•			• ;	8 7	류 :	7			.		7.07	ę :	= '
1883 KIN 3 38 44 CL 1883 KIN 3 38 44,620 68327 88 901, 8.52 14 CL 188 CL 1883 KIN 3 44,620 68327 88 901, 8.52 16.06 7 2 34 45 24 17 CL 1883 KIN 3 44,620 68327 89 901, 81,53 5.00E-07 3 77,2E-04 7 4 2 34 45 24 17 CL 18 18 18 47,620 68327 18 901, 81 18 901, 81 18 901, 81 901, 81 901, 91 901, 91 901, 901, 901, 901, 902 901, 902, 902 902, 902, 902, 902, 902, 902, 902, 902,	_				ห พ			ž			0.0		3.00-0	m			=	2	ņ	5 0	ω.		ėg.		12.0	ς,	2
1893 180 4 31 41240 86337 0444 944, 5 5 4 4 5 5 4 4 5 5	_			_	N N						5.0						m	æ	23	Ξ	5		_			ĸ	~
1883 KRT 3 38 44220 865822 810 81 8 5 5 100E-07 3 5 5 9 9 9 9 9 9 9 9	-	P 196		5	ಸ +							64,5			1.876-04	~					44	_					
1983 KEN 3 19 44220 BESSEZ BE	_	P 198		_	E P	3 4426		829	88		5,5		1.005-07				~	Ä	4	21	=	-			22.0	ន	2
1983 KEH 3 8 412630 885822 Bit 15.5 5.00E-07 3 4 25 31 51 17 DL 1983 KEH 3 38 44220 88522 Bit 16.5 5.5 6 28 31 51 17 DL 1983 KEH 3 38 44220 88522 Bit 16.5 5 6 28 50 20 22 DL 1983 KEH 3 38 44220 88522 Bit 16.5 2.00E-07 3 7.32E-64 7 5 5 20 DL 55-78 1983 KEH 3 38 44220 88522 Bit 16.0 5.5 2.00E-07 3 7.32E-64 7 5 5 2.00E-07 3 5 5 2.00E-07 3 4 3 3 4 3 4 3 4 3	_	195			3	8 4426		829			2.5						10	82	•	24	٠		•		16.0	2	=
1983 KKI 3 38 44520 685322 810 815 85 85 85 85 85 85 8	_	100			*	7777		424	_		ur ur		5.00E-07				۶,	F	.	2						74	•
1993 KEI 3 4 4 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20<					. F	4017											; ¬	. *	17	: 7			. 40		0.01	. 2	=
1981 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181 181				• .	, ,				2 2	٠							٠.,	: 8	3 5	; \$	2 6					; ;	: :
1983 KEG 99 38 442228 865327 B15 904.2 5.5 3.6 92.8 14.8 14.2 865327 B15 904.2 5.5 3.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8 14.2 94.8				., s	3 F	9744 8		č							10 716 6	,	0	97	ਨੇ	77			4		24.0	9	4
1993 KR1 99 38 44268 865829 B13 903.2 1.0 2.00E-07 3 5 52 346 13 5.5 1408 865829 B13 903.2 1.0 2.00E-07 3 5 52 346 13 5 52 346 13 5 52 1408 865829 B13 903.2 1.0 2.00E-07 3 13 644288 865829 B13 903.4 14.5 5.5 1408 865829 B13 903.4 14.5 14.5 14.0 14.5 14.5 14.5 14.5 14.5 14.5 14.5 14.5			# :	2 .	, ,	274									- X-	٠.	;							:			
1993 KEK1 37 38 442628 865822 B15 90.2 5.5 5.0 5.0 6-07 3 5 5 2 5 4 5 5 5 5 6 1 5 5 5 6 1 5 5 5 6 1 5 5 5 6 1 5 5 6 1 5 5 5 6 1 5 5 6 1 5 5 6 1 5 5 6 1 5 5 6 1 5 5 6 1 5 6 1 5 5 6 1 5 6 1 5 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5 6 1 5				2	- 5 - 5	9711						20.0	!	•			ሐ የ	:		. ;	'n		- ;	3			;
1983 KRI 3 38 442628 BS5628 B13 903.2 1.0 1983 KRI 3 38 442628 BS5628 B14 904.7 5.5 1983 KRI 3 38 442628 BS5622 B15 903.9 14.5 15.0 1983 KRI 3 38 442628 BS5822 B15 903.9 14.5 15.0 1983 KRI 3 38 442628 BS5822 B15 903.9 14.5 15.0 1983 KRI 3 38 442628 BS5827 B15 B59.9 15.5 1983 KRI 3 38 442628 BS5827 B15 B59.9 15.5 1983 KRI 3 38 442628 BS5827 B15	_			-	~	8 44Z¢					'n		2.00E-0	'n			-	5	8	2	sa.		29		0.22		2
1983 KEM 3 38 447268 858262 B15 949.7 5.5 B16 94 14.2 B18 95822 B15 949.7 B18 95822 B18 949.7 B18 95822 B18 949.7 B18 95822 B18 949.7 B18 949.	_		_	<u></u> ,	ri m	8 4426			-		<u>°</u>						1 73	8	22	==	٥		~		16.0	e	~
1983 KEK1 3.38 412226 BESSEZZ B15 94.12 1.5 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	_			- -	e E	25 25 8					5.5						Ħ	2	8	•	.		29 .	23			
1983 HD 4 33 44228 BESSOZ 815 91.4 1.5 1.0 4 31 52 17 CL 1983 KRI 3 44226 865837 81.6 89.6 5.5 5.00E-08 3 59 23 17 CL 1983 KRI 39 44226 865837 81.6 89.5 5.5 6.00E-08 3 59 23 17 CL 1983 KRI 39 44226 865837 81.9 90.1 10.2 CL 3 4426.0 1.0 5.0 1.0 6.00E-08 3 5 29 23 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 <t< td=""><td>_</td><td></td><td></td><td>=</td><td>es m</td><td>8 4426</td><td></td><td></td><td>_</td><td></td><td>5.5</td><td></td><td></td><td></td><td></td><td></td><td>~</td><td>₽</td><td>n</td><td>₹</td><td>J</td><td></td><td>99</td><td>-</td><td></td><td></td><td></td></t<>	_			=	es m	8 4426			_		5.5						~	₽	n	₹	J		99	-			
1983 KEK1 3 38 412A26 895837 816 890,9 5.5 2,00E-07 3 4 31 52 17 0.0. 1983 KEK1 3 38 442A26 895837 818 890,5 5.5 5.00E-08 3 5 5 5 5 5 6 1983 KEK1 3 38 442A26 895837 818 890,5 5.5 5 5 5 5 5 5 5 5	_			9	۳. ۳	8 4428			-			16.0					ន				·,		=	æ			
1983 KEK1 3 38 412626 895837 816 890-9 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.	_	P 19		٠,	₩ ₩	8 4426			_		5,5		2.00E-07	•			4	គ	23	:	<u>د</u>		90		3.0	%	=
1983 KEK1 99 38 44226 855.3 6.00E-08 3 59 23 19 SE 1983 KEK1 3 44226 88527 81.0 6.00E-08 3 6.00E-04 7 5 29 43 13 6.0 1983 KEK1 3 44226 88527 814 6.00E-08 3 6.00E-04 7 5 29 43 12 7 7 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12	_			~	5	18 442F		38			10.5						67	53	\$	22			2		14.0	ĸ	•
1983 KEK1 3 38 44226 B18529 B18 B99-5 5.5 6.00E-08 3 4.20E-04 7 5 5 5 5 6.00E-08 3 4.20E-04 7 5 5 5 5 5 5 6.00E-08 3 4.20E-04 7 5 5 5 5 5 5 5 5 5	_	25		7	۳ چ	9Z }+ 8.		5834			e.						м	ŝ	ĸ	≏ :	G,		55		21.0	23	=
1963 HI 4 38 41224 825827 914 4 58 4 50.00E-08 3 4 50E-07 7 5 5 5 4 5 5 5 5 5 5	_			=	m	32 4428		5829			5.5		5.005-01	m			0 0		:	=	Ų		×		15.0	8	=
1981 KEK1 3 M 472626 BESSAT B19 90.1.1 [0.5] 6.00E-08 3 45 75 47 27 CL 1983 KEK1 3 M 47261 BESSAT B20 903.1 [0.5] 2.00E-08 3 45 45 44 19 CL 1983 KEK1 3 M 47261 BESSAT B20 903.1 [0.5] 2.00E-08 3 5 35 44 19 CL 1983 KEK1 3 M 47261 BESSAT B20 903.1 [0.5] 80.0E-08 3 4.21E-04 7 5 35 44 20 CL 1983 KEK1 3 M 47261 BESSAT B20 ACA R 801.1 [0.5] 80.0E-08 3 4.21E-04 7 3 4.42E-05 59-58 1983 KEK1 3 M 47261 BESSAT BASA R 802.3 SA.2 SA.2 SA.2 SA.2 SA.2 SA.2 SA.2 SA.2	_			₽	**			829 04				9.69			1. 20£-01	^					"	۵.					
1963 KEK1 3 38 442626 B5824 B20 903.1 5.5 F. Conc08 3 F. Con				=	P)			2827			10.5		9-300 9	m 			so	8	*	23	_		2:			я	91
1983 KEK1 3 38 442624 BSSS24 BZS 9 933,1 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 1	_	IP 19		c	n			5824			5.5						-	8	=	5	-		25		18.0	ន	ŭ
1983 H0 4 38 442621 865824 823 894.9 10.5 98-5K 198-5K 198-5	_			5	17			1824			10.5		2,805-0	n			N)	ĸ	7	×	ω		92		13.0	2	2
1963 HD 4 38 447621 885824 BZ 31.0 SP-SH PS-SH SP-SH PS-SH PS-SH-SH-SH-SH-SH-SH-SH-SH-SH-SH-SH-SH-SH				9	*			5829			10.5						8	28	=	-0	S-S		55	8			
1983 KEKI 3 44 12621 8635537 FZ 87.11 B.5 B.00E-08 3 9 12 51 18 CL 1983 KKI 3 84 47221 885837 RZ 89.11 1.6 53.0 4.21E-04 7 9 12 51 18 CL 1983 KKI 3 44 42621 885827 RZ 89.11 1.6 53.0 4.21E-04 7 85.87E-9.59 9.58F-9.59 1983 KKI 3 44.2621 885829 RZ 3.5 4.00E-08 3.47E-04 7 3 43 4.5 5.8F-9-9.9 9.5 9.8F-9-9.9 9.8F-9-9.9 <t< td=""><td></td><td>4 19</td><td></td><td>æ</td><td>-</td><td></td><td></td><td>3824</td><td></td><td></td><td>8</td><td>31.0</td><td></td><td></td><td></td><td></td><td>ž</td><td></td><td></td><td></td><td>å</td><td></td><td>-</td><td>23</td><td></td><td></td><td></td></t<>		4 19		æ	-			3824			8	31.0					ž				å		-	23			
1983 KEKI 3 24 (262) 885837 876 891.1 16.5 8.00E-08 3 9 32 51 18 CL 1983 KEXI 3 44 (262) 885837 87.2 691.1 41.0 53.0 4.00E-08 3 4.20E-04 7 8.5H-5P.5P CL 1983 KEXI 3 8 (422) 8828.2 82.3 5.5 4.00E-08 3 43 23 CL 1983 KEXI 3 8 (422) 863824 83.0 899.9 5.5 4.00E-08 3 39 42 23 CL 1983 KEXI 3 8 (422) 863824 83.0 899.9 5.5 3 7 42 28 CL 1993 KEXI 3 4 (422) 883824 83.0 899.9 15.3 11 30 40 29 CL		91 91		. E	m	-		2837			5.5						'n	*	#	2	,		2	Ş	17.b	22	=
1983 HQ 4.38 44.28271 868537 0.08 8.00 4.21E-04 7 95-SN-59-59 87-SN-59-59 10.1 13.3 4.3 23 0.1 10.1 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 </td <td></td> <td></td> <td></td> <td>₹</td> <td></td> <td>-</td> <td></td> <td>5837</td> <td></td> <td></td> <td>10.5</td> <td></td> <td>B.00E-0</td> <td>m</td> <td></td> <td></td> <td>۰</td> <td>ä</td> <td>5</td> <td>#</td> <td>_</td> <td></td> <td>33</td> <td>19</td> <td>12.0</td> <td>32</td> <td><u>\$</u></td>				₹		-		5837			10.5		B.00E-0	m			۰	ä	5	#	_		33	19	12.0	32	<u>\$</u>
1963 KEK1 3 38 442621 865829 828 872.3 5.5 4,00E-08 3 i 33 43 23 CL 1963 KEK1 3 38 442621 868829 QLZ64 882.3 50.3 59.5 5.47E-04 7 3 5.4		£1 4±		2	*	-			_		41.6	53.0			4.21E-04	۲-					ŝ	g,					
1963 HD 4 38 442621 885829 QMZ6A 872.3 56.3 54.7E-04 7 5 5.47E-04 7 5 5.47E-04 7 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		HP 15		=				5829		852.3	5.5		4.00E-0	<u>س</u>				S	₹3	×	_	ببر	*		23.0	72	2
1983 KEK1 3 38 442821 885824 830 899,9 5.5 18 Ct. 1983 KEK1 3 38 442282 885824 830 899,9 15,5 28 Ct. 1983 KEK1 3 38 44221 830 899,9 15,5 28 Ct. 1983 KEK1 5 38 442821 830 899,9 15,5 28 Ct.		£ ₩		9	+	•					50,3	59.5			5.478-04	_					•	٠.					
1983 KEKI 3 38 442621 885824 850 899,9,16,5 Ct 1983 KEKI 5 38 442621 886824 830 899,9,15,5 Ct 1983 KEKI 5 38 442621 8868824 830 899,9,15,5 Ct 1983 KEKI 5 38 442621 830 899,9,15,5 Ct 1983 KEKI 5 442621 830 KEKI 5 4		帮 19		₽	w	_		5824			5.5						m	š	4	8	_		99		22.0	æ	=
1983 KEK! 3 38 442621 8368284 830 899.9 15.5				₽	ы Б	18 442¢		3824			5.0						~	ន	2	83	_		S		13.0	29	=
				;;	ю,	38 442		5824			5.5						=	ñ	\$	29	_		45	22			

+ FUDRAULC + GRAINSIZE PERCENTAGES + ENGINEERING PROFERIES + COMDUCITUITY + Ratrix Z Matrix Z + Unified Bulk + Samel Samele Bank + Bulk (2.4 + Unified Bulk + Bulk | Forthormal Matrix ឧឧឧ けたねれはななねむ 3775255 3 2 四世四日第二日 20 日本日日 20 日本日日 20 日本日日 20 日本日 20 日日 20 24825-64 2022382 Appendix 3 - HYDROSEOLOGIC AND ENGINEERING DATA FOR WALPACA COUNTY, TOWN OF ROYALTON SITE 3.5 51.0 51.0 50.0 50.0 50.0 51.0 31.0 31.0 811.7 2.0 811.7 14.5 801.7 39.4 803.8 4.5 801.4 9.5 801.4 19.5 791.8 4.5 791.8 4.5 788.6 19.5 Surf. Brog. Elev. Lat. Long. no. (#1) 885.655 885.655 885.655 885.655 885.655 885.655 885.655 442034 442034 442034 442029 442023 442013 442013 + County unit Mat. Site + (code) Year (code) (code) No. 5 x x 5 x 50 MP 1982 P 1982 MP 1982

+ +	+ +	•	}																																					
	S	3																																						
	3	ug ex	22	=		2	7	•		8	7		2			2	3								Ξ	: ~	ļi.	*	23 ;	2 3	₹ 5	2 2	: :	1 25	8	27	,		8	=
	iouid Pl	init	\$	38		9	3 😄	:		우 :	2		ŝ			ž	:								2	2		2	<u>ن</u> د	;	¥ :	3 8	2 2	2 23	=	: 8			5	92
	Maist, Liouid Plastic, UC	(#) cont.(I) linit index (tsf) +																																						
	æ		00	~ ;	3 .	•	=			æ			2	n	3	= =	:	25	≅						α	, Z	125	ž		•	~ =	2 -	` =	: 2	R	:		-	æ	~ :
TIES	Bulk Ory Perceat Unit Wt.	(\$36)																																						
34084 9I	Bult Percest	8	8	S. 1	3	Ě	*	=	1	* 3	2	66		=	7	\$ 50	8	~ :	2 2	* \$	# 1	\$ 5	. &	∓ :	3 \$: 22	\$	22	e 8	2 8	2 2	49	6	. 6	47	\$	43			:
+ ENGINEERING PROPERTIES +	Unified Soii	Class.	ದ	료 (% z	3 2	ದ	25	₹ :	ಧ ಕ	5	펄		3 2	3 =	<u> </u>	5	ದ :	5 2	5 3	四	3 2	ಕ	3 5 2		-39 -39	55	S-28	3	5 2	ತ ಕ	3 6	ಕರ	; 3	ದ	3	3	بر بر	5	٦. ٣.
	+ +	+								• •		_				-												_	~ .		2 4					~				
Katrix I		0.002es) ((0.002es)	99	ñ	7	ō	~		٠	\$ 2	3	23				ŝ	•								^	: 13		= 1	2 5	~ .	~ 0	ni.	-3	i in	55	-0	~			
SES Satrix Z	silt (0.0625 to	0.002ex)	Z	ŝ	٤	3	23		1	R #	8	59				e	i								82	8		£ :	8 2	3 7	9 5	2	2	: 29	8	æ	11			
E PERCENTAGES Matrix I Natrix I	sand (2.0 to (2	· 0 :	ę -	-	7	8	٠	- -	•	+		82	9	3 ~	#	Ξ.	. r	• ·-·	~	>-	~	2	ñ -	器		ភ	٠.		₩ €	•	-		~		'			;
SRAINSIZE PERCENTAGES Hatrix X Nati	+ + Buls 1 (2	+ >2.0ss 0.0625ma)	2	φ.		•	•	33	٠	~ ~	•	0		•	•	٠ ~	22	٠.	> <	۰۰	٠.	- 0	۰	2 2	2	9	2	F '	7.	- <	>	>	۰	. 🗢	-	0	-			÷
• •																																								
	FId K Meth	(ca/s) code																																						
	Ke th	code				-			m •	~ ~				۳	•														e-	3						m	*7	P**)		
HYDRAUL IC Conductivity		(ca/s)				1.60E-08			1.00E-08	005-0	3.006-08	2.00E-04		2 655.67	4.00E-V													444	2. WE 48	60-30A-7						3,005-08	1.006-08	8.00E-08		
77	Sample + bottom +	÷				12.5		2	21.8	17.6	0.04	55.0		4 7	;									50.5	10.0	36.0	41.0	0.04	2.5	2.15						17.8	32.8	45.5		
	Sauch top		9.0	÷ ÷	2 2	9	20.0	8.5	29.0		9	53.0	20.	9 8	200	32.0	55.0	2.5	2.0	17.0	2 2	2.5	35.0	88	0.0	33.0	0.0	• • • •	2 2	2 2	2 5	30.0	15.0	39.0	25.0	15.0	20 0	9	9 4	2. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4.
		į		2,197			763.0	762.3	797.5	76.2				97.6				0.197		9.192	9.197			8.057			261.5	6.0		A 170	9	752.0	762.7	760.0	759.9	23.9	59.9	29.9	e .	2
	Surt. Brng. Elev.	39. 4ft)	128					33 a				•		2 2			•	298				362		22 2				2 2	2 4						328	F268	P26B	288 888	179	5 2
	<u>ئە</u>					_		_	-					-	_									S 25													_	883309 P		
		Ė	£ :	ž .							~	88	ώ.	3 2	3																									
		٥	13 883315												ತ	ន	3					2 2	8	440500	ş	ş	10201	3 5	1000	8	. 7	לט ו	-		W				90501	11001
-		Lat. Long.	440513 883315					440517 86		440523 88				440508	41050	440502	440204	440511	\$	440511	\$ 3	₹	=		_	~		•	- =	=	*1050	440504	440508	440599	410508	4	440508	₹:		_
	Site	No. Lat. Lon				440513	440517	440517	(1001)	440523		440523		440508	40504		40 440504				9			 -														¥ ;	• • • •	2 5
-	Mat. Site	No. Lat. Lon			440513	440513	440517	440517	(1001)	440523	440523	440523	440264	440508								2																	, r	3 5
Litho-	straf. unit Mat. Site	(tode)(tode) No. Lat, Lon		5 40 440515	3 40 446513	440513	3 40 440517	440517	3 40 446517	KEL 3 40 440523	KE \$ 40 440523	UN 3 40 440523	KEK! 3 40 440364	KEk) 3 40 440568	\$ 45 45	XE \$ 40	2 2 2	KERI 3 40	KERI 2 49	KEk1 3 40	KELL 3 40	KE11 3 40	KE 513 40	2	KE11 3 40	\$		2 5	35 40	9	9	9	9 0	9	9 : 2 :	9 n	2 : E :		2 ¥	2 5
+ IDENTITY + Litho-	straf. unit Mat. Site	No. Lat. Lon	3 40 440513	180 PA 04 PA 0513	KEN: 3 40 440513	KEN 3 40 440513	KE11 3 40 440517	UK 3 40 440517	3 40 446517	KEL 3 40 440523	5 40 440523	UN 3 40 440523	KEK! 3 40 440364	KEk) 3 40 440568	\$ 45 45	XE \$ 40	2 2 2	KERI 3 40	KERI 2 49	KEk1 3 40	KELL 3 40	KE11 3 40	KE 513 40	우 후	KE11 3 40	24	우 \$ ~ F	4 C 40	22 TE	9	KER1 3	KER1 5 40	KEk1 3 40	9	XEII 3 40	9 n	KEH I 40	<u></u>	2 13	

+ +	+ + +	1																																					
	35 E																																						
	SPT Maist, Liquid Plastic, UC (M) cont,(X) limit index (tsf)	=:	ξ.	Ξ	: #								2	2																									
	iquid P init	\$:	2	24	\$								9	=																									
	18																																						
	fais cont.																																						
				=	: ≌					2	:			• 8	3 8	1 5	: =	53																					
<u>s</u>	Bulk Bry Percent Unit Mt. P200 (pcf)																																						
OPERT:	** ** **			6	*	8		3 8	\$ 8	5 8	: 23		;	: :	2 =	=	*	23																					
£																						支										¥					ಕ		
+ ENGINEERING PROPERTIES	Unified Soil Class.	ರ	3 5	ೆ ದ	ದ	2	<u>~</u>	3	5 2	, E			;	명 2	5 7	8	ರ	\$	සි දි ප් ද	5 2	do 1.5	CHEM. CLYCH	sel t	3 23	2	ರ :	e c	1 23	호	ದ	2	보 보 다	3 2	\$ ±	1	20.00	ព,ជអា,ជ	5.	ದ
+ +	* * *																					ä										T				ದ	ದ		
Matrix I	silt clav (0.0625 to 0.002mm) ((0.002mm)			ន	8								;	, ·	• •	•																							
				\$	4								:	: 5	3 15	;																							
raees Natrio																																							
SRAINSIZE PERCENTAGES Matrix X Natrix X	+ sulk I (2.0 to + Sulk I (2.0 to + >2.0ss 0.0625ss)				M	Ξ	= :	2 2	2 2	; ~	×		•	7 ×	: 5	8	-	72																					
23SK2	0 2 0 8 0			0		۰	۰.	o <	- 0		25		•	> <	, -	79	•	0																					
\$ * +																																							
	Heth code																		-	, 1~	~	_	~ ~		~ .	۲,		. ~	~ ·	٠.	۲.		_ ~			-	٠.	٠.	~
	Fld K Heth (ca/s) code																		5.875-07	525 05	2 02F-04	1. BBE -07	2,286-04	7.538-05	29E-03	2.89E-06	0.00	.67E-06	095-05	. 695-07	7.5	5. BOE -05	186-05	50 30	355-05	3.556-06	225.4	. 01E-04	2, 17E-07
<u>~</u>	Meth code	m r	, m									m							vi -	-	7	*	4	÷ p~		ci i	· -	٠.	*	-	- '	ne	Ψ.	• ~	-	m	۰,	·- , (2
U.IC CTIVES		7.006-09	7.005-08	:								3.00E-08																											
+ HYDRAULIC + CONDUCTIVITY	Lab K (ca/s)	2.2	8 8									8																											
* +	Sample Sample + top Sattom + Lab K (ft) (ft) : (cw/s)	12.5	55.6							55.0		28.5							2.5	9.0	£3.0	9.0	9.6	33.0	20.0	6.4	2 0	8.0	27.0	20.3	20.5	e e	2,8	15.0	0.03	20.0	÷.	9.0	3.6
	Sapie top (ft)	0.0	3.0	25.0	8	2.0	9.6	2 ° 4	2 0	31.5	20.0	26.5	9.9	2 5	8	55.0	45.0	22.0	9 :	2	37.0	5.2	53.5	29.0	9:	7.0	9.0	2	23.5	9	2.0	7 0	2	8,8	55.4	7.0	37.6	: :	?
		762.4						0.14					764.6						7.6				8,8			25.3											761.4		
	E E																								-							- •						•	-
	Brns.	P31	_	· _				3 3			_		2 2 2 2				_			₹	_		2 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8		_	45 S	-	•			7 DM25A					O	5 P358		3
	Ę	883259	88325	88325	88330	881325	88325	5000	89325	98330	883309	B8330	883307	200	88330	88330	88330	88330	88323	88323	883239	88331	88331	88325	89325	883256	983369	88323	88323	8822	05589	162 BK	882288	88325	883258	983215	88321	700	88555
	# 1	440513	110513	140513	140513	1921	11007	11001	146511	10508	140515	440520	110320	660520	110520	440520	440520	440520	140523	2020	140500	440500	440500	440500	10500	40204	110504	440508	440508	8050	90004	16.51	440513	440513	440513	440513	440513	21604	100
	Site No.	2 9	: =	2		-		2 2	2 9	: 2	2	?:	2 2	2 9	: 2					: 2			2 2			\$ \$	· ·				2 :				9	\$	÷	· } :	•
	_	m =	'n	**	4 0 I	5	<u>ب</u>	, r	, v	۶.	m	m	· •• •	; -	-	-	10	+ 1	~ r		21		m m	m	ဌ	m r	3 PY	*	m	, رم	- J		, m	177	S	m	v =		-
Litho-	strat. unit Mat. (code)(code)	23 5	3	5	썾	₩ !	# 5	5 Z	<u> </u>	H	3		- -		3	⋽	3	5	# E	3	3	Œ.		*	3	S =	i (2	KEN	KERN	3	7 KE	, re	KE	쎂	썦		¥ 3	5 5	ž
=		:		=	*	£ 5	1985	6 8	2 58 2 58 2 58	8			2 5 2 5 3 5		1982	1985			13 SE61				28 28 28 28			## 7861 1861				1861	=	-					S 55		
_	₩.	맞으	: =	~	* '								,, ,				•	ب	~ •		0	-	, ,	G,	5		- 0-	.,~	5	- 0						.,-	07	. 9	÷
+ IDENTITY	+ + County + (code) Year	WI 1985						_	-		_					-					_				_				_				_	_					_

+ CDMDCTIVITY + Natrx I Marrx I Matrx I + sand silt clay + Unified Bulk Dry + top bottos + Lab K Meth Fid K Meth + Bulk I (2.0 to (0.0425 to + Soil Percent Unit Wt. SP7 Moist. Liquid Plastic. UC + (ft) (ft) + (se/s) code (ca/s) code + 72.0as 0.0625es) (0.002es) + Class. P200 (pci) (W) cont. (2) Nisit index (1sf) + + ENSINEERING PROPERTIES 로 급 당 다 보 급 급 급 급 급 급 급 급 당 다 된 당 * SRAINSIZE PERCENTAGES 1,41E-05 1,41E-07 1,98E-06 1,58E-06 1,58E-06 1,58E-06 1,58E-06 1,58E-06 1,68E-06 1,88E-06 1,88E-+ HYDRAUR IC + CONDUCTIVITY 752.5 Sert. 882528 0438 883258 0438 883252 04428 883252 P428 883252 P420 883354 04438 883354 04438 883327 04448 Srng. E Long. no. ta. 440517 440517 440523 440523 440523 440523 440524 440524 440524 440524 440504 440504 + Strat. + County woit Mat. Site + (code) Year (code) Koo. + IDENTITY

Appeadix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR NINNEBAGO COUNTY - DARTLETT STIE

SPT Moist, Liquid Plastic, UC + IN) cont.(I) limit index (tsf) + + Unified Bulk Dry + Soil Percent Unit Wt. + Class, P200 (ocf) Harrix X Natrix Matrix X + ENSINGERING PROPERTIES + sand silt tlay + Bult 1 (2.0 to (0.0525 to + 22.0ss 0.0625ss) 0.002ss) (0.002ss) + SRAINSIZE PERCENTAGES Fld K Neth ~ **.** 1.70E-05 2.10E-06 Lab K Neth (ca/s) code * KYDRALL IC * CONDECTIVITY Samoie + bottom + 1 (ft) + (Samit top (ft) 777.33 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 777.34 77 883355 B5-1 88349 B5-2 88349 B5-4 88349 B5-4 88349 B5-4 88349 B5-4 88349 B5-7 88349 B5-8 88349 B5-1 88349 B5-1 88349 B5-1 88349 B5-1 88349 B5-1 88349 B5-15 883499 B6-4 883499 B6-5 883499 B6-7 883499 B6-7 883499 B6-8 883499 B6-9 883199 B6-11 883153 BC-1 883153 BC-1 883153 BC-2 883159 BC-2 883159 BC-3 Вга<u>ф.</u> 20. 883499 470356 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 47 ij + County unit Hat, Site + (code) Year (code) (code) No.

Adpendix 3 - Hydrobeologic and embineering data for Winnebaso County, Winnebaso County Landfill

3

8

5

+ Unified Bulk Drv + Soil Percent Unit Mt. SPJ Moist, Liquid Plastic, UC : + Class, P200 (pcf) (N) cont.(1) limit index (tsi) + 9.6 Ξ ÷. 5.8 125.8 125.8 14.7 112.9 + ENSINEERING PROPERTIES + Matrix Z Matrix Z Matrix X + sand silt tiav + Fld K Meth + Bulk Z (2.0 to (0.0625 to + (cs/s) tode +)2.0m 0.062ms) 0.002ms) ((0.002ms) + + GRAINSIZE PERCENTAGES 取って非がすり込 80 22 2 2 2 2 8 **4444664444** 4.40E-07 1.40E-07 3.80E-07 7.40E-06 1.50E-06 3,206-04 6.40E-06 2.90E-05 1,606-04 1,906-05 2,306-03 1,806-07 3,106-07 2.90E-07 3.50E-07 6.50E-07 3,80E-06 3,60E-05 Sable Stable +
top bottom + Lab X Meth
(it) (it) + (tm/s) code + HYDRAULIC + CONDUCTIVITY 2.40F-04 1.10E-08 6.105-07 2,305-04 22.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 10.0 785.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 770.7 Sert. 883401 P-C-6
883407 P-C-7
883407 P-C-7
883380 P-C-8
883380 P-C-8
883380 P-C-8
883380 P-C-8
883380 P-C-9
883380 P-C-9
883407 P-C-10
883407 P-C-863409 9C-17
863401 P22
863341 P29
863334 P20
863334 P20
863335 P21
863335 P21
863335 P22
863335 P23
863337 P23
863337 P23
863331 P24
863341 P2 18. 10. 40037 40037 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 40035 + Ecunty unit Nat. Site + (code) Year (code) (code) No.

Apoendix 3 - Hydroerologic and ensimering data for Hinneraso Colaty, Hinneraso Colaty Landfill

*T Koist. Liquid Plastic. UC + N) cont. (E) ligit index (155) + % **≘** + sand silt ciav + United Bulk Drv fid K Neth + Bulk I (2.0 to (0.0625 to + Soil Percent Unit Ht. fcs/s) code + 72.0ss 0.0625ss) 0.002ss) ((0.002es) + Elass, P200 (pcf) GRAINSIER PERCENTAGES + ENGINEERING PROPERTIES
Addrix X Natrix X +
sand silt ciav + Unitics Bulk Day 23 Hキリのパロ・コリドリドスドののいとのいとのではないによりのとれたれてないともになってもに Addendix 3 - Hydrogellosic and ensineering data for kinnebago county. Hinnebago county landfill Reth Code + HYDRAULIC + CONDUCTIVITY Sample Sample +
top bottom + Lab K R
(ft) (ft) + (cm/s) c 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 1941.7 19 Sert, 51 (*) 883.49 80.86 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 883.49 81.26 833.49 81.26 833.40 81.26 833.40 81.26 833.40 81.26 833.40 81.26 833.40 81.26 833.40 81.26 833.40 81.26 833.40 81.26 833.40 81.26 833.40 81.26 833.40 81.26 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833.40 833. Brng. 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 Litho-strak, unit Mat. S (code)(code) M + County u + (rode) Year (

~ ≃

ដ្ឋ

2 22

SPT Moist, Liquid Plastic, UC + (N) cont.(2) limit index (tsf) + 89 27.5 13.9 9.0 8.5 16.1 13.8 5.9 + Unified Bulk Bry + Soil Percent Unit Wt. + Elass, P200 (pcf) 162.2 150.6 95.2 132.8 130.6 15.9 119.8 123.0 + RAINERING PROPERTIES

+ Sand Silt Clav + United Bulk Dry
+ Bulk I (20 to (0.0525 to + 55i Percent Unit Bry
+ 72.048 0.05280 0.00248) (0.00248) + Class. Proc 2333 **网络公司中央公司中央** ವವಹ್ಹಹಿ ವರ Fld K Neth (ca/s) code 6. 30E-05 8. 40E-05 4.005-07 Satole Samore +
top bottom + Lab X Meth
(ft) (ft) + (cm/s) code + HYDRAULIC + CONDUCTIVITY 1.30E-05 1.30E-07 9.80E-05 3.90E-05 9.70E-05 1.80E-04 760.5
761.9
761.9
761.9
771.0
770.7
770.1
770.1
770.1
770.2
770.2
770.1
770.2
770.2
770.2
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3
770.3 762.9 766.2 765.1 765.2 765.2 767.6 767.5 767.5 767.5 767.5 767.5 767.5 767.5 767.5 767.5 767.5 767.5 767.5 767.5 767.5 ri di di 883499 81.6 883499 82.4 883499 82.4 883499 82.4 883499 82.6 883499 83.2 883499 83.2 883499 83.2 883499 83.2 883499 83.4 883499 83.4 883499 84.4 883499 84.4 883499 84.4 883499 85.5 883499 85.5 883499 85.5 883499 85.5 883499 85.5 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883499 86.6 883498 86.6 883499 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88349 86.6 88340 86.6 88340 86.6 88340 86.6 88340 86.6 88340 86.6 88340 86.6 88340 86.6 88340 86.6 88340 86.6 88340 86.6 88340 86.6 88340 86.6 88340 86.6 88340 86.6 88340 86.6 88340 86.6 88340 86.6 88340 86.6 88340 86.6 88340 86.6 88 Brno. Ro. 883499 883499 883499 883499 883499 883499 883499 1000 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 470339 + County unit Nat. Site + (code) Year (code) (code) No.

Apoendia 3 - Hydrogeoldsic and ensineering dria for Winnebago County. Winnebago county Landfill

SPT Moist, Liquid Plastic. UC + (H) cont.(1) limit index (1sf) + 報りには 52.5 6.7 22.2 + Unified Bulk Drv + Soil Percent Unit Mt. + Class. P200 (ptf) 135.5 117.5 133.0 + ENGINEERING PROPERTIES 22222222222 8 ស % ជ % ជ ជ ជ % % ជ % Hatrix I Hatrix I Batrix I + + sand silt clav + Bulk % (2.0 to (0.0625 to +)2.0ss 0.0625ss) (0.002ss) ((0.002ss) 28 23 + GRAINSIZE PERCENTABES Fld K Neth (ca/s) code 2.60E-07 4.30E-05 3.60E-07 2.70E-06 2.10E-06 Appendix 3 - HYDROGEOLOSIC AND ENGINEERING DATA FOR WINNERAGO COUNTY, WINNERAGO COUNTY LANDFILL Sample Sample +
top bottom + Lab K Meth
(ft) (ft) + (cm/s) code + HYDRAULIC + CONDUCTIVITY 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25.00 25 761.8 769.7 769.7 769.7 782.8 782.8 777.2 777.2 777.2 777.2 777.2 777.2 777.8 775.8 775.8 775.8 Surf. Brng, Elev. No. (ft) 883346 P-4-60
883346 P-4-60
883346 P-4-60
883344 P-5C
883337 P-4C
883337 P-4C
883337 P-4C
883337 P-6C
883344 P-6C
883344 P-6C
883344 P-6C
883344 P-6C
883344 P-6C
883344 P-10C
883344 P-10C
883349 P-10C
883497 II
883499 II 470345 470354 470338 470338 470338 470338 470339 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 470331 47 + County unit Nat. Site + (code) Year (code) (code) No. + IDENTITY

SPT Hoist, liquid Plastic, UC + (M) cont.(X) limit index (tsf) + ೩ 2 = 2 = Ξ _ * ≂ R 2 13.8 16.6 15.4 12.0 21.2 29.5 17.3 5.9 16,2 Unified Bulk Dry Soil Percent Unit Mt. St Class. P200 (pcf) (47.4 3 25.6 $\begin{array}{c} \mathbf{c} & \mathbf{x} & \mathbf{c} & \mathbf{$ Fld K Neth (ca/6) code Sample Sample +
top bottom + tab K Meth
(ft) (ft) + (ce/s) code + HYDRAULIC + CONDUCTIVITY 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 709.3 Rrag. 875106 875106 875106 875106 875106 875106 875106 875106 875106 875106 875106 875106 875005 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 875055 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 87505 8750 875041 875041 875041 875041 875041 875041 875041 875041 875041 875041 875041 875041 875051 875051 875052 875052 875052 45214 45214 45214 45214 45214 45214 45214 45214 45214 45214 45214 45214 45214 45214 45214 45214 45214 3 + County unit Hat. Site + (code) Year (code) (code) No. **858588388**888888888888888888888888888

Aporndix 3 - KTBROCECLOSIC AND ENGINEERING DATA FOR MILHAUNEE COUNIT - BENDER PARK

sand sili clay + Unified Bulk Dry + Bult Z 12.0 to GAZE to + 5011 Percent Unit Wt. SPT Koist, Liquid + 32.0 as G.65.2 as 0.002as) ((G.002as) + Elass. P200 (pri) (M) ronf.(I) lisit	1	2	Ct. 87.2 35 13.0	181			28	# ⁴ 대 대	_			901			15 18.3		27 29 39 4		3 22	15 41.7	15 23.9	51 50	20.0	19.0	16.0				25.0	15.0	35.0	
+ Unified Bulk Dry + Soil Percent Unit Bt. + Class. P200 (pcf)				}											2 52	. 22	2 2	1 12	ii ƙ	5 23	53 5	2										
+ Soil + Soil Class.	1	ರಃ	Ct. 87.2		s i z	ತ ಪ	ದ :	ත් ස	ಕ ಪ	בר/שר	ಪ ೭	ಕ ದ	ı 																			
+ Soil + Soil Class.	Q. 81.	ರಣ	ਲ ਹ		ed Z	ತ ಪ	ದ :	ස් ස	ಕ ಕ	\$1.78L	ವ ೭	ಚ ದ																				
+ + +	A	ರಣ	ಶ ಚ	1 2 1	ed Z	ਤ ਤ	ದ :	ದ ದ	ಕ ಪ	Z /3	ರ 2	ಕರ	<i>i</i> =																			
sand silt clay 0.0 to (0.0625 to 0.055ml 0.002ml ((0.002ml)	, h												,	ದ 8	ਕ	ದ	ಕ ರ	ಕರ	ਰ ਟ	ਰ ਫ	5 8	더 2	ជ	ರ	부 다	로	, ,		: :	ದ ಸ	ರ ದ	
sand silt ?.O to (0.0625 to 625ma) 0.002ma) ((0																																
sand 1.0 to (0 3625mm) (1																	٠															
Bulk 2																																
bottos (ft)	36.5	£ 5.5	SI.5	3, 2	3	71.5	× 5.5	86.5	2.5	8.5	106.5	111.5	2	c =	16.5	22.5	31.5	36.5	‡ ‡	51.5	25.5 2.5	2.0	÷	e e	: :	15.5 22.0	27.0	, 33 9, 53 9, 60 9, 60	2.0	- v	8	
± 6 5	35.0	÷ 5	80.0	8.8	65.0	9.	K 8	3 23	96.0	\$ \$	92.0	10.0	0.0	ų 5	5.0	8. 8 8. 8	9	35.0	45.0	8	S 5	3	3.5	, ,	9.0	20.0 20.0 20.0	23.0	s, s;	5:	, k	?	\$
	689.2	689.2	689.2	689.2	689.2	689.2	689.2	189.7	89.2	689.2	689.2	689.2	989	686.	\$86	686.4	68¢.	486.4	686.4	4.86.4	486.4	χ.	695.0	6.55 6.55 6.55 6.55 6.55 6.55 6.55 6.55	695.0	695.0 695.0	695.0	635.6	687.0	0.789	687.0	V 107
ė ė	1	I	# #	7 7 8 8	, Q	Į.	Z 2	Į.	7	7 2	7 2 3	7	۲ هم	2 25 24 25 24 25	7	주 등 소 시	. S	5- 4- 8- 8-	i i	·冷·	4	I	I	<u>.</u>	: I	<u> </u>	I.	: Z	25	2 2	2	
Fore.	75057	75057	13057	75057	75057	175057	75057	175057	75057	75057	382	15057	175057	175057	75057	75057	75057	75057	75057	175057	75057	75053	975053	2007	175053	75053	375053	25057	175647	75047	75047	10520
Ħ,	!								_																							8 V515CF
e it	1		8																											38		S
at. S ode) #	m	m m		nn	m	ъ.	- P	· ••	m (m P	, m	P	m ,	, ru	PD 1	m m	ĸ	ន្តន	8 8	12	ខ ង	m	, n	9 M	, kJ	M1 PO	m r	2 m	m r	מי	m	
unit M	8	ଧ ଧ	8	පුස	8	ខន	2 2	3 8	8	8 2	8	8	8 8	3 8	ខ	8 8	8	8 8	8	ឧ	3 8	8	88	3 5	8	88	8 8	5 8	មុខ	3 8	용	2
	1984	<u> </u>	<u>æ</u>	2 2	18 18	E 2	F 20	8	198	<u> </u>	138	188	1981	138	38	<u> </u>	198	<u> </u>	<u>38</u>	36	2	1982	1982	285	1982	1982 1982	26.5	1982	1982	1782	188	1982
	Hat. Site Brag. Elev. top bottos + Lab K Weth Fld X Weth (code) No. Lat. Long. no. (ft) (ft) (ft) code (code) code (cols) code (cols) code	unit Mat. Site Bran. Elev. top battos + Lab K Neth Fld K Neth Ctode) No. Lat. Long. no. (ff) (ff) (ft) + (cafs) code (cafs) co	unit Mai, Site Bran, Elev. top batios + Lab Meth Fid x Meth	unit Mai. Site Brna. Elev. top battlos + Lab K Meth Fld X Meth CCC 3 50 425205 BF3057 BP-4 689.2 36.5 BB-5 36.5 BB-4 689.2 40.0 41.5 BB-5 469.2 40.0 41.5 BB-5 469.2 40.0 41.5 BB-5 469.2 46.0 41.5 BB-5 469.2 56.0 51.5 BB-5 46.5 BB-5 56.0 51.5 BB-5 46.0 BB-5 56.0 51.5 BB-5 86.0 86.0 86.0 86.0 86	unit Mat. Site Brna. Elev. top battlos + Lab K Meth Fld X Meth Meth	unit Mat. Site Brna. Elev. top battlos + Lab K Meth Fld X Meth Meth	unit Mt. Site Brna. Elev. top battlos + Lab K Meth Fld X Meth Meth	unit Mt. Site Brna. Elev. top battlos + Lab K Meth Fld X Meth Meth	wait Mt. Site Brna. Elev. top battlos + Lab K Meth Fld K Meth Meth	wait Mt. Site Brna. Elev. top battlos + Lab K Meth Fld K Meth Meth	unit Nt. Site Bran. Elev. top battlos+ Lah Fld Neth Fld Neth	unit Nt. Site Bran. Elev. top battlos+ Lah Fld Neth Fld Neth	unit Nt. Site Bran. Elev. top battlos+ Lah Fldt Heth Heth Fldt Heth Heth	unit Nt. Site Bran. Elev. top battos + Lab K Meth Fld K Meth Meth Fld K Meth Meth	unit Nt. Site Bran. Elev. top battlos+ Lah Fidth Fidth <t< td=""><td> Math Math Site</td><td> Math</td><td> Math Math Site</td><td> Math</td><td> Math</td><td> Math</td><td> Math Math Site</td><td> Math Math Site</td><td> Math Math Site Math Math </td><td> Math</td><td> Math Math Site</td><td> With With Site</td><td> Math</td><td> Mat. Site </td><td> Mat. Site Mat. Site</td><td> Mat. Site </td><td> Math Math Site Math Concel Math Concel Co</td></t<>	Math Math Site	Math	Math Math Site	Math	Math	Math	Math Math Site	Math Math Site	Math Math Site Math Math	Math	Math Math Site	With With Site	Math	Mat. Site	Mat. Site Mat. Site	Mat. Site	Math Math Site Math Concel Math Concel Co

+ IDENTITY										+ HYDRAULIC	2		+ GRAI	GRAINSTIE PERCENTAGES	HATABES		*	ENGINEERING PROPERTIES	NG PROPES	1165			
	Ξ.	Litho-								+ CONDUCTIVITY	TIVITY		+	Litrix	ž.		Natrix 2 +	:	;				
· Founda	Strat.	Strat. unit Kat.	35	و		Rrag	היילי		#	Sample + bottom + tab K	Keth	Fld K Keth		+ Salk X (2.0 tn	5111 0.0625 to	11 25 to Clay	• • •	Soil	Perrent	Bulk Dry Percent Unit Nt.	SPT Kois	SPT Moist, tionid Plachic, (8)	9
+ (code) Year		(code) (code)	de) No.	; ;	t. Long.	•	3			(5/83) +	_	(ca/s) code		+ >2.0es 0.0625se)		0.002mm ((0.002mm)	12443 +	Class.	28	() () ()	CIO cont.	(W) cont. (I) livit index (tsf)	r (tsf
=	1982	8	, P	0 425150	50 875047	1	2 687.0	0.25.0	ł									ದ					
· =	1987	5	2	475150	_	-2	_											=					
9	682	3 2	, ř	5		_			2									: Z					
4 ;		3 8	•	100	•													ŧ a			2	•	
덛 :	20.	3 2	۸ i	7107	_	•	0.7.0											# *			3 :	7.07	
럳		3	, ,	3107	4/06/8													4			=		
z		8	'n	425147			_	e:										걸			=	2:	
=		9	N.	0 425147		74	4 692.0	0.9										건			**	0.0	
:	_	8		C1155113			_	_										2			2	=	
į	-	ì	,	15.00			•											1			:	•	
랃		片	•	422147			_											댐					
Ħ		8	m	425147		1-8 91	4 692.0											ದ					
=		٤ :		CT15CT V	47 875046													£					
1 1	_	3 8																ł z					
Ę	_	3	ή ·				•											3					
분		8	n															겁					
z		8	n			<u>2</u>	•											ರ			~;	5.0	
뻝		8	*	425146		2 2 3	5 701.0	.0 2.0										ᅺ			~	7.0	
발	1982	8	'n	50 425146	46 875054	25 T-2			0.5.5									겁			==	15.0	
豐		ឧ	M	50 425146		2		0.0 0.00										겁				5.0	
¥	1982	98	M,	•		S-8	•											ದ			_	1.0	
2		æ	**					701.0 15										Z					
2	1987	8				_		2	2 2									1 2					
į		3 8	, ×			-												į 2					
4 ;		3 ;	• •															:					
ŧ		3	л ~	-														달					
=		×	m m	50 425146		2 2	5 701.0											겁					
2	1982	8	M	50 425145		49 8-6	_											ದ			2.	19.0	
Z		8																Z			_	0.3	
×		8	M	_														E			- 34	18.0	
ä		8																l c			-		
ŧ;	701	5 :	,,				•											d :			• •		
ď	_	3	2	_			_											5			-	•	
포		8	-, -,	50 425145	145 875048		569 9-B											루			~	0.0	
¥	1982	8	r)	50 425145	145 875049			695.0 11.	5 12.0									ದ				9.0	
ż		٤	P-1	_														=					
! =		3 8		5915CF V5			707	202 0 207										4 #					
1		3 8	, ,															į					
ŧ	_	ᇙ .	. ·	_														Š					
퍞	1982	움	m)	50 425145	145 875048		507 7-0											1					
								2.50										75 12					

50 00

SPT Moist, Linuid Plastic. UC + (M) conf.(X) limit index (tsf) + + Unified Bulk dry + Soil Percent Unit Ht. : Class. P200 (pcf) + GRAINSIRE PERCENTAGES + ENGINEERING PROPERTIES
+ Rairix I Motrix I Matrix I + United Bulk dry
+ Bulk I (2.0 to (0.0425 to + 5.01) Percent Unit
+ 72.0ss 0.0425ss 0.002ss) (0.002ss) (Class. P200 (pcf 001 ರದರ ಜಿಜ್ಞಾನ ಕ ಜ್ಞಾನಕ್ಕೆ ನಿರ್ವಹ ವ ಈ ಈ ಈ ದಿರ್ವಹಿಸಿ ಕ್ಷಾಪ್ತ ಕ್ಷಣೆಗಳ ಪ್ರತಿಕ್ಷಣೆ ಕ್ಷಾಪ್ತ ಕ್ಷಣೆಗಳ ಪ್ರತಿಕ್ಷಣೆ ಕ್ಷಾಪ್ತ ಕ್ಷಣೆ ಕ್ಷಾಪ್ತ ಕ್ಷಣೆ ಕ್ಷಣೆ ಕ್ಷಾಪ್ತ ಕ್ಷಣೆ ಕ್ಷಣ 58 42 62 38 62 38 62 38 Fld K Neth (ca/s) code Saeple Saeple +
top bottom + Lab K Meth
(ft) (ft) : (ce/s) code + HYDRALLIC + CONDUCTIVITY Áppendíx 3 - Hydrűbeck dősic and engineckting data for Milkadnee cadaty – Derosso site (ISR) 7 BH 666.0 17.0 17.5

22 BHB 666.0 10.0 10.5

23 BHB 666.0 10.0 10.5

24 BHB 666.0 17.0 7.5

25 BHB 666.0 17.0 7.5

26 BHB 666.0 17.5 75.0

27 BHB 666.0 17.5 75.0

28 BHB 666.0 17.5 75.0

29 BHB 666.0 17.5 75.0

20 BHB 666.0 17.5 15.0

20 BHB 666 Surt. Brnq. Elev. no. (ft) 47520 67547 47213 87522 47213 87522 47213 87522 47219 87523 47520 87528 47520 87528 47520 87528 47520 87528 47520 87528 47520 87528 47520 87528 47520 87528 47520 87528 47520 87528 47520 87528 47520 87528 875752 875757 875757 875758 875758 875758 875758 875758 875758 875758 875748 875748 87538 87528 87528 87529 87529 87529 87529 87529 87529 87529 87529 87529 87529 87529 87529 87529 87529 87529 87529 87529 87529 87529 87529 87529 + Lithor + strat. + Courty unit Nat. Site + (tode) Year (tode) No. * IDENITY

9 4 4 4 4

2

7

2

≓

SPT Moist, Liquid Plastic, UC + (R) cost, (X) limit index (tsf) + ឌនដ 23 **** 222554742 2322 222 2222 222 + Unified Bulk Dry + Spil Percent Upit Wt. + Class. P200 (pcf) + ENSINCERING PROPERTIES 2 Ş ĸ ಶ ದ ដេនភភ Matrix I Matrix I Matrix 1 + Fld K Neth + Bult I (2.0 to (0.6525 to (cm/s) code + 22.0m 0.0625ms) ((0.002ms) Ę, + GRAINSITE PERCENTAGES Sand 2, 206-03 1.406-03 3, 50E-05 2.106-06 Sample Sample + top K Meth (ft) (ft) + Ica/s) code + HYBRAULIC + CONDUCTIVITY Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR MILAAUXEE COUNTY - FALK LANDFILL 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 3.5 659.9 Surf. Brng. Elev. no. (fft) 875200 875200 875200 875200 875200 875200 875200 875200 875200 875200 875200 875200 875154 875154 875155 875155 875155 875155 875155 875155 875155 875155 875155 875155 875155 875155 875155 875155 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 42503 Site No. + strat. + County unit Nat. + (Ende) Year (code) (code) + IDENTITY

=

38

SPI Moist, tiquid Plastic. UC + (M) cont. (2) light index (tsf) + ~ ~ 2 22 P, 5.8 16.8 3 22.3 2222 強性は関係的なな 2882K3887-788824E8=225 + sand silt ciay + Unified Bulk Bry Fld K Heth + Bulk I (2.0 to (0.0625 to + Soil Percent Unit Bt. (ce/s) code + 32.0m 0.0625ms 0.002ms) ((0.002ms) + Class, P200 (pcf) + BRAINSITE PERCENTAGES + ENSINEGRING PROPERTIES + Matery I Matery I + 2 88 ま ರದ ಸಹಕ್ಷನೆ ನೆರೆ ರನೆ ರೆರೆ ರೆನೆ ನೆ ಹೆಕ್ಕೆ ನೆ ಭೆರೆ ಕೆರೆ ಬಿ ಜಿ ನೆ ಹೆಚ್ಚೆ ರೆ ರವರದವರಹಹಹಹಿಹರರ ಹ ~ K 2 ≃ ¥ 23 \$ \$ 2 3 2,406-05 2,705-04 Sample Sample +
top bottom + Lab K Meth
(ft) (ft) + (ca/s) code + HYDRAULIC + CONDUCTIVITY Appendix 3 - HYDROGEOLOSIC AND ENSINERING DATA FOR MILMANKEE COUNTY - FALK LANDFILL 630.8 630.8 630.8 630.8 630.8 630.8 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 628.5 631.3 631.3 631.3 631.3 631.4 631.6 632.6 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 633.7 . E 8r 10 972201 972201 972201 972201 972201 972201 972201 973153 973153 973154 973154 973154 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 973155 Long. | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | 1522 | strat. unit Mat. 9 (code)(code) + County u + (code) Year (+ IDENTITY

SPT Moist, Liquid Plastic, UC + (*) cont.(2) limit index (tsf) + 2 15.9 7.8 4 用环次式对开格拉拉拉拉拉拉拉拉拉的 \$ \$ \$ \$ \$ \$ \$ Sable Sample + CANDUCTIVITY + GARINSIIE PERCENTAGES + ENGINEERING PROPERTIES

+ CONDUCTIVITY + HATCH X Match X + Cold clay + Unified Bulk Dry
top bottom + Lab X Meth Fid X Meth + Bulk I (2.0 to (0.0625 to + 50if Percent Unit Mt.

(ft) (ft) + (ca/s) code (ca/s) code + 72.0mm 0.0625mm) 0.002mm ((0.0026m) + Elmss. P200 (pcf) ĸ ರ ಈ ಥೆ ವಹಿಸಿದ ಔಹಿಸಿ ನಟರವನ್ನೆ ಹೆ ಹೆ ಈ ರದವರ ಈ ಈ ಈ ಈ ಹಿಸಿ \$ 2 = S 6, 305-05 7.306-05 Apoendix 3 - Kyrkoseclogic and Ensinering data for Milhauxee County - Falk Landfill 633.6 26.0
633.2 3.5
633.2 3.5
633.2 13.5
633.2 13.5
633.2 18.5
633.2 18.5
633.2 28.5
633.2 18.5
633.2 18.5
633.2 18.5
633.2 18.5
633.2 18.5
633.2 18.5
633.2 18.5
633.2 18.5
633.0 18.5
633.0 18.5
630.0 18.5
630.0 18.5
630.0 18.5
630.0 18.5
630.0 18.5
630.0 18.5
630.0 18.5
630.0 18.5
630.0 18.5
630.0 18.5
630.0 18.5
630.0 18.5
630.0 18.5 Surf. Brac. Elev. Long. ap. (#1) 875159 8-13 875159 8-13 875159 8-13 875159 8-13 875159 8-13 875159 8-13 875159 8-14 875158 8-14 875158 8-14 875158 8-14 875158 8-14 875158 8-14 875158 8-14 875158 8-14 875158 8-14 875158 8-14 875158 8-15 875158 8-15 875158 8-15 42524 42519 42519 42519 42519 42519 42515 42515 42515 42515 42515 42515 42515 42515 42515 42516 42516 42516 42516 42516 42516 42516 42516 42516 42516 42516 42516 42516 42516 t titho-t strat. + County unit Mat. Site + (code) Year (code) (code) No. + IDENTITY

SPT Moist, Liquid Plastic, UC + UN) cont.(2) limit index (154) + + Unified Bulk Dry + Soil Percent Unit Mt. + Class, P200 (prf) Hafrix J. Matrix Z. Matrix Z. + ENSINGERING PROPERTIES 76.9 + sand silt ciay Fid K Meth + Bolk I (2.0 to (0.0425 to (tw/s) code + 72.0ss 0.0425ss) 0.002ss) ((0.002ss) -2 + GRAINSIZE PERCENTAGES 2.806-08 Sample Sample +
top bottom + tab K Neth
(ft) (ft) + (cm/s) tode + HYDRAULIC + EGNENCTIVITY 2.5 m 788.0 788.0 788.0 788.0 788.0 788.0 788.0 788.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 792.0 £8£ 425127 880446 Mul8 175127 880446 Mul9 175127 880441 Mul4/18 175127 880442 Mul4/18 175127 880443 Mul4/18 175127 Mul4/18 1 880452 NW6A/B B80452 NW6A/B Brno. no. tong. Ę. + County unit Mat. Site + (code) Year (code) (code) Mo. 装潢装置表页要再要要要再算等等更是是是

ĸ

2

Appendix 3 - Nydrobeologic and ekbineering data for bankesha county - future parkland site

SPT Moist, Liquid Plastic, UC + (N) cont.(2) limit index (tsf) + ₹ ¥ 37. 82222222222 335 22222222 285 + Unified Bulk Bry : Soil Percent Unit Mt. + Class. P200 (pcf) 8 + ENSINEERING PROPERTIES 100.0 + Matrix X Matrix X Matrix X + sanf silt ciav + Fld K Meth + Bulk 1 (2.0 to (0.0625 to :(cm/s) code + 72.0sm 0.0625m) 0.002am) ((0.002am) S + GRAINSIZE PERCENTAGES Seth code + CONDUCTIVITY + HYDRAULIC Saple Sable + tab K top bottos + tab K (14) (ft) + (ce/s) 425131 880422 NW6A13 777.6 47 475131 880427 NW5A18 777.6 47 475131 880427 NW5A18 778.6 47 475131 880427 NW5A18 788.9 18 475131 880427 NW7A18 788.2 18 475132 880413 NW8A 788.2 18 475124 880414 NW8A 783.9 18 475123 880414 NW8A 783.9 18 475133 880414 NW8A 7 Surt. Brng. Elev. no. (ft) Leag. + County unit Nat. Site + (code) Year (code) (code) No. + IDENTITY

Aporodix 3 - Hybrogeolosic and engineering data for Krukesha county - future parkland Site

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR MAUKESHA COUNTY - FUTURE PARKLAND SITE

IDENTI		Pakka.									HYDRAUL1				+ GRAINS	IIZE PERCI	NTAGES		ŧ	ENGINEERI	NG PROPE	RTIES					
		Litho- strat.						e			COMPUCTI	VITY			+			Z Hatrix)	٠ +								
County			Mat.	Cita			D	Surt.	Sassie	Sample +					+	saná	silt	Clay		Unified		Dry					
			(code)		iał.	Lone.	Proo.	ELEY.	(43)	(4+) A	Lab K	neth	FIG K	Beth	+ Bslk 1	12.0 to	10.0525	te	+	Soil	Percent	Unit Wt.	SPT Mais	it. L	iquid P	lastic.	UΣ
													168/6/	5005	+ 72.081	0.002381	0.00Zm	((0.002mm)	: +	Class.	P200	(pcf)	(N) cost.	. (2)]:	isit	i ndex	(tsf)
EK.	1482	UC	ž	53	425121	880452	: MW10A	781.9	18.5	20.0										CL							
	1985	20			425121															CŁ			13				
	1985	20		53	425121				28.5											CŁ			9				
	1985 1985	OC OC		53 53	425121 425121				33.5											£Ł.			10				
	1985	ĐC			425121				37.5 43.5											CL			12				
	1985	9C		53	425121				48.5											CL.			11				
	1985	30		53	425121				9.0				5.60E-07	,						ξL			13				
	1985	30		53	425123				3.5	5.0			3.005-01	,						ឩ							
WX.	1985	ĐC	3	53	425123				8.5											CL CL			15				
ШK	1985	Œ	3	53	425123				13.5											EL			14 11				
HK.	1985	30	3	53	425123	880433	AHHA		18.5											EL			11				
	1985	Œ	3	53	425123	880433	ALLEN	787.2	23.5	25.0										CL.			12				
	1985	00	3 .	53	425123	880433	ALLIAN	787.2	28.5	30.0										CŁ			11				
	1985	ĐC	3	53	425123	880433	BWI1A	787.2	33.5	35.0										ČŁ.			ii				
	1985	30	3	53	425123	880433	MN11A	787.2	37.5	40.0										CL			11				
	1985	DC	3	53	425123				43.5	45.0										CŁ			13				
	1985	OC			425123				48.5	50.0										CŁ			14				
	1985	30	2	53	425123				53.5											CL			14				
	1985	20	3		425123					26.0			1.60E-08	?						CŁ			14				
	1985 1985	30 30	3	53	425115				3.5	5.0										CL			7				
	1985	96		53 53	425115 425115				8.5	10.0										CŁ.			5				
	1985	Œ	3	53	425115				13.5 18.5	15.6										CŁ			21				
	1985	OC.		53	425115				23.5	20.0 25.0										CL.			10				
	1985	30	3		425115				28.5	30.0										CL.			7				
	1985	30	3	53	425115				33.5											CL			В				
WX	1985	OC	3		425115				38.5	40.0										CL CL			4				
WK.	1985	OC	3	53	425115				43.5	45.0										EL.			11				
W).	1985	30	3	53	425115				48.5											CL			14 16				
KK.	1985	90	3	53	425115	880445	NN12A	784.3	9.0	21.0			2.00E-06	7						CL.			10				
	1985	00	3	53	425117	880428	MV13A	9 803.4	3.5	5.6				-						ει			15				
	1985	30	3	53				B 803.4		10.0										13			40				
	1985	00	3	53				B 803.4		15.0										£L			22				
	1985	20	2	\$3				802.4												EL			22				
	1985	30	3		425117					25.0										CL			16				
	1985	30	3	53				B 803.4		30.0										EL			22				
	1985 1985	30 30						9 803.4		35.0										€L			17				
	1785	90	3	53 57	125117	000428	MU47	B 803.4	38.5	40.0										EL			16				
	1985	30	ु	53 53				§ 803.4												CL			15				
	1985	30						B 893.4		50.0										α			16				
	1985	30	د د	53	425117			8 803.4 B 803.4												£1			16				
	1985	00	3		425117															CL			17				
	1985	00	3		425117															EL.			17				
	1985	90						B 803.4							0					EL			36				

SPI Moist. Liquid Plastic. UC + (M) cont.(2) limit index (1sf) + Š × 23.9 * ENSINEERING PROPERTIES 8.0 85.0 = Z + GRAINSIZE PERCENTAGES 2 2.20E-07 7 + HYDRAULIC + CONDUCTIVITY 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 863.4 1788.0 1788.0 1788.0 1788.0 1788.0 1788.0 1788.0 1788.0 1788.0 1788.0 1788.0 1788.0 1788.0 1789.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 1787.0 Surf. Brog. Elev. no. (ft) BBO428 MMI3AS 880434 B-12 880434 B-12 (2512) 889423 M (2512) 889423 (2512) 889423 (2512) 889423 (2512) 889423 (2512) 889423 (2512) 889423 (2512) 889423 (2512) 889433 (2512) 889433 (2512) 889433 (2512) 889433 (2512) 889433 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (2512) 88943 (25 Long. + steat. + County unit Nat. Site + (code) Year (code) Lode) No. + IDENTITY

Appendix 3 - HYDROGEOLOGIC AND ENGINEERING DATA FOR MAUKESHA COUNTY - FUTURE PARKLAND SITE

+ 1DEM! 15T									•	+ HYBRAULIE	ديا		+ BEGINSITE PERCENIAGES	C PERCEN	65.5		+ ENGINEERING PROPERTIES	MG PKG-12	115				•-
+	Litho-								+	CONDUCTO	71 I.Y		.,	Matrix 1	Matrix 2	Hatrix I							+
	strat.						Sert.	Sample	Sante +					1400	siłt	C13V	+ Uhissed	R.	Pry				•
+ County	unit Het. S	Het.	Site			groo.	Elev.	top	bottoe +	tab X	Meth	fld K Keth	+ Bulk X	(2.6 to	(0.0625 to		+ Soil	Percent	Unit St.	SPT Noist	. Liquid	Plastic.	÷
+ (code) Year (code) (code) No.	r (code)	(code)	Ж. Э	Lat.	tog.	ė	Long. no. (ft)	£	# #	(cs/8)	tode	(#t) (#t) + (ca/s) code (ca/s) code + >2.0m 0.0425am) 0.0426am) (0.002am) + Class. P200 (pcf) (#) cont.(I) limit index (tsf) +	+ >2.0m	0.062544)	0.00200)	((0.002m)	+ Class.	200	(bcf)	(N) cont.	2) linit	index	(tsf) +
1981 XI	8	m	B	425123	880438	7P-6	788.0	0.0	0.4			WK 1984 CC 3 53 425123 BB0438 TP-8 788.0 0.0 4.0					7						
NK 1984		**	3		88043	4-4£	788.0	11.0	1 TP-6 788.0 11.0 13.0								2						
NK 198		m			88043	9-41	788.0	17.0	17.0								3				23	ä	
KK 1984		M		425123	88042	19-7	788.0	0.0	5.0								ದ						
MX 1984	8	m		125123	258	17-71	789.0	789.0 7.0	10.0				•	~>	7	ž	ದ	97.0			**	27	
1881		***		125123	89.47	19-7	788.0	11.0	4.5								4						

aporráix 3 - hydadseologic and engineerins data for hautesha county - future pariland site

Appendix 3 - HYDROSECLOGIC AND ENGINEERING DATA FOR MILMAUREE COUNTY - (MEPCO) CALEDONIA EXPANSION

IDENTIT		Litho-									HYDRAUL IS		÷		IZE PERCEN				NGINEER	NS PROPE	RTIES					
		strat.						Suri	Sant	+ + Sample +	CONSUCTIV	111		+			Matrix I									
County		unit		Cita				Elev.						+	sand	silt	clay		Unified		Brv					
(code)					1.4					DOTTOR +	Lab K	Meth	Fld K Heth	+ Bulk X	(2.0 to	(0.0625 t	0	:	Soi i	Percent	Unit ¥t.	SPI	Moist.	Liquid	Plastic	. uc
		110067				Long.	40.	(11)	(11)	(11) +	(Ca/S)	COSE	(ce/s) code	+ >2.0m	0.0525as)	0.002mm1	((0.002es)	+	Class.	P260	incfl	CMA	cost ill	limit	inder	16+41
	1986			54	425020			700.	3.5	5.0									CL			28				4.5
RA			3		425020			700.6	8.5	10.0									EL			29				4.0
	1986		3	54	425020	875050		700.	10.0	12.0	1.31E-08	3							ä		109.0	21	2.0	40	22	3.5
RA			3		425020				18.5										ČL.		111.0	20		36	17	
	1984		3	54		875020			31.5	33.5									a		109.0	••	21.0	37	19	
RA		30	3		425010				3.5	5.0	5.25E-08	3							CL			23		•	• • •	4.5
	1986	30		54		875021			8.5										α			43				****
RA		30	3	54	425010				13.5										CL			27				3.8
	1986		3	_	425010				18.5										CL			21				3.3
RA		00	3		425010				23.5								*		CL			28				4.5
RA		DC DC	3	54	425010				28.5										CL.			12				
RA		20	3	54	425010				33.5										CL.			16				1.0
RA		00	3	54	425010				38.5							25			εL		115.0	24	19.0			2.3
RA		30	3	54	425010				43.5										CŁ		104.0	25	21.0	35	18	2.0
	1986	30	3	54	425010				47.0										α						•••	
RA		OC	3	54	425017				32.5		4.56E-08	3							CL.		122.0		15.0	25	11	
	1986		3	54	425016					5.0									α			28			•••	4.5
	1986	00	3	54	425016					10.0									Ü		122.0	29	16.0			4.5
	1986	DC	3	54	425016				13.5	15.0									α			33				
	1984	30	3		425016				18.5										CL			14				3.5
	1986	00	3	54	425016				23.5	25.0									£1.		122.0	19	16.0			3.0
RA		30	3	54	425016				28.5	30.0									εL			24				3,3
	1986	OC.	3	54	425016				33.5										CŁ			27				2.0
RA		20	3	54	425016				38.5	40.0									£L		133.0	25	15.0	22	7	2.0
	1986	00	3		425016				43.5	45.0									£L			25				4.0
RA A		90	3	54	425016				45.0	46.5	1.895-08	3							£L		118.0		16.0	29	14	
	1986	00	3	54	125022				30.5		5.70E-0B	3							£		89.0		32.0	36	14	
RA DA		20	3		425029					4.0									£L			35			• •	
	1988	30	3	54	425029					10.0									£Ŀ			26				
RA		20	3	54	425029				12.5	14.0									£1.			15				
RA		20	3	54	425021					5.0									£L			11				
RA		00	3		425021					10.0									FL.		119.0	38	15.0			4.0
	1988	20	5	54	425021				13.5	15.0									ЖL			56				
RA		30	5	54		875021			18.5	20.0									CL			70				
RA		20	3	54	425021				23.5	25.0									CL			18	15.0	28	13	3.5
RA		DC	3	54	425021				28.5	30.0									CL			14			•••	2.0
	1986	20	3	54	125021				33.5	35.0									EL			29				2,0
RA		00	3	54	425021				38.5	40.6									EL			29	20.0			3.3
AA AA			3	54	125021				43.5	45.0									CL.		123.0	44	16.0	27	12	2.8
RA DA		20	3		425021				46.5	48.5									C1.							
RA DA		30	3	54	425024				3.5	5.0									CL			15				2.5
AA CA		90	3	54	425024				8.5	10.0									CL		121.0	43	16.0			4.5
	1986		3	54	425024						5.87E-08	3							CL		126.0		14.0	25	11	
RA DA		20	3	54	425024				13.5										CL.		117.0	19	17.0	28	13	
	1986		3	54	425019					5.0									ČL.		115.0	13	20.0			2.3
RA	1986	36	3	54	425019	875032	¥-29	707.5	8.5	10.0									EL			36	•			1.5

SPT Maist, Liquid Plastic, UC + (W) cont. (2) liaft index (tsf) + 2.0 3.3 2 2 Ξ 2 53 23 2 ≃ ≌ 22828282 ⋍우⋷ * + Unified Bulk Drv + Soil Percent Unit Mt. + Elass. P200 (pcf) 120.0 117.0 108.0 8.0 + Matrix I Matrix I Matrix I + EMGIMEENING PROPERTIES
+ sand silt clay + Unitied Bulk Dry
Fid K Meth + Bulk I (2.0 to (0.0625 to + Soil Percent Unit Bi
(cafs) code + 22.0se 0.0625se) 0.002me) ((0.002me) + Eless Properties 2 おひださ ひこむ ひ ひ ひ ひ ひ ひ ひ ひ む せ は 来 量 重 오 botton + Lab K Meth (ff) + (cn/s) code + HYDRALLIC + CONDUCTIVITY 9.996-08 2.615-08 20.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115.00 115 707.5 707.5 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 705.0 Surt. Brng. Elev. Long. no. (ft) 87502 H-29
87502 H-29
87507 H-20
87507 H-30
87507 H-30
87507 H-30
87507 H-30
87507 H-31
87507 H-32
87507 H-32 425019 425014 425014 425014 425014 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 425016 42 + County unit Mat. Site + (code) Year (code) Good RA 1986 RA 198 + IDENTITY

Apsendix 3 - HYDROBECLOGIC RND ENSINEERINS ONTA FOR MILHAUKEE COLUTY - (WEPCO) CALEBONIA EXPANSIÓN

Moist. Liquid Plastic. UC + cont.(%) Limit index (tsf) + -S æ % € 82222 2822222222222 Unified Bulk Bry Spii Percept Unit Ht, S Class, P200 (pcf) (+ EMSINEBRING PROPERTIES
+ Unified Bulk Bry
+ Spil Percent Unit #1
+ Class, P200 (pcf) 6 3 8 42 ದವರದರೆದರೆದರೆ ನೆನೆ ಮದದರೆದೆ ದೆದರಿದ್ದ ವೆಸ್ತರದ ದರವರದ ವರಸ್ಥೆ ಪರವರದ ದೆ. ಈ ಸಂಪರ್ವದ ಪರಿಸ್ತರ ಪರವರ ಪರಿಸಿದ್ದ ಪರವರ ಪರವರ ಪರಿಸಿದ್ದ ಪರವರ ಪರವರ ಪರಿಸಿದ್ದ ಪರಿಸಿದ್ದ ಪರವರ ಪರವರ ಪರಿಸಿದ್ದ ಪರಿಸಿದಿದ್ದ ಪರಿಸಿದ್ದ ಪರಿಸಿದ ಪರಿಸಿದ ಪರಿಸಿದ ಪರಿಸಿದ ಪರಿಸಿದ ಪರಿಸಿದ ಪರಿಸಿದ ಪರಿಸಿದ ಪರಿಸಿದಿದಿದೆ. ಪರಿಸಿದ ಪರಿಸಿದ ಪರಿಸಿದಿದ ಪರಿಸಿ Hatrix I Hatrix I Hatrix E + Sulk 1 12.0 to (0.0625 to + 20.0s 0.0625ss) 0.002ms) (<0.002ms) 33.0 88 ÷. 8.0 32.0 70.0 SRAINSIJE PERCENTAGES 3. **\$** ž 3 5.0 ÷ 2 . 2 Keth F16 K 2.53E-06 2.71E-06 4.26E-06 5.11E-04 1.155-05 Keth Code + KYDRAULIC + CONDUCTIVITY bottos + Lab K K (ft) + (cs/s) c Sapte top (ft) 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 8833.0 88 £ 5.5 881047 TH-65
881041 P-648
881053 P66-8
881054 TH-62
881046 TH-62
881046 TH-62 Brng. Bo. Logi. 4 6 2 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 4 5 3 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 3 4 5 Ę, Site No. strat. unit Mat. S (code)(code) N + County us + (code) Year (+ 10ENTITY

Appendix 3 - HUDROSEOLOGIC AND ENGINEERING DATA FOR MILHAUSE COUNTY - MUSICESD

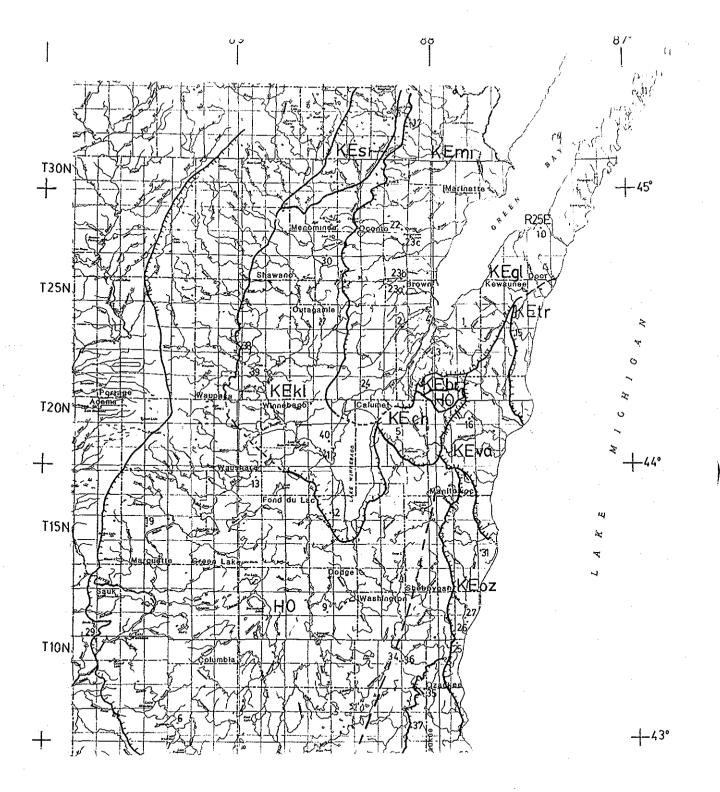
SPT Moist, Liquid Plastic, UC (IN) cost,(2) limit index (1st) のの計の可のなんになめのとの名は、それは言ななめのはのでのからもなれなにとななられるともなる。 + Unified Bulk Drv + Soil Percent Unit Mt. + Class, P200 (pcf) + ENSINEERING PROPERTIES 2 8 23 다 그 다 중 중 다 다 다 다 다 보 보 보 法 法 15.0 6.0 ₽. 2,0 5.0 38.0 21.0 5.0 15.0 ERAINSIZE PERCENTAGES 200 ÷ 79.0 9.0 2.0 63.0 39.0 Sarcie Sanie +
top button + Lab K Helh
(H) (H) + (cm/s) code + HYDRAIM IC + CONDUCTIVITY 837.6 887.6 887.6 887.6 887.6 888.4 888.4 888.4 888.4 888.4 888.4 888.4 888.4 888.4 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 887.1 881046 Th-42 881046 Th-42 881046 Th-42 881046 Th-42 881040 P-438 881050 P-438 881029 TN-61 881029 TN-61 68199 947-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 60-4 601188 601188 601188 601188 601188 601188 601188 601188 601188 601188 601188 601188 601180 Brae. 65338
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538
65538 + County unit Mat. Site + (code) Year (code) (code) No.

Apaendix J - HYDROGEDLOGIC AND ENGINEERINS DATA FOR MILWAUKEE COUNTY - MUSKEGD

SP? Moist. Liquid Plastic. UC : (M) coat, (2) limit index (tsf) + 2.5 5.5 2.2 Unified Bult Dry Soil Percent Unit Ht, S Elass, P200 (pcf) (Hatry Z. Hatry X. + ENGINEERING PROPERTIES sand silt + sand silt clay Fld K Meth + Bulk X (2.0 to (0.0625 to (ce/s) code + 22.0se 0.0625ss) (0.002ss) ((0.002ss) 5.6 0 0. ÷. 3 8 22.0 16.0 19.0 GRAINSTIE PERCENTAGES 3.0 68.0 73.0 20.0 73.0 9 23.0 Neth Code + ECMOUCTIVITY + HYDRAULIC (s/s) 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 839.6 83109 P-678
881109 P-678
881109 P-678
881109 P-678
881109 P-678
88109 P-678
88109 P-68
88104 P-68
88108 P-7
88108 P-7 881051 IN-71 881051 IN-71 881051 IN-71 881051 IN-71 881051 IN-71 881051 IN-71 881056 IN-72 881046 IN-72 88104 891048 TN-70 881048 TN-70 881048 TN-70 ğ. 9 + County unit Nat. Site + (rode) Year (code) (code) No.

Apoendix 3 - BYDROGEOLDGIC AND ENSINEERING DATA FOR MILKRUKEE COUNTY - NUSKEBO

SPI Moist, Liquid Plastic, UC + 18) cont.(2) limit index (tsf) + 5.5.5.5.5. S 医乳体 经股份的证据的证据的 化铁铁 Unified Bulk Drv Soil Percent Unit Wt, Si Elass, P200 (pcf) H ENGINEERING PROPERTIES E ದವದದದದದದವನ ಹಹದ ಚ + SPAINSIE PERSENTAGES + Matrix Z Matrix I Satrix I + and sill crav Fid K Meth + Ball 2.2 to (0.0452 to (tes/s) code + 72.0as 0.0625as 0.002as) % 12.0 67.0 . ? 2 Sample Sample +
top bottom + Lab K Neth
(ft) (ft) + (cm/s) code + HYDRAULIC + CONDUCTIVITY Apoendix 3 - Hydrosedydosic rad ensineering data for milhankee county - niskeed 55.0 77.0 77.0 77.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 75.0 852.7 852.7 852.7 852.7 852.7 852.7 852.7 852.7 835.7 835.7 835.7 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 835.5 Surf. Brng. Elev. 80. (ft) 425340 881044 8-72
475340 881044 8-72
475340 881044 8-72
475340 881044 8-72
475340 881044 8-72
475340 881049 8-73
475340 881049 8-73
475347 881049 8-73
475347 881049 8-73
475347 881049 8-73
475347 881049 8-73
475347 881049 8-73
475347 881049 8-73
475347 881049 8-73
475347 881049 8-73
475347 881049 8-73
475347 881049 8-73
475347 881049 8-73
475347 881049 8-73
475347 881049 8-73
475347 881049 8-73
475348 881034 8-74
475348 881034 8-74
475348 881034 8-74
475348 881034 8-74
475348 881034 8-74
475348 881034 8-74
475348 881034 8-74
475348 881034 8-74
475348 881034 8-74
475348 881034 8-74
475348 881034 8-74
475348 881034 8-74
475348 881034 8-74
475348 881034 8-74
475348 881034 8-74
475348 881034 8-74
475348 881034 8-74
475348 881034 8-74
475348 881034 8-74
475348 881034 8-74 + strat. + County unit Mat. Site + (code) Year (code) (code) No. + IDENTITY



EXTENT OF ICE ADVANCES RESPONSIBLE FOR LITHOSTRATIGRAPHIC UNITS

The extent of ice advances responsible for lithostratigraphic units is after Mickelson et al. (1984). Ice marginal positions are indicated by moraines: these were traced from Lineback et at. (1983) and Parrand et al. (1984). The tills in lithostratigraphic units were deposited by ice within the approximate margins drawn on this figure, but tills are not always present at the land surface within the margins. For example, till of the Glenmore Member does not cover all the land surface of the Door Peninsula (the peninsula separating Green Bay and Lake Michigan), but the ice advance that deposited the Glenmore Member covered the Door Peninsula entireiv.

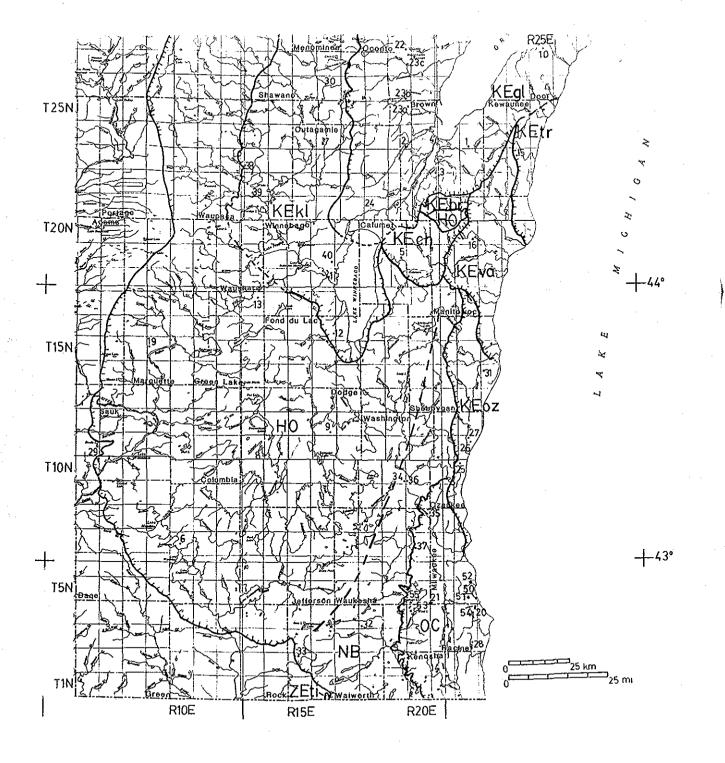
The southern extent of the gracial advance that deposited the Haven Member of the Kewaunee Formation is problematic. Mickelson et al. illustrate the Haven Member as extending farther south than the Valders Member. No southern ice margin associated with the Haven Member is shown here, and the mapped location in Mickelson et al. (1984) is "purely diagrammatic" (Mickelson, personal communication, 1987).

Site numbers are consistent throughout the text, illustrations, and appendices. Appendix 2 includes township and range coordinates for each site.

- •2 location of land disposal site studied
 - inferred position of the ice margin

ice marginal position indicated by a moraine

KΕ Kewaunee Fm. KEmi Middle inlet M. KEk1 Kirby Lake M. **KESi** Silver Cliff M. KEgi Glenmore M. Chilton M. KEch KEbr Branch River M. KEtr Two Rivers M. **KEva** Valders M. KEha Haven M. KEoz Ozaukee M. Oak Creek Fm. NB New Berlin Pm.



deposited by ice within the approximate margins drawn on this figure, but tills are not always present at the land surface within the margins. For example, till of the Glenmore Member does not cover all the land surface of the Door Peninsula (the peninsula separating Green Bay and Lake Michigan), but the ice advance that deposited the Glenmore Member covered the Door Peninsula entirely.

The southern extent of the glacial advance that deposited the Haven Member of the Kewaunee Formation is problematic. Mickelson et al. illustrate the Haven Member as extending farther south than the Valders Member. No southern ice margin associated with the Haven Member is shown here, and the mapped location in Mickelson et al. (1984) is "purely diagrammatic" (Mickelson, personal communication, 1987).

Site numbers are consistent throughout the text, illustrations, and appendices. Appendix 2 includes township and range coordinates for each site.

•2 location of land disposal site studied

Inferred position of the ice

ice marginal position indicated by a moraine

Tiskilwa M.

KE. Kewaunee Pm. KEmi Middle Inlet M. KEk l Kirby Lake M. Silver Cliff M. KEsi KEgi Glenmore M. KEch Chilton M. KEbr Branch River M. KEtr Two Rivers M. KEva Valders M. KEha Haven M. Ozaukee M. KEoz OC. Oak Creek Fm. NB New Berlin Fm. Roricon Fm. но Zenda Pm. ZE

ZEti